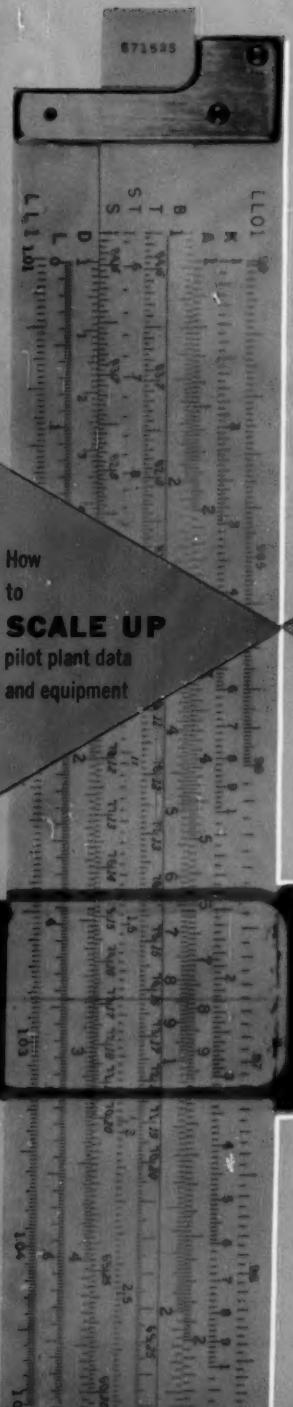


OCTOBER 6, 1958

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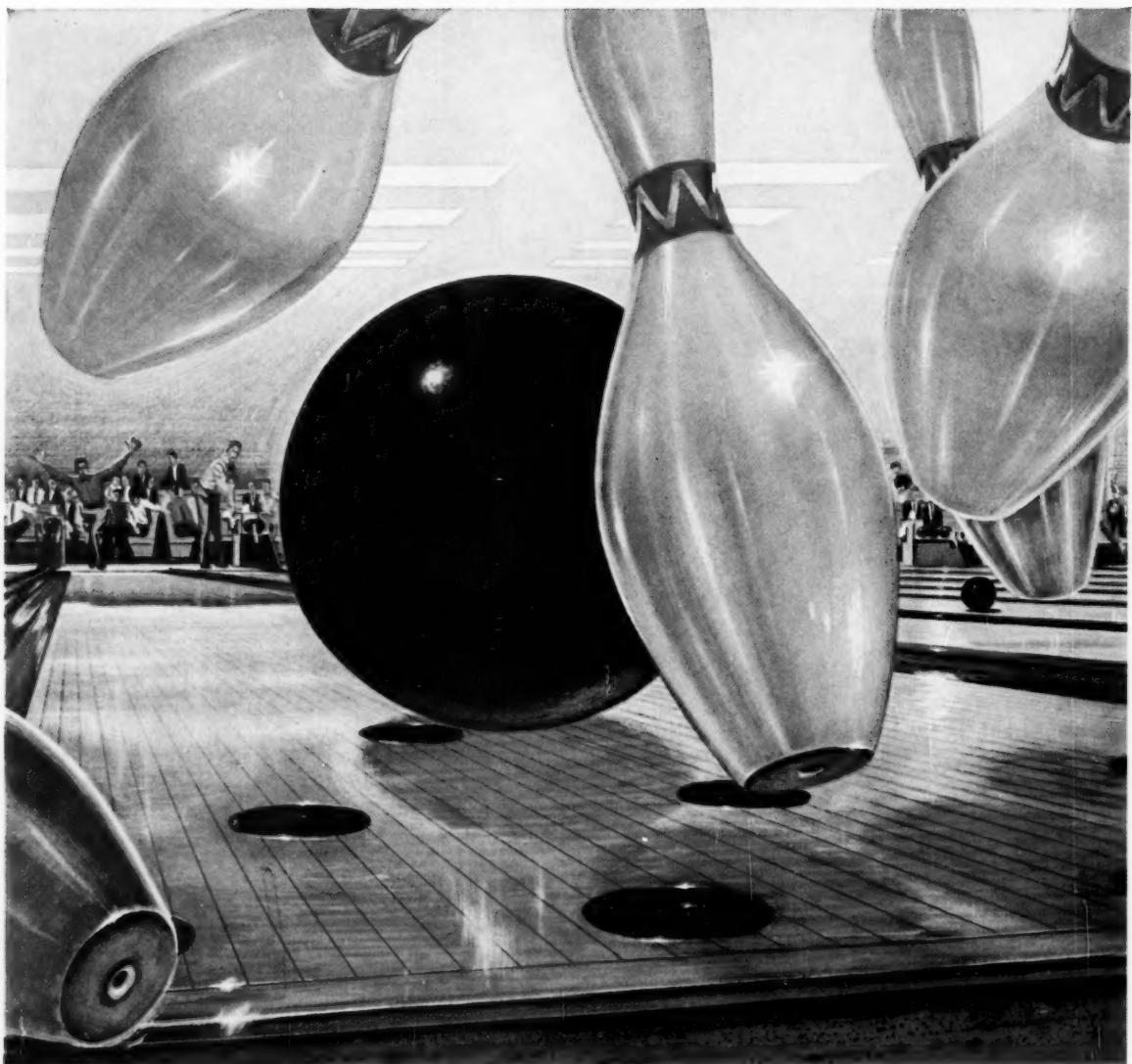
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data and
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ENGINEERS ON STRIKE

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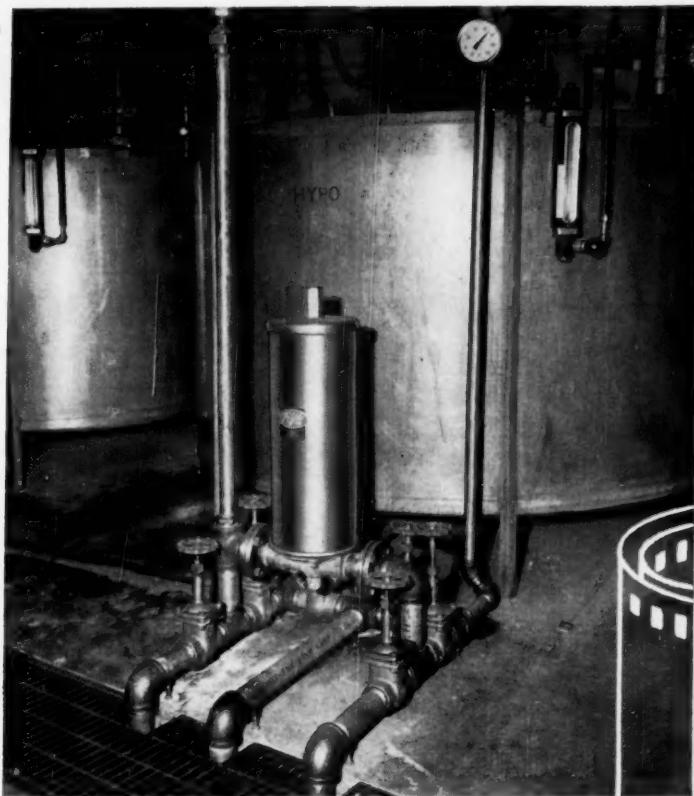
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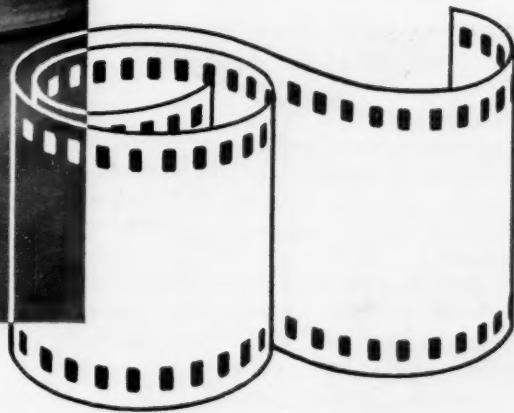




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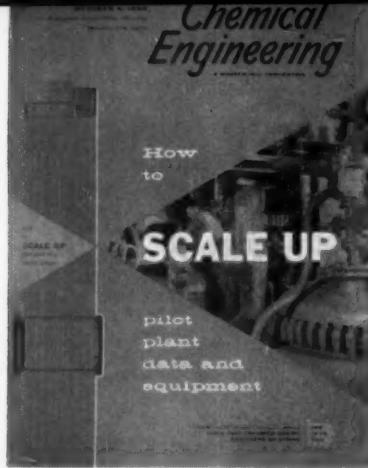
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20/26

Best way to grow oaks from acorns

Here's how to successfully and painlessly extrapolate your pilot-plant data and equipment into a full-size working plant. You'll be able to thread a much safer course through a maze of problems: heat and mass transfer, process rates, equipment geometry. Now you'll be better able to convert your reaction and other small-scale facts into a set of logical and usable relationships for big-scale planning. (p. 129)

Up-to-the-minute costs

This time we've some U-tube heat exchanger curves. They'll convert heat transfers area into fob. dollars—a mighty big help with your preliminary cost estimates. They're part of a new series of provisional standards and we'll bring you more. (p. 141)

Three answers from one chart

Single new chart is latest aid for your countercurrent extraction operations, even if they're multistage. It quickly finds your optimum economic conditions. It's another time-saver; a simple way to cut out needless figuring. (p. 142)

To keep siphons in their prime

Always-ready siphon is a smart way to keep tank levels under control. Especially where your under-liquid connections are hard to make—or impossible. Where can you use this prize-winning idea? (p. 153)

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Chemical Engineering

This issue's
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OCT. 6, 1958

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This 12-page feature report—final installment in our pilot-plant series—will give you expert help in using pilot-plant data for production scale-up.

Here are up-to-the-minute heat exchanger costs 141

Sleuthing for timely, reliable sources of cost information? Here's the first of a series of cost charts, based on data from the American Assn. of Cost Engineers.

Use this chart for extraction design problems 142

Now, one chart gives optimum values for the many variables in multistage, countercurrent operations. Chart works for systems of linear and moderately linear distribution.

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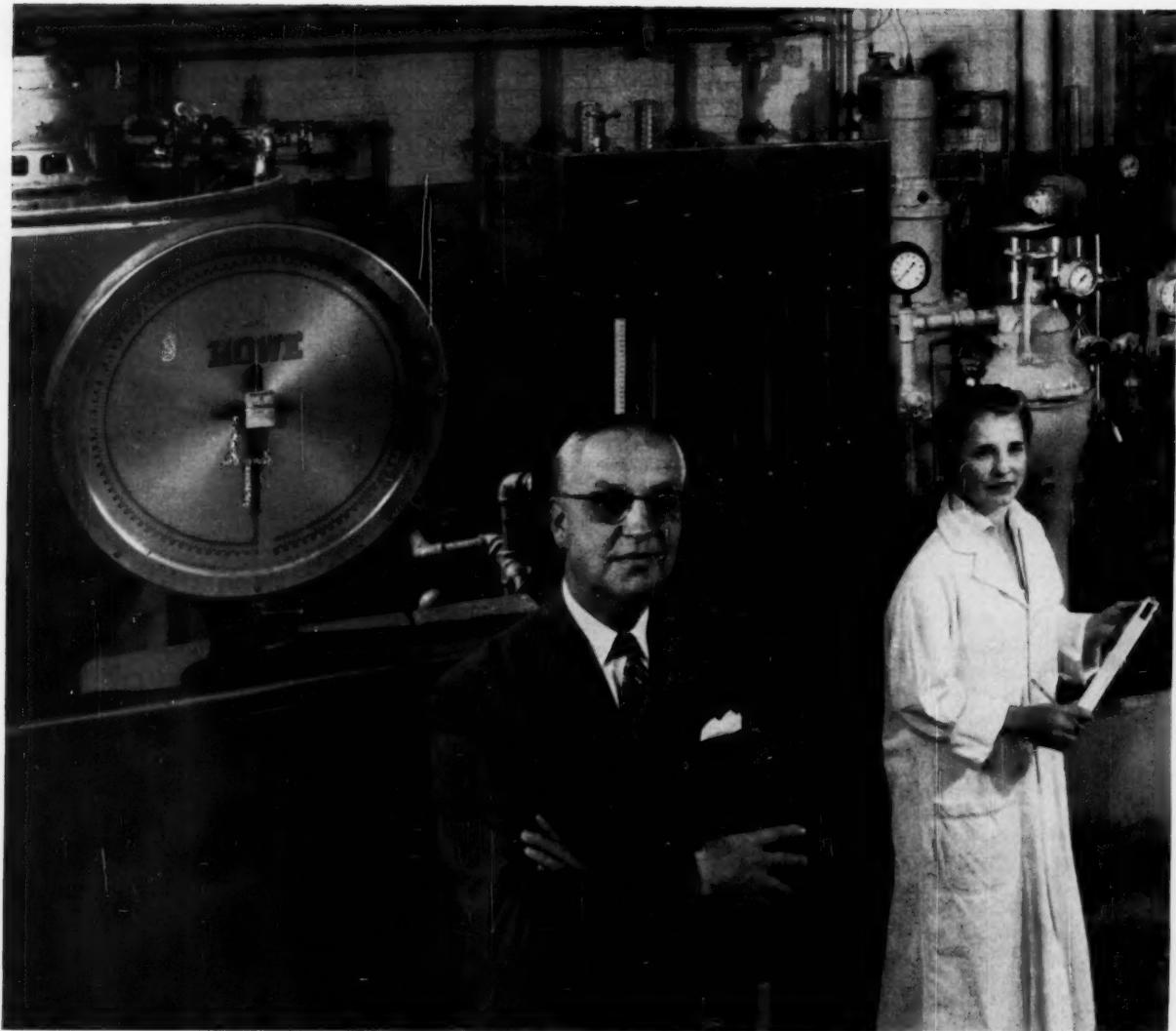
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"De Laval's pilot plant simulates your process conditions to solve centrifugal processing problems."

Fred Wheelwright, De Laval Separator Company

"The photograph above shows the major portion of De Laval's pilot plant setup at our Poughkeepsie, N. Y., headquarters . . . and some of the key people responsible for its operation.

Basically, what we provide here is a complete centrifugal processing facility in which you can test your processes without having to build your own pilot plant. We find the answers to problems concerning separation, clarification, classification or concentration of liquid-liquid-solid or liquid-solid mixtures. These findings are then applicable to the operation and/or construction of your own process facilities.

Facilities: Our plant has the capacity to handle samples in reasonable production quantities. It has stages for mixing,

reaction, heating and three stages of separation . . . followed by a continuous high vacuum dryer. Most of the equipment is stainless steel to permit us to handle corrosive liquids. We've found very few situations in which we could not simulate process conditions well enough to give an accurate reading on process efficiency or feasibility.

Examples: We've done work here for many of the country's leading chemical companies. Typical examples of the problems we've handled are:

- removing oversize particles from polyvinyl latex.
- continuous high-volume removal of uranium salts from loaded solvents.
- removing catalysts from re-arranged lard.



And one of the best-known products of this pilot plant is the patented De Laval tall oil process. The patent on this continuous acidulation process (full information on request) is based on work done here by our Manager of Industrial Engineering, Frank Sullivan.

Personnel: In the center of the picture: Frank Sullivan, B.Ch.E. at N.Y.U., and a Master's at Stevens Institute . . . one of the country's foremost authorities on centrifugal processing, has published many papers on various aspects of centrifugal technology. With De Laval since 1950, Mr. Sullivan is responsible for the engineering development of all De Laval's industrial equipment and processes, and for the industrial laboratory and process laboratory.

Next to Mr. Sullivan is Mrs. Lois Crauer, B.S. degree from U. of Rochester, a member and active in the A.C.S. and A.O.C.S. Undoubtedly one of the best-known authorities (and certainly one of the prettiest!) in the field of vegetable oil processing, Lois Crauer's work at De Laval places particular emphasis on development of chemical processes.

At the far right of the picture is Victor Lindenman, Jr., Chemical Engineer (Northeastern University) responsible for direct supervision of the pilot plant. Between him and

Mr. Sullivan is Lowell Signor, Jr., Test Man responsible for operation and maintenance of the pilot plant equipment. And that's me, Fred Wheelwright, on the left.

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DE LAVAL PACIFIC COMPANY,
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New casting technique produces sound, high-quality shapes at fraction of machined part cost

For the first time, *cast* titanium shapes are readily available—such as the globe valve pictured at left. One piece or a hundred can be produced at reasonable cost. This important development was made possible through the efforts of skilled foundrymen working with a new rammed graphite mold composition developed by Du Pont.

Sound, high-quality titanium castings are highly resistant to many corrosive environments such as hypochlorite slurries, brackish water and chlorinated organic compounds. Result: long service life, reduced downtime, lower initial and operating costs.

PIGMENTS DEPARTMENT



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life... corrosion resistance... economy in use

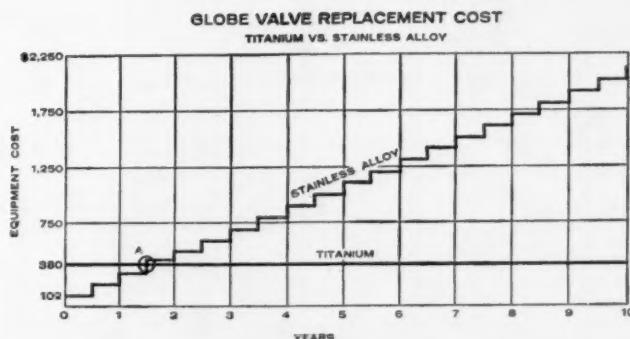
Proven Economies

Titanium is actually the *least expensive* metal you can use under many corrosive influences. It withstands conditions that reduce the service life of ordinary and high-alloy metals... cuts downtime and replacements.

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Wet Chlorine
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Most Inorganic Chloride Solutions
Molten Sulfur
Chromic Acid
Aqua Regia
Hypo-chlorites and Chlorine Dioxide



GREATER ECONOMIES are now possible through use of cast titanium valves. Stainless alloy and titanium globe valves were tested in an environment of 65% nitric acid at 110° C. Stainless alloy valve cost \$102*... but had a *maximum* service life of only 6 months (some lasted only 3 months). The titanium valve cost \$380*, showed no sign of corrosion after 6 months. Life expectancy: 10 years *minimum*. The \$278 difference in cost was absorbed in less than 1½ years (Point A). After 10 years, a single titanium valve will save more than \$1,750 in replacement costs alone!

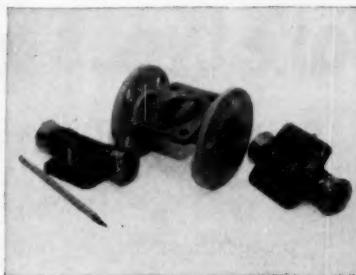
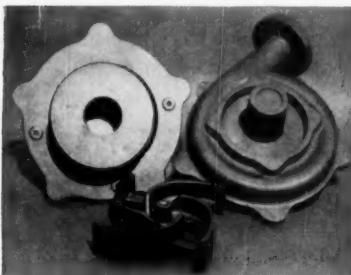
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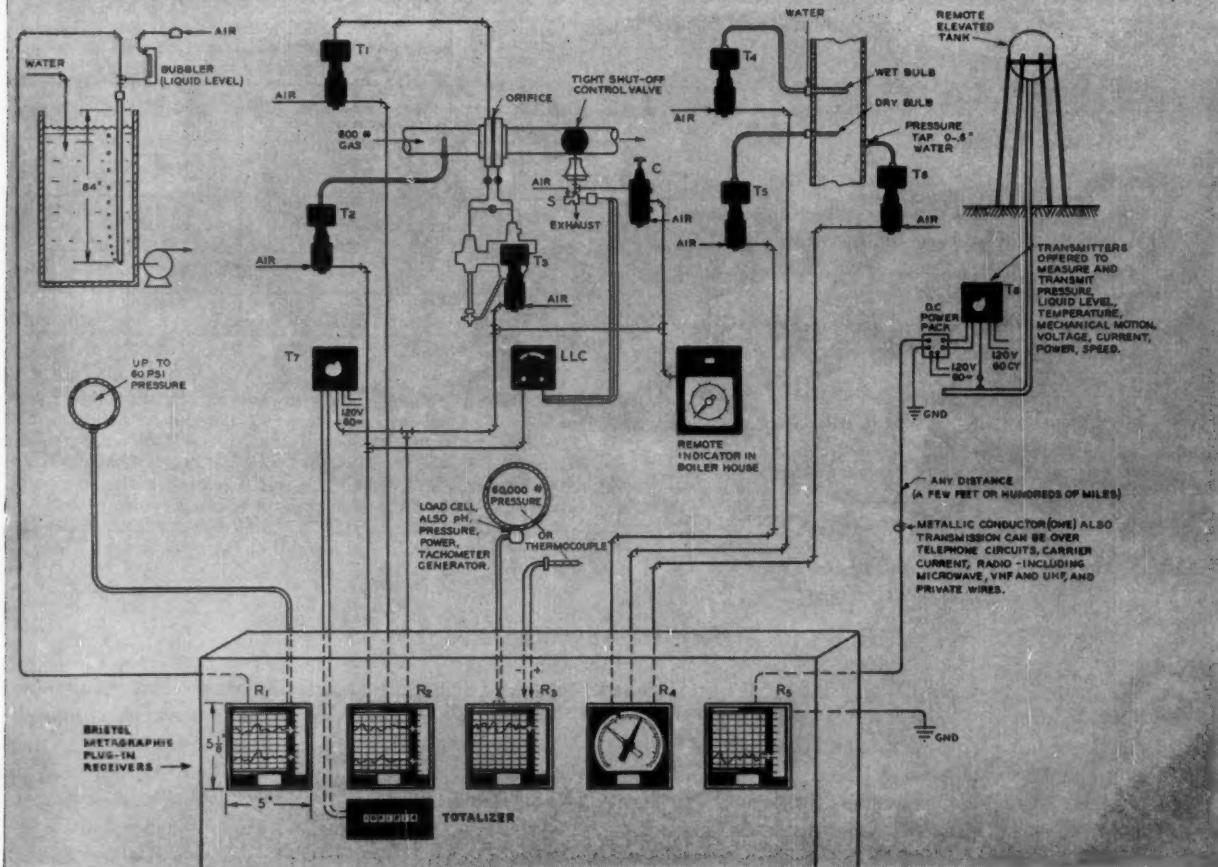
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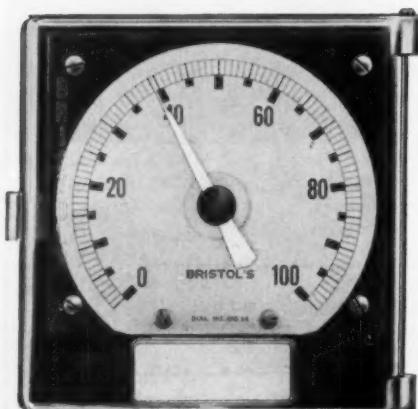
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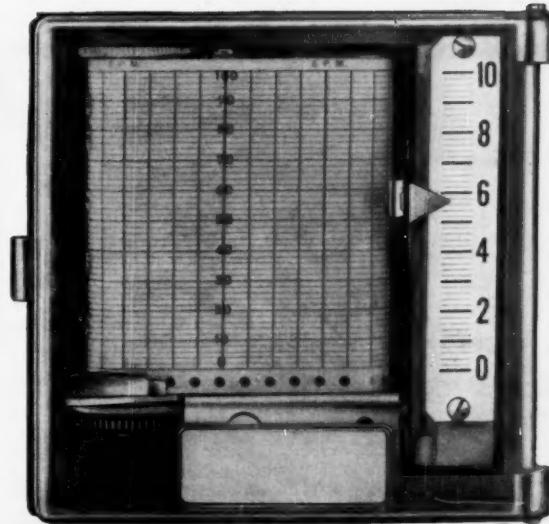
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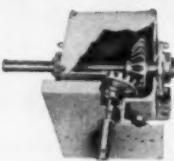
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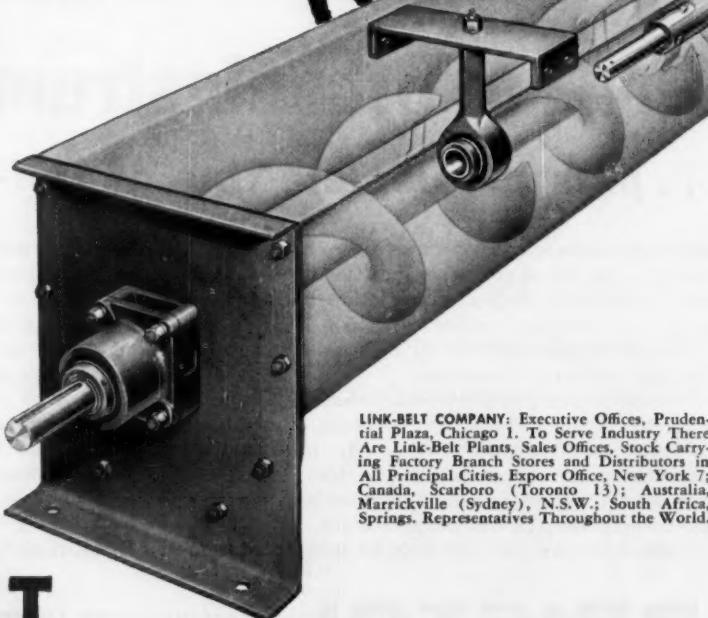
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Pressed Steel Tank Company

Manufacturer of Hackney Products

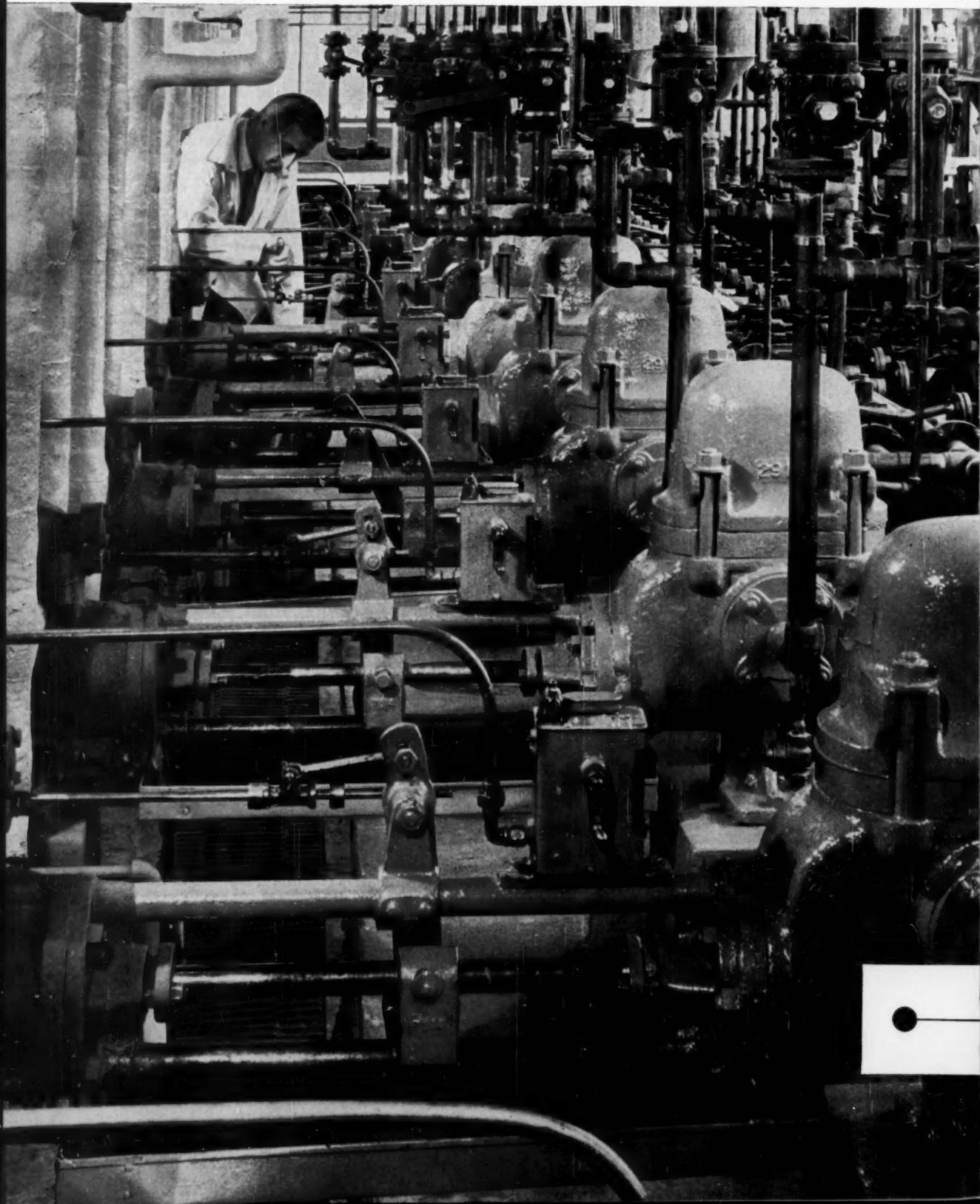
1447 South 66th Street, Milwaukee 14, Wisconsin

Branch offices in all principal cities

CONTAINERS AND PRESSURE VESSELS FOR GASES, LIQUIDS AND SOLIDS

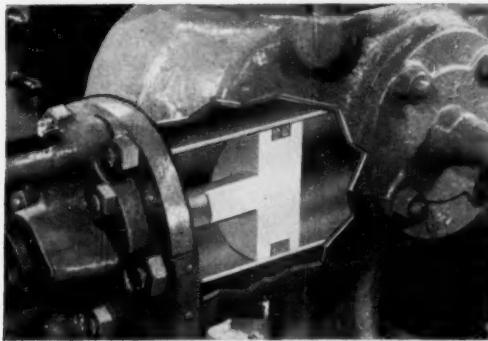


Garlock Lattice-Braid* Teflon[†] Packings help Kodak



Recover 95% of Film Process Solvent for Re-Use

TODAY, at Eastman's Kodak Park Works in Rochester, Garlock LATTICE-BRAID Teflon packings are playing an important role in helping to recover, for later re-use, 95% of the solvents used annually in the coating of film.



DOING A JOB that neither rubber-impregnated canvas, duck, or other packings could do in the past, the LATTICE-BRAID Teflon packings provide tight seal up to 100 psi pressure in more than 100 pumps which move solvents from underground storage to various distilling operations where it's refined and prepared for use again. As part of the piston that furnishes pumping compression, the packings are constantly exposed to the solvent mixture and must be able to withstand its action without swelling or deterioration. In addition, the packings must create as little friction—and resulting wear—as possible on the cylinder liners while the piston moves at rates as high as sixty 12" strokes per minute.

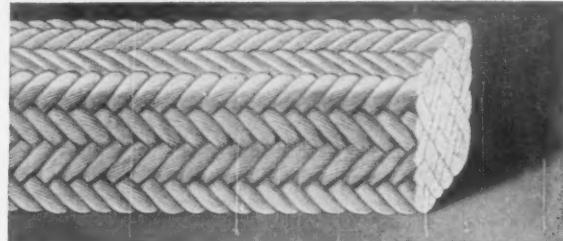
Garlock LATTICE-BRAID Teflon Packings have provided reliable service, without shutdowns for

*Registered Trademark
†DuPont Trademark

Ten of the reciprocating pumps used in solvent recovery at Kodak, Garlock LATTICE-BRAID Teflon Packings on the pump pistons have given satisfactory service since the first installation 2 1/2 years ago.

THE GARLOCK PACKING COMPANY, Palmyra, N. Y.
FOR PROMPT SERVICE, contact one of our 30 sales offices and warehouses throughout the U.S. and Canada.

maintenance, as well as increased pump efficiency due to reduced slippage. There is also a lower coefficient of friction of packing to cylinder liner, while the liners themselves appear to remain in excellent condition.



LONGER OPERATING LIFE of both pump and packing lies in Garlock's use of Teflon yarn woven in lattice-braid construction. Each strand of Teflon passes diagonally through the body of the packing at an angle of approximately 45°. This through-and-through braiding makes a completely unified structure, resulting in greater strength. Garlock's LATTICE-BRAID has no outer cover to wear through; its through-and-through structure holds together when worn far beyond the limit of ordinary packings, resulting in longer packing life.

ADD to these features the fine physical properties of the Teflon yarn—chemical inertness, low friction coefficient, temperature stability, excellent cold-flow resistance—and you have the finest packing on the market.

LATTICE-BRAID Teflon Packing is another important part of "the Garlock 2,000" . . . two thousand different styles of packings, gaskets, and seals to meet all your needs. The only complete line. That's why your Garlock representative can give you unbiased recommendations. Call him or write for Folder AD-131.

GARLOCK

Packings, Gaskets, Oil Seals, Mechanical Seals,
Molded and Extruded Rubber, Plastic Products



MEASURING UNIT

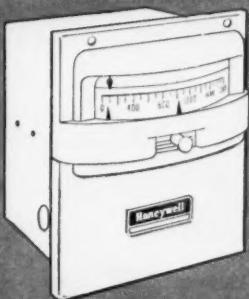
- A. A thermocouple signal to a d'Arsonval galvanometer, the only moving part, moves the indicating pointer up scale.
- B. Aluminum vane adjusts the amount of light received by the photocell from the operating lamp.
- C. If operating lamp or photocell fails, output voltage assumes a value equal to high temperature.



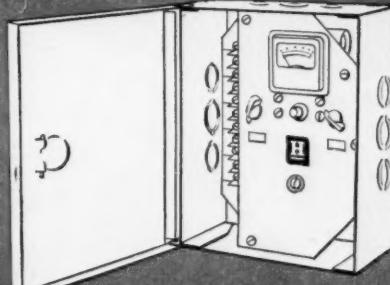
CONTROL UNIT

- D. A one-stage magnetic amplifier amplifies small current from the photocell in the measuring unit. This is the only active electronic element in the controller.
- E. Pilot light goes out on line power failure.

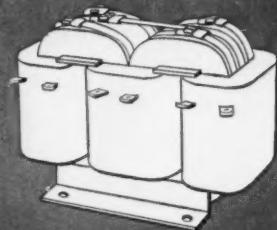
Pyr-O-Volt controller is dependable and trouble-free. Built-in voltage regulator maintains voltage within $\pm 1\%$ of level required for maximum operating stability. Thermocouple burnout protection is optional. Spare operating lamp is supplied with all instruments. Available in both horizontal and vertical case models.



MILLIVOLTMETER CONTROLLER



MAGNETIC AMPLIFIER



SATURABLE REACTOR

For your electric heating applications...

Use this accurate, dependable Pyr-O-Volt* controller

- No tubes to wear out
- Voltage regulation
- Fail-safe design
- Contactless, stepless control

Here's an accurate instrument for reliable stepless control of saturable reactors, r.f. generators and other power amplifiers. It has a proportional band adjustable from $\frac{3}{8}\%$ to 5%, and a manual reset adjustment which shifts the control point over 100% of the proportional band.

The *Pyr-O-Volt* controller can control saturable core reactors up to 100 kva, if used with a Brown magnetic amplifier. You can also use this proportional output millivoltmeter-controller with the General Electric *Reactrol***, and with the Westinghouse *Furnatron*.*** Complete packaged systems available.

Contact your nearby Honeywell field engineer for complete details. He's as near as your phone.

MINNEAPOLIS-HONEYWELL, Wayne and Windrim Avenues, Philadelphia 44, Pa.

Honeywell

• REFERENCE DATA: Specification S103-5

*Tradename, Minneapolis-Honeywell Regulator Co.

**Tradename, General Electric Co.

***Tradename, Westinghouse Electric Corp.



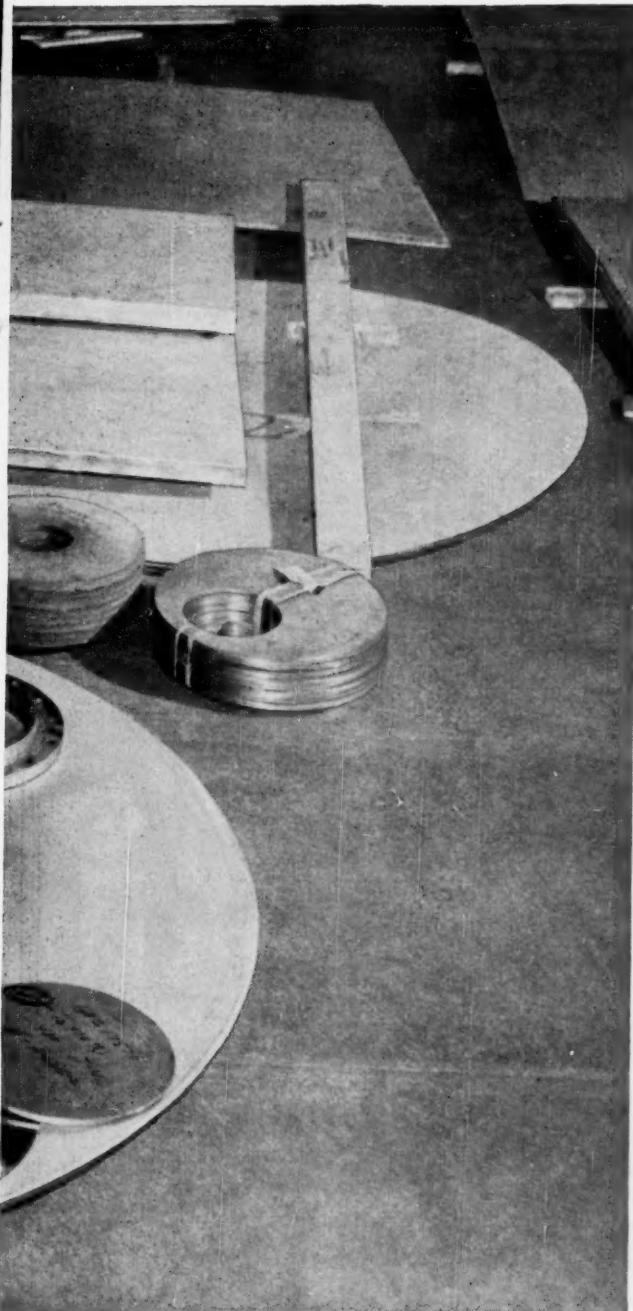
First in Control



12" x 2" Disc or 200" x 132" x 2" Plate

**... Carlson is your ONE source for ALL
stainless steel components**

STAINLESS STEEL PLATES • PLATE PRODUCTS • HEADS • RINGS



Check your drawings and you may find that you require all of the stainless steel items shown here—plates, heads, tube sheets, discs, forgings, flanges, rings, special patterns, bars, and sheets (#1 Finish) in the heavier gauges. When you buy all these material components from one source you save time, effort and money.

Your assembly costs are kept to a minimum when you use Carlson's abrasive cut material. Cleaner edges mean less true-up time on the job. There is no heat-affected zone because little heat is developed during the cutting. Fabrication is easier and the finished product is of the highest quality, more dependable in use.

Who pays freight on "offcuts" you can't use? No one, when you use Carlson's service for cutting plate to shape, ready for your fabrication. Plate is sheared, sawed, flame or abrasive cut and machined to your specifications. Eliminating freight charges on excess material lowers your costs.

There's the matter of delivery which also means time and money to you. As specialists in stainless steels, Carlson has the diversified equipment and the technical and practical knowledge to produce the plate or shapes you want, the way you want them with delivery as promised.

Stainless Steels Exclusively
CARLSON Inc.

THORNDALE, PENNSYLVANIA

District Sales Offices in Principal Cities

DISCS • FORGINGS • FLANGES • BARS AND SHEETS (No. 1 Finish)

Holiday destination-

Saturday problem:

Damaged 8,000 gallon reactor

Sunday job: Trouble-shoot and repair

Monday result: Reactor back "on-stream"

It's nine Saturday night. Home phone rings long distance. It's a Texas customer's voice: "One of our 8,000 gallon reactors was damaged. How soon can you fix it?" Answer: "Trouble-shooter leaving earliest flight." Glascote service engineer packs. Takes-off 7 a.m. Sunday. Repairs completed 10:30 that night. Monday — and he's up early. Repairs inspected. Reactor started up and back "on-stream."

Case in point: Every Glascote customer is automatically enrolled in our life-long preventive maintenance and flight-fast service programs!

Our objective: *Protecting profitability of your Glascote glass-lined equipment.* This basic protection program includes process engineering and consulting help, in-plant seminars and specialized field service.



What's behind the Glascote sales engineer . . . and his glass-lined products?

He's an experienced engineer who can give you on-the-spot product and process assistance. And behind him—38 years of Glascote experience in manufacturing glass-lined vessels and tanks for the process industries. Through continual research and development engineering, Glascote stays ahead of the demand for new and improved processes requiring a wider range of corrosion, temperature and thermal shock-resisting properties for glass linings.



Custom and Standard Reactors — Designs include the HR (Heavy-duty closed), CR (clamp-top), SR (standard closed) and the new spherical reactor. Capacities range from 300 to 8,000 gallons dependent on design.

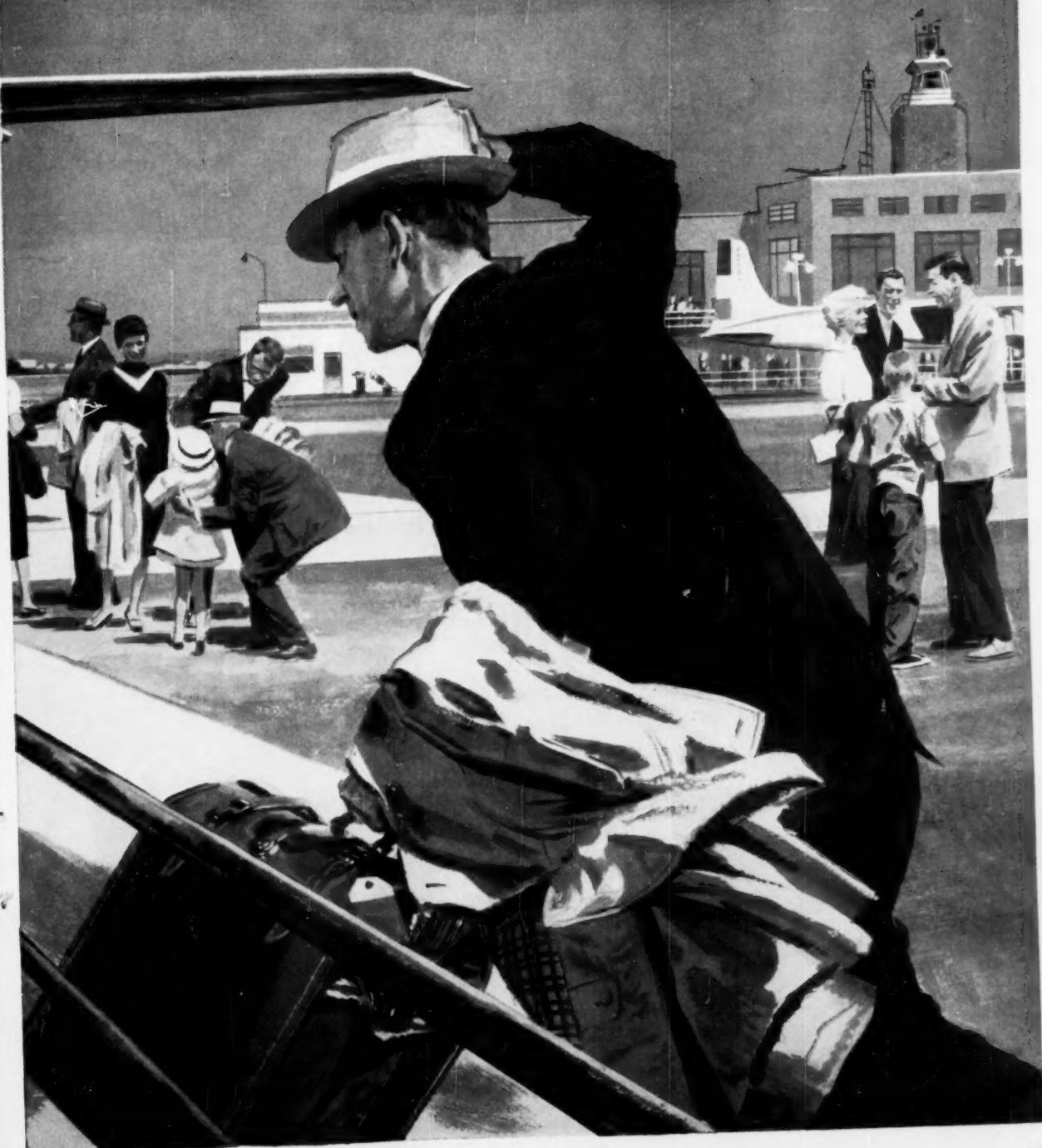
Glascote®
PRODUCTS, INC.
CLEVELAND 17, OHIO

Sales offices or agents in principal cities. Export sales:
A. O. Smith International S. A., Milwaukee 1, Wisconsin, U. S. A.

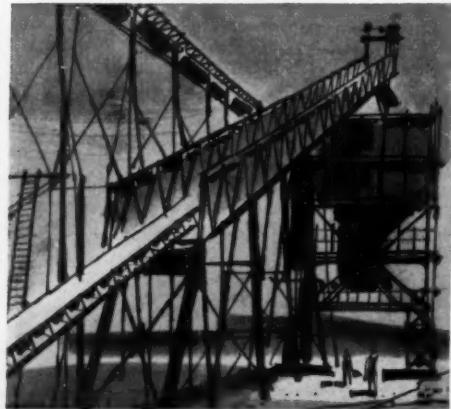
A SUBSIDIARY OF A. O. SMITH CORPORATION
World's largest manufacturer of glass-protected steel products



- a customer's plant



Wherever you use
rubber products of
neoprene or HYPALON®
you cut costs



Conveyor belts of neoprene or HYPALON often keep rolling twice as long as ordinary belts, even though exposed to chemicals and hot materials which quickly destroy ordinary rubber.

Acid hose gives longer service when it is lined with HYPALON for strong oxidizing chemicals or with neoprene for other chemicals. As covers, both resist wear and weather.



You get longer service life . . . reduced maintenance costs

... and less downtime. In chemical applications, there's a double benefit in the unique properties of Du Pont neoprene and HYPALON. Whether they are used in acid hose, conveyor belting, gasketing, tank lining or safety clothing, they do a better job and cut costs while they are doing it.

Results speak for themselves. Neoprene lining in a hot acid fumes scrubber stopped costly shutdowns during the production of critical lithium hydroxide and carbonate. In soda ash storage tanks, submerged neoprene check valves, exposed to 265°F. steam, have been used since 1955 with practically no maintenance. Neoprene—offering resistance to oil, grease, abrasion and flexing—is capable of withstanding more deteriorating influences than any other rubber.

HYPALON, a new Du Pont synthetic rubber, gives products still greater resistance in specialized conditions. For instance, HYPALON seals on an acid fume condenser have been exposed to Aqua Regia, chlorine, nitric oxide, nitrogen dioxide, and nitrogen tetroxide since 1956 without signs of deterioration. HYPALON also has excellent resistance to ozone, oxidation-aging, abrasion and high temperatures.

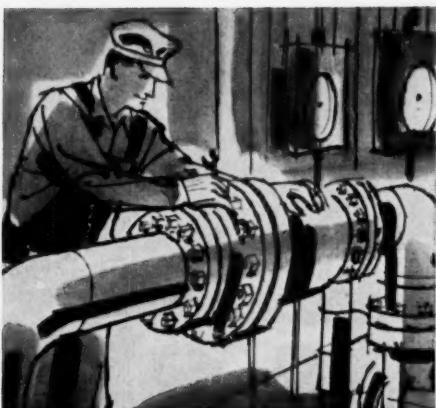
Rubber products which offer you the longer-term economy of neoprene and HYPALON are available through your local rubber goods distributor. He can suggest the right product for your applications and offer quick delivery on small or large orders. Take advantage of his convenient service by calling him soon. For more information about the properties and many industrial uses of Du Pont neoprene and HYPALON, write for *Du Pont Elastomers in Industry* to: E. I. du Pont de Nemours & Co. (Inc.), Elastomer Chemicals Dept. CE-10, Wilmington 98, Delaware.

DuPont synthetic rubbers do more things better...

NEOPRENE • HYPALON®



Better Things for Better Living . . . through Chemistry

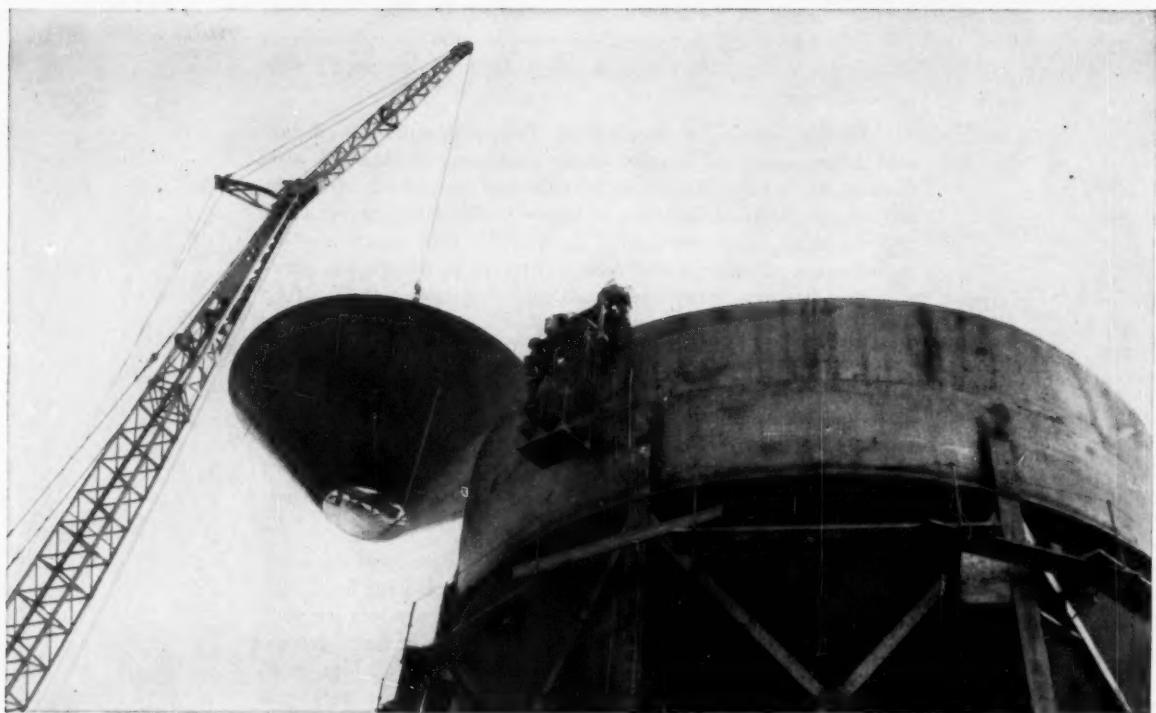


Gasketing of DuPont neoprene and HYPALON resists chemical attack and compression set . . . keeping joints tighter longer. Under extreme conditions it holds up where others fail.

Neoprene safety clothing allows freedom of movement while giving the wearer long-lasting, positive protection against chemicals and acids, and even hot oils.



Ready now at Orange, Texas



You name it . . . we'll make it . . . and erect it too!

Anything American Bridge fabricates, it can also erect. Possessing the most complete range of construction equipment in the industry and skilled personnel backed by

over 50 years of experience, we can handle any plate job anywhere. American Bridge has no peer in the specialized business of steel construction.



BIG EQUIPMENT for important jobs. The modernized plate fabricating shop is a two-aisle building, 177' wide and 750' long, with extended crane runways, 270' and 200' lengths at either end. The heavy aisle is furnished with two 50-ton, one 15-ton and one 10-ton crane and the light aisle has one 25-ton, one 15-ton and one 10-ton crane.

modern fabricating facilities for Top-quality plate work of all kinds

Tanks • Pressure Vessels • Stacks • Bins • Pipe

To better accommodate the growing needs of the dynamic industries of the South and Southwest, our Orange, Texas, plant has been completely modernized, enabling us to handle literally any type and size of plate work—including heavy wall pressure vessels for the petroleum, chemical, paper and other industries.

Plate fabricating facilities include large car bottom-heating and stress-relieving furnaces, high-capacity bending rolls, a variety of presses and press brakes, the latest in welding and X-raying equipment, high-capacity plate shears, edge planers, boring mills and drills.

The plant, strategically situated to serve the industries of the South and Southwest promptly

and economically by rail, truck or water, is also designed for fast, efficient material handling. It is equipped with 7 cranes capable of lifting over 100 tons.

American Bridge also offers complete construction service. We have the experience, manpower and equipment to handle any plate construction work efficiently and economically.

Our Orange plant is ready to serve you now. Specialists at Orange and all other American Bridge Contracting Offices around the country are prepared to discuss your plate requirements. For high-quality, economical plate work, just get in touch with the nearest office.

USS is a registered trademark

Write for our new booklet completely describing facilities and services

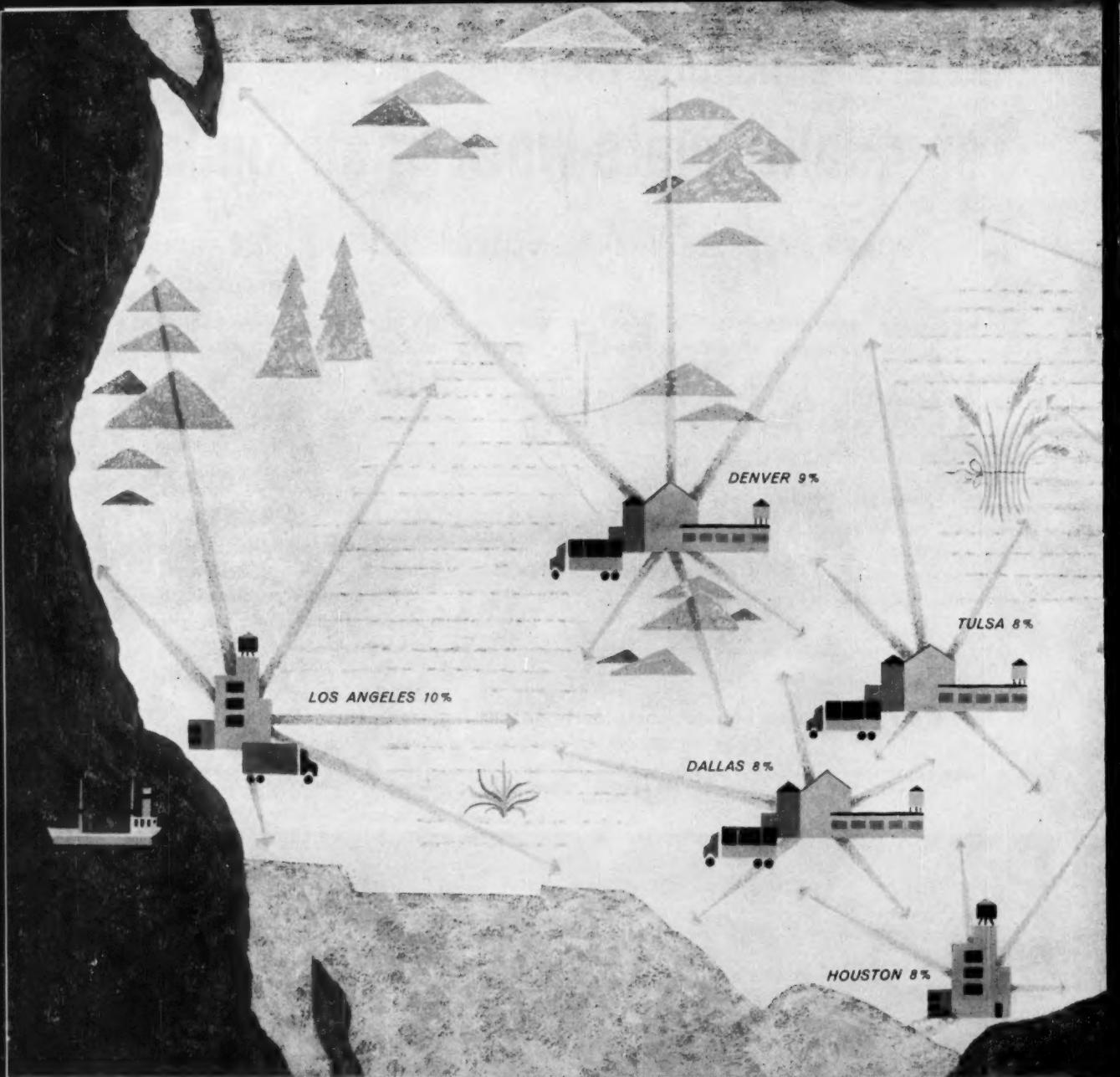
General Offices: 525 William Penn Place, Pittsburgh, Pa. Contracting Offices in: Ambridge • Atlanta • Baltimore • Birmingham • Boston • Chicago • Cincinnati • Cleveland • Dallas • Denver • Detroit • Elmira • Gary • Houston • Los Angeles • Memphis • Minneapolis • New York • Orange, Texas • Philadelphia • Pittsburgh • Portland, Ore. • Roanoke • St. Louis • San Francisco • Trenton • United States Steel Export Company, New York



**American Bridge
Division of**



United States Steel



NEW SAVINGS ON

Look at the map
to see how much
less you pay!

Refer to Chemical Engineering Catalog for Detailed
Description of Worthington Standard Pumps

Worthington has reduced the cost of SESC pumps by spanning the nation with *new regional assembly depots*. In addition to the primary depot in East Orange, (N.J.), others have been established in Cleveland, Atlanta, St. Louis, Houston and Los Angeles. Worthington can now pass along savings to you in three ways. One, on the price: as much as 10% depending upon your location. Two, on time—because your order can be processed and shipped in a matter of hours. Three, on parts service—because each of the assembly depots maintains a stock of spare parts.

In addition to assembly points, Worthington also maintains stocks of completely built pumps in Buffalo, Chicago, Denver, New Orleans, Dallas and Tulsa.

But there are other reasons why SESC (standard end



Because you pay only freight charges from the *nearest* assembly depot, Worthington pumps now cost you up to 10% less. Map shows how much you save on the total cost of a pump at each assembly depot or warehouse.

WORTHINGTON PUMPS

suction centrifugal) is far and away your best pump buy. Standardization gives you a high degree of interchangeability. Pumps may be all iron, all bronze, standard fitted, or Worthite*. 120 different sizes, with open or closed impellers are available with capacities up to 2700 GPM and heads to 550 Ft. Conventionally packed boxes or mechanical seals are optional in all pumps, and conversions from packed boxes to seals may be made on units in the field. All in all there are 70,480 modifications of the SESC pump to choose from—the broadest combination the pump industry has to offer.

SESC pumps also give you these benefits of standardization. You can cut your spare parts inventory by 50% because only four bearing frame sizes are used for the entire 120-pump line, and all pump parts are interchangeable.

This means reduced downtime if repair or conversion is made. Finally, one basic design for the complete line simplifies maintenance and lowers overall operating costs.

Take advantage of the new low costs—the speeded delivery—the many outstanding features of the Worthington SESC line now. For detailed information, write for Bulletin W-300-B-4-B, Worthington Corporation, Section 20-3, Harrison, New Jersey. In Canada: Worthington, Ltd., Brantford, Ontario.

*Worthite is a high nickel, high-chromium, low-carbon alloy steel. Trademark Reg. U. S. Pat. Off.

WORTHINGTON

Another "Quality Controlled" application of Teflon by Doré



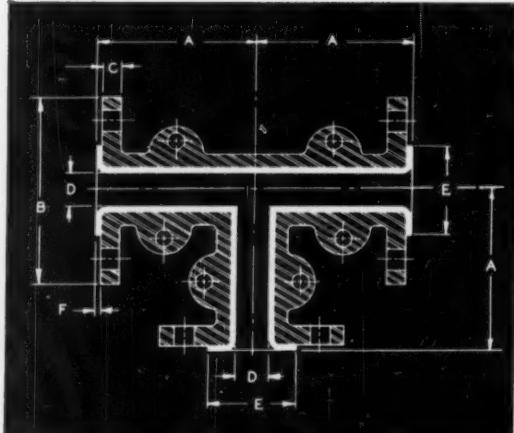
DORE' TEES LINED WITH TEFLON*

Have Standard** Face to C/L Dimensions.

This exclusive feature of Doré Teflon lined Tees means you can plan corrosion-free, contamination-proof piping layouts with the same specifications and install them with the same efficiency as you do standard piping. There are no special calculations required . . . no "off-size" fittings to complicate and upset your piping installation schedule. And only Doré Tees have these standard dimensions.

Doré Tees are lined with pure, white Teflon, 1/8" thick. The Teflon lining is tough, dense, hole-free. IT HAS NO WELDS. The Teflon lining, including the flange face seals, are molded in one piece. The seal covering the raised face of the flange is perfectly flat and smooth . . . not wavy. Flanges make up leakproof without the use of an extra flange gasket.

Doré engineered and "quality controlled" Teflon lined pipe and fittings can be the solution to corrosion and contamination problems. Write for bulletin K-57-A, giving us information about special problems you have.



Face to C/L dimensions ("A") are in accordance with ASA 125# Cast Iron Flange Fittings standards. Tees are ductile iron with flanges drilled to ASA 125# standards. Pressure Rating: 400 psi, Vacuum Rating: Full, Temperature Rating: -90°F to 500°F.

*Du Pont's registered Trademark for fluorocarbon resins, including tetrafluoroethylene resins.

**ASA 125# Cast Iron Flanged Fittings.

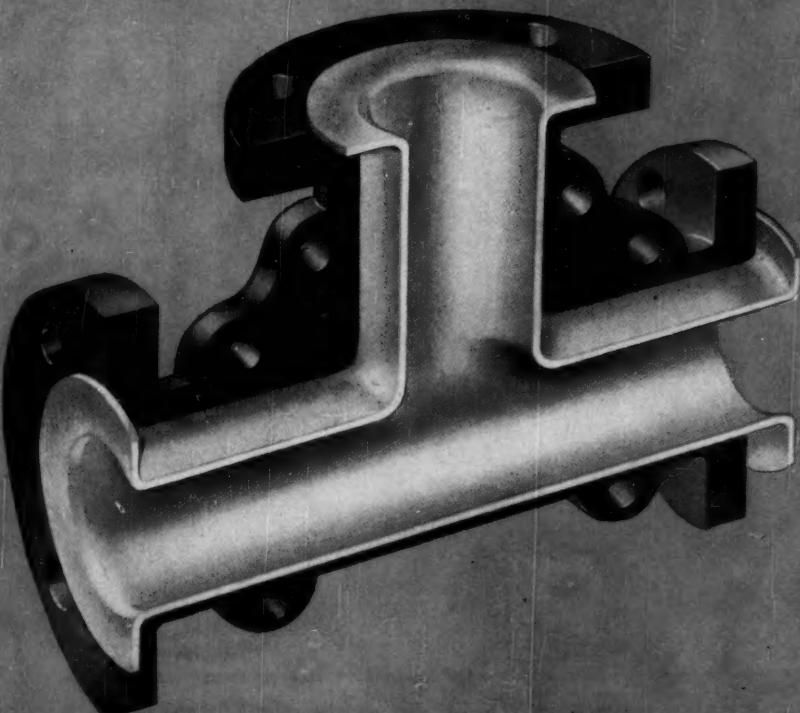
John L. Dore Co.

5406 SCHULER • P. O. BOX 7772 • HOUSTON 7, TEXAS
EXPORT: 1505 RACE ST. • PHILADELPHIA 2, PA., U. S. A.
CABLE ADDRESS: DOREX

SALES ENGINEERS
FOR JOHN L. DORE, INC.

DU PONT'S TEFLON
HI-QUALITY NYLON

It's the Inside that counts in handling corrosives...



Protect against costly breakdowns by using pipe lined with a TFE-fluorocarbon resin

In handling corrosive materials, maintenance can be a major problem. A single shutdown for pipe repair can cost you more than an entire piping installation. In corrosive services, the only pipe worth using is pipe you don't have to replace . . . pipe lined with a **TEFLON** TFE-fluorocarbon resin. This pipe is unaffected by the most powerful acids, bases, and solvents.

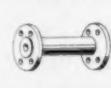
For example, pipe lined with a TFE-fluorocarbon resin replaced stainless steel pipe in a process stream containing sulfuric acid, sulfur, and sodium sulfate in water, under pressure, at a temperature of more than 240°F. Corrosion was eliminated, and, with it, the possibility of contamination with metal ions, which can often act as catalysts. The non-adhesive surface of the liner prevents plugging by the high viscosity material.

TFE-fluorocarbon pipe lining has many other advantages. It won't shatter under vibration or thermal or physical shock,

like brittle liners. It can be used at temperatures up to 500°F. The liner flared over the flanges provides complete protection for the steel from the process fluid and eliminates the need for additional gasketing. And now you can get a complete assortment of standard sizes of flanged pipe and fittings, including tees, elbows, and reducers, all lined with Du Pont **TEFLON** TFE resin.

To minimize maintenance and downtime in chemical services, install pipe lined with **TEFLON** TFE resins. Check with your local supplier for details, or, for more information, write to: **E. I. du Pont de Nemours & Co., (Inc.)** Polychemicals Department, Room 710, Du Pont Building, Wilmington 98, Delaware.

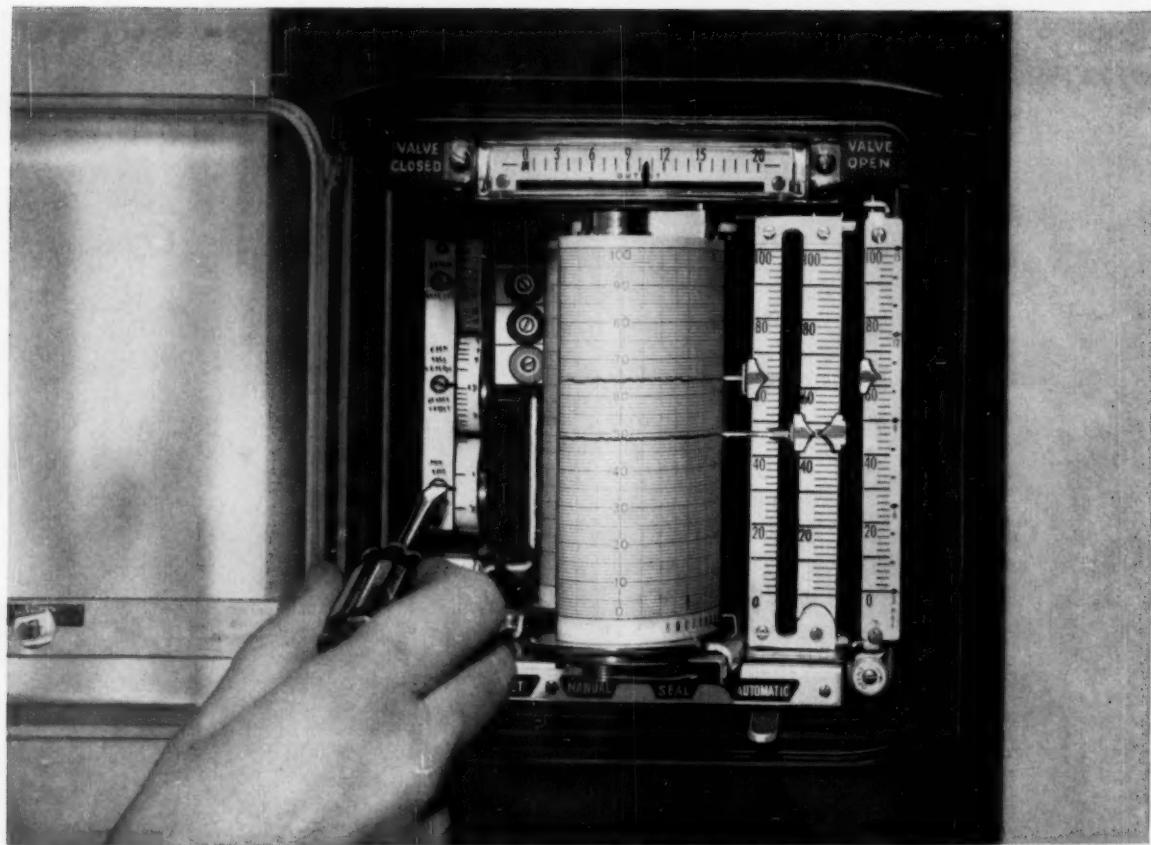
IN CANADA: Du Pont Company of Canada (1956) Limited, P. O. Box 660, Montreal, Quebec.



TEFLON[®]
TFE-FLUOROCARBON RESINS

[®] **TEFLON** is Du Pont's registered trademark for its fluorocarbon resins, including the TFE (tetrafluoroethylene) resins discussed herein.

BETTER THINGS FOR BETTER LIVING . . . THROUGH CHEMISTRY



WHY USERS ARE STANDARDIZING ON THE TAYLOR TRANSCOPE* RECORDER

Never before so many features in so little panel space!

1 All settings and adjustments made from front. Results are immediately obvious and the record is uninterrupted. Control response adjustments—when a TRANSCOPE Controller is mounted on the rear of the recorder—can be made with a screwdriver *without going behind the panel board*. Gain, reset and PRE-ACT* dials are calibrated in specific units.

This elimination of 'blind adjustments' is typical of the attention to detail that has gone into the design of the 90J series Recorders.

Also color-coded, adjustable signal-dampers (one for each recorded variable) are easy to get at, located right behind the chart drive.

2 Plug-in design. All principal assemblies are

plug-in mounted for flexibility and easy accessibility. Individual unit parts are interchangeable.

3 Left-to-right record. 4" rectilinear strip chart travels from right to left for easy reading. Gives continuous 30 day record (optional 24 hr.)—3 hour visibility. Most dependable chart drive ever devised—available in electric or pneumatic form. Pneumatic impulse twice as smooth as in conventional impulse drives.

4 Bumpless Automatic-to-Manual switching. Air leakage while switching is eliminated by an ingenious "O" ring slide valve. Selector lever travel is limited by mechanical stops, insuring positive positioning.

5 More accurate records. The Servomatic Motors give precise pen positioning. Essentially a power piston with a built-in positioner, the servomatic motor is the heart of the TRANSCOPE Recorder. Delivers 150 times more power than the conventional bellows type actuation, insure lifetime accuracy and sensitivity, a minimum of maintenance. *Servos are sensitive to changes of less than 0.1% in the pneumatic signal.*

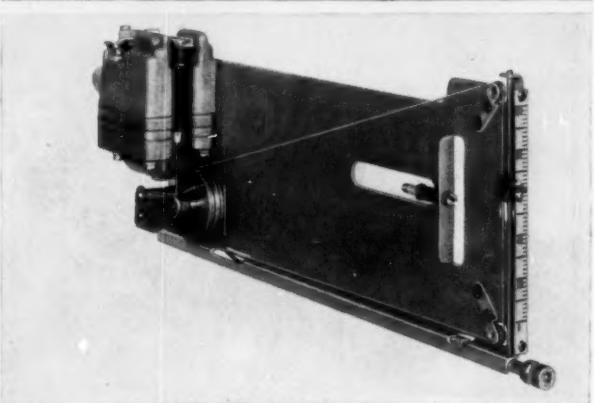
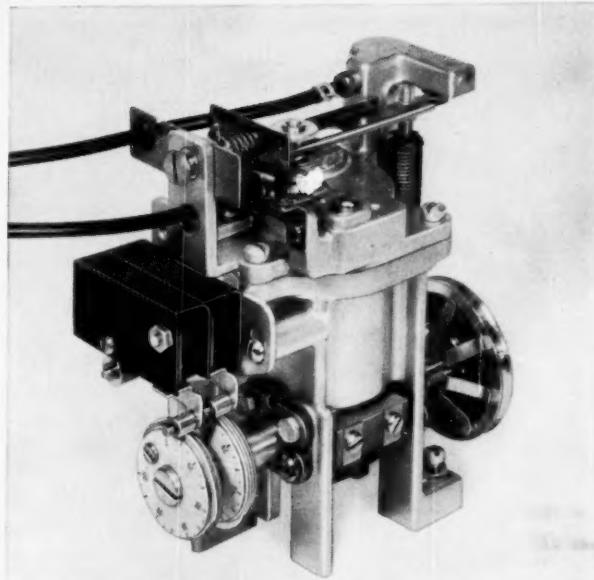
6 Process Alarms provide built-in protection. As many as six process alarms can be incorporated in one recorder housing. Attached to the servo drive shaft, they may be either electric or pneumatic. Alarms are available in various combinations and may be set for high level, low level or band.

7 A Complete Cascade System in one case. The 90J Recorder was the first to incorporate a complete cascade system in one recorder case in a 6" panel cut-out. It provides the simplest, smoothest process start-up. There are no external switches or relays. (Note unique Cascade-Balance-Set Switch.) Master and secondary variables are continuously recorded. Master and secondary controller outputs, as well as set points, are continuously indicated.

This outstanding feature of the 90J Recorder means substantial savings in instrument costs, panel space, operator's time.

8 Unique Set Point Transmitter allows continuous control. The 90J Recorder's Set Point Transmitter is a complete plug-in unit, separate from the main recording mechanism. Thus when the recorder slide is removed for checking the transmitter remains plugged into housing, keeping the process on uninterrupted, fully automatic control.

Thanks to this exclusive TRANSCOPE feature there's no need for process down time for instrument inspection or servicing.



See your Taylor Field Engineer, or write for Catalog 98286

Taylor Instrument Companies, Rochester, N. Y., or Toronto, Ontario

*Trade-Mark

Taylor Instruments MEAN ACCURACY FIRST

**FOR
MOVING
HEAT
TRANSFER
LIQUIDS...
RELY ON
"BUFFALO" HIGH
TEMPERATURE
PUMPS**

These pumps are designed especially for handling high temperature liquids. The following description will help you evaluate the suitability of these pumps for this specialized service.

In addition to these special features, "Buffalo" High Temperature Pumps bring you the famous "Buffalo" hydraulically efficient impeller and casting design. Accessibility, dependability and long, maintenance-free life are important *extra* values in every "Buffalo" Pump.

Whatever your heat transfer problem — including vapor phase — phone your "Buffalo" engineering representative for full information.

Only "Buffalo" Pumps bring you the famous "Q" Factor — the built-in **QUALITY** that provides trouble-free satisfaction and long life.

BUFFALO PUMPS

Division of Buffalo Forge Co.
501 Broadway, Buffalo, N. Y.

Canada Pumps, Ltd., Kitchener, Ont.
Sales Representatives in all
Principal Cities





Approximate
Service Limit Brand

3200°F. Castolast (Castable)

3100°F. H-W High Alumina Castable

Apache (Plastic Fire Brick)

3000°F. Chromepak (Casting Mix)

H-W Super Plastic Fire Brick

Apache G (Plastic Fire Brick with Graphite added)

2900°F. H-W Black Patch (Plastic Fire Brick)

2800°F. Harcast (Castable)

2700°F. H-W Super Castable

2600°F. H-W Lightweight Castable 2600

Harchrome (Castable)

H-W Chrome Castable

2500°F. H-W Standard Castable

H-W Periklase Castable

H-W Baffle Mix (Castable)

2400°F. H-W Extra Strength Castable

2300°F. H-W 85 Lightweight Castable

2200°F. H-W 56 Low Iron Castable

H-W 56 Lightweight Castable

1800°F. H-W 25 Lightweight Castable

1500°F. H-W Castable RC

The complete series of HARBISON-WALKER PLASTIC and CASTABLE REFRactories

can assure the proper selection for maximum life and economy

In addition to the wide range of service temperature limits as here illustrated, these monolithic refractories possess the many different combinations of physical and chemical properties needed for best protection against widely diversified destructive factors. From these brands the best balanced selection can be made for adequately withstanding the most severe operating conditions. Some examples of the many destructive influences against which maximum resistance is needed, are: corrosion by slags, fuel ash and various other fluxes; thermal shock;

disintegrating action of gases; erosion by molten metals and slags; mechanical stresses at the high working temperatures.

To help secure maximum service from these refractories, Harbison-Walker freely offers engineering service, recommendations based upon wide experience, and quality-controlled products.

HARBISON-WALKER REFRactories CO.
AND SUBSIDIARIES GENERAL OFFICES: PITTSBURGH 22, PA.
World's Most Complete Refractories Service

TYPICAL FURNACE APPLICATIONS: ARCHES • ASH PITS • BOILER SETTINGS • BREECHINGS • BURNER BLOCKS • BAFFLES • CATALYTIC REACTORS • DOOR LININGS • DUCTS AND PIPING • HEARTHS • INSULATION • KILNS AND CARS • LADLE LININGS • ROTARY KILN CHAIN SECTIONS • SOAKING PIT COVERS

SPECIALLY BUILT



for all atmospheric and hazardous conditions

Depend on *ME* for designs that assure safe, long motor life despite corrosive elements in and about chemical plants. From a complete range of chemical and explosion-proof motors, Marathon quickly supplies your needs from a single motor to power-fitting an entire plant.

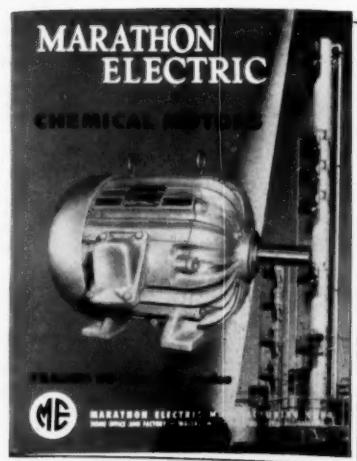
Free detailed information.

Marathon chemical motors incorporate the most recent features and improvements based on almost 50 years of motor building. For complete factual information, write for your copy of bulletin SB-185. *Marathon Electric Manufacturing Corporation, Wausau, Wisconsin.*



Motors and generators—that's our business!

Motors from 1/20 HP to 3500 HP
Generators from 1/2 KW to 2500 KW



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LESS BOILER MAINTENANCE BECAUSE A LJUNGSTROM CUTS SLAGGING

A Ljungstrom air preheater reduces slagging and cuts boiler downtime by boosting combustion air temperature, in some cases by as much as 1000°F. Whatever fuel you use, hotter combustion air makes it burn more cleanly and completely, with less slag and deposits.

More complete combustion also makes standard equipment work at top efficiency, producing more heat from less fuel. One east coast refinery saves \$129,000 a year on

their fuel bill through increased furnace efficiency. This increased efficiency contributes to an upgrading of the product by 1½ octane numbers, providing an additional annual profit of \$58,000.

How fast is "WRITE-OFF"?

Savings like these — where equipment makes a better product . . . lasts longer . . . and costs less to

maintain — can pay for a Ljungstrom air preheater *in as little as two years*. Or, if you use the higher combustion efficiency of a Ljungstrom-equipped furnace to increase throughput, write-off time can be cut to nine months!

For further information on potential fuel economy, write today for your copy of a factual article by O. F. Campbell describing one company's fuel savings with a Ljungstrom air preheater. Call or write The Air Preheater Corporation.

THE AIR PREHEATER CORPORATION

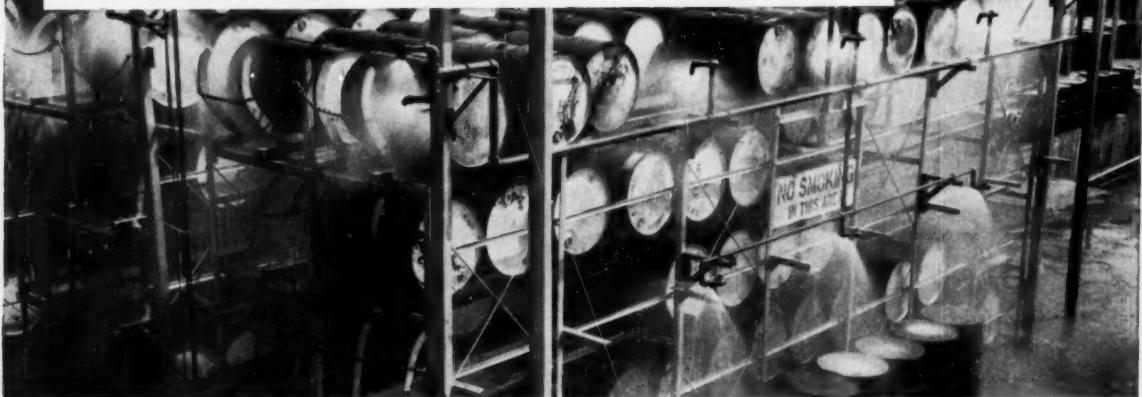
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special hazard fires need



Grinnell Special Hazard Protection



Fairly commonplace in industry today are special hazard areas, where special protection must be provided to assure against possible serious loss by fire. Grinnell, with 88 years' experience protecting against fire hazards of every description, has the most effective extinguishing agents and best systems for each type of hazard.

Remember, too, the installation of the proper Grinnell System usually serves to reduce fire insurance premiums drastically, often pays for itself in a few years!

FREE REFERENCE MANUAL! This new 44-page reference manual — "Special Hazard Fire Protection by Grinnell" — gives you a comprehensive picture of all the most advanced methods for Special Hazard fire protection. It includes explanations, applications, photographs, case histories of Grinnell systems and specialized equipment . . . and a Quick Selector Chart to help you determine the most effective system for your special fire hazard.

Write for your complimentary copy today. Grinnell Company, Inc., 277 West Exchange St., Providence, R. I.

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- Recognizing Your Special Hazards
- The Fire Triangle in Special Hazard Fire Protection
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- Research and Testing
- Sales, Engineering, Installation and Inspection Service



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WHENEVER FIRE PROTECTION IS INVOLVED

Manufacturing, Engineering, and Installation of Fire Protection Systems since 1870

IN SRE... Zallea expansion joints absorb thermal expansion of reactor core tank and outer tank

The very nature of the Sodium Reactor Experiment, conducted by Atomics International for the AEC, and the method of handling the liquid sodium reactor coolant demand reliability in expansion joints. Because of the operation there can be no compromise in design or quality.

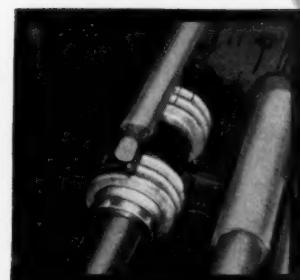
The high temperature SRE uses Zallea Expansion Joints where thermal expansion must be absorbed and where a gas seal must be maintained. An 11-ft. diameter Zallea Expansion Joint at the top of the outer tank absorbs the expansion that results from the temperature increase in these components as the reactor comes up to operating temperature, 960°F. In addition, the expansion joints form a seal for the helium gas and sodium vapor above the sodium pool at the top of the reactor as well as for the helium gas within the outer tank.

In the sodium coolant piping circuit gas seals are effected by means of Zallea Expansion Joints in the region where the pipes leave the reactor cavity and enter the pipe galleries.

Zallea has worked with almost every major engineering and manufacturing firm engaged in atomic, nuclear and missile work—and has provided the large majority of expansion joints for such projects. As a result, we have accumulated a store of expansion joint engineering data and manufacturing skills that cannot be equalled. Whenever expansion is involved in piping systems, reactors, tanks—whatever the application—let our engineers work with you. We already have the answer to many of the difficulties you will encounter. And we welcome the chance of tackling your problem.

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expansion joints

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WORLD'S FIRST COMMERCIAL SCALE SHELL PROCESS ETHYLENE OXIDE PLANT ON STREAM

**Plant for Wyandotte Chemicals Corporation
Reaches Capacity Within 2 Weeks of Start-up**

The first commercial scale plant to use the Shell Development Company's direct oxidation process for making ethylene oxide is on stream for Wyandotte Chemicals Corporation at Geismar, La.

This is the first of three ethylene oxide plants being designed, engineered and constructed by The Lummus Company, each with an annual capacity equivalent to 60,000,000 lbs. of ethylene oxide.

Most of Wyandotte's oxide will be converted by thermal hydration to ethylene glycol for industrial and antifreeze uses.

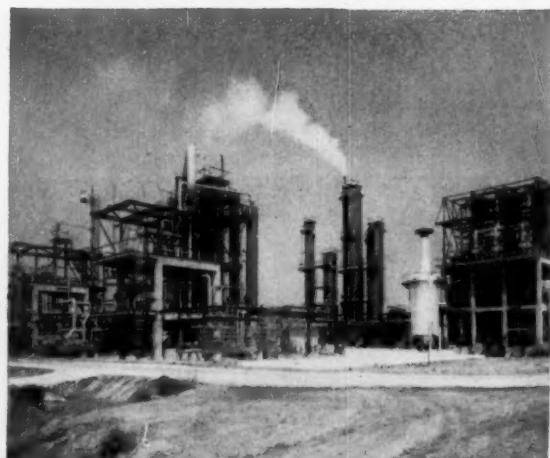
The process units at Wyandotte consist of an ethylene oxide reaction section, an ethylene oxide purification section, an ethylene glycol section and an oxygen generation section.

Non-process units provided by Lummus include: tankage and yard transfer facilities, cooling and fire-water system, an administration building, change and gate house, warehouse and shop building, and a garage and firehouse.

In the Shell Process for making ethylene oxide, ethylene is reacted with oxygen over a silver catalyst in a fixed bed reactor.

The Shell innovations which have been thoroughly tested in pilot plants offer several noteworthy advantages. Among these are high yields and virtual elimination of the waste disposal problems encountered in the chlorohydrin process. The plant uses oxygen, which requires less capital investment than the use of air.

The other two plants currently under construction by Lummus are for Calcasieu Chemical Corpora-



tion, at Lake Charles, La. and for Petrochemicals Ltd., one of the Royal Dutch Shell group of companies, at Partington, England. Both are scheduled to go on stream later this year.

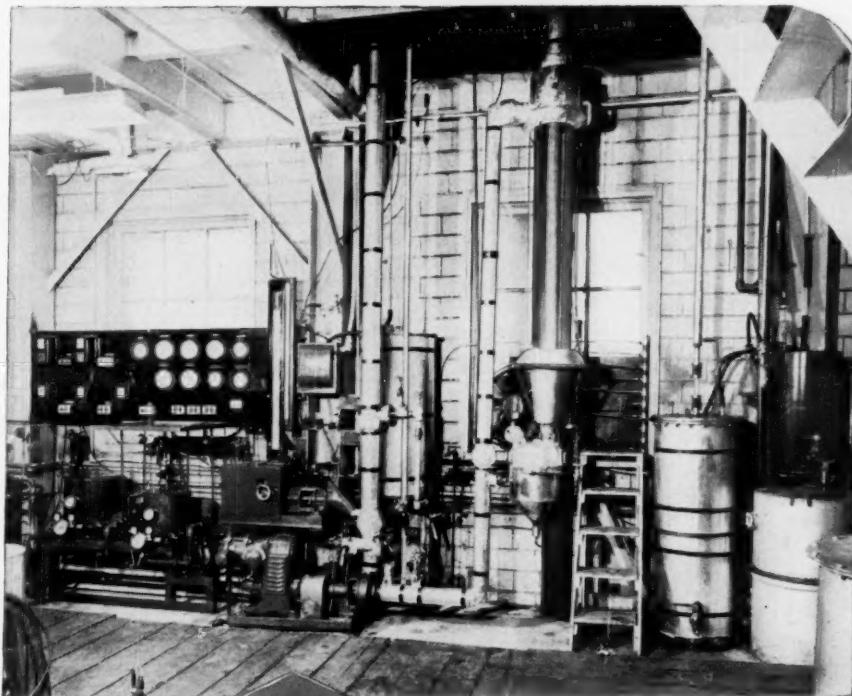
Lummus is proud of the initial performance at Wyandotte in placing the Shell Process into full scale application. These ethylene oxide plants are 3 more of the over 800 plants designed, engineered and constructed by The Lummus Company throughout the world, in the last 50 years, for the process industries. Lummus is ready to place this experience at your disposal.

THE LUMMUS COMPANY, 385 Madison Avenue, New York 17, N. Y., Houston, Chicago, Washington, D. C., Montreal, London, Paris, The Hague, Caracas, Maracaibo. *Engineering Development Center: Newark, New Jersey.*

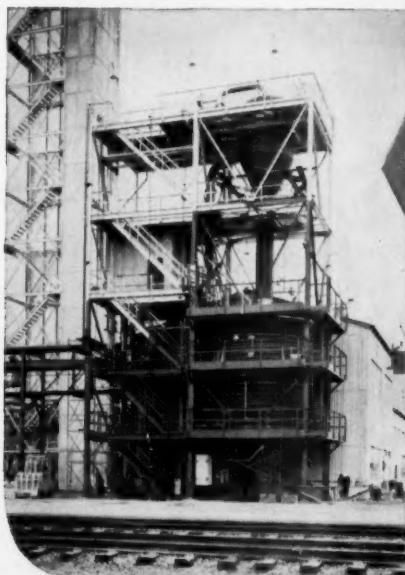
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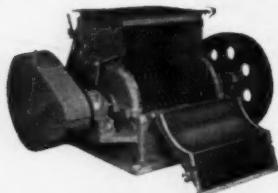
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Published in the interest of better processing by Sprout, Waldron & Co., Inc., Muncy, Penna.

PHENOLIC STOCK REDUCED IN SAW TOOTH CRUSHER

The reduction of calendered sheeting for phenolic molding compounds is being accomplished in a single pass through a heavy duty Sprout-Waldron saw tooth crusher. The warm material comes to the crusher in strips 6" to 9" wide, 12" to 18" long and in a variety of thicknesses. It is reduced to approximately $\frac{1}{4}$ " square pieces.

This precision-built heavy duty 16 x 25 Saw Tooth Crusher has been in successful operation at the

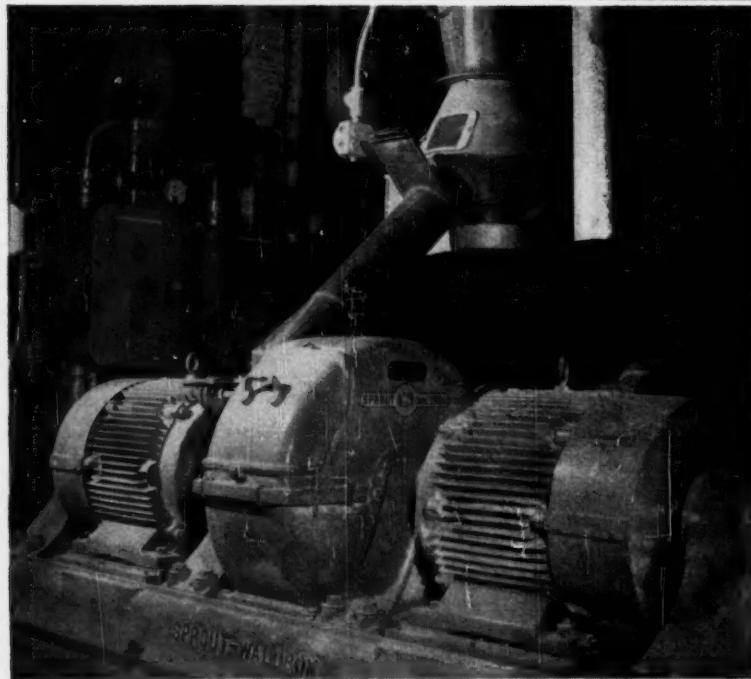


This Sprout-Waldron 16 x 25 Heavy Duty Saw Tooth Crusher has given more than 10,000 hours of satisfactory service in the crushing of phenolic stock at General Electric.

General Electric Company plant in Pittsfield, Massachusetts for over 10,000 working hours, and it is still going strong. Its hard faced 16" diameter breaker saws are designed specifically for the reduction of tough or brittle materials. In fact, everything about this crusher suggests high productivity under the most demanding conditions. Here are some of the key design points:

1. Precision-built.
2. Hinged covers to facilitate inspection or servicing.
3. Rugged construction. Alloy steel round shafts, mounted on large roller bearings.
4. Close fitting shrouds to prevent material by-passes.

For details, request Advance Specification Sheet No. 204.



STREAM SPLITTER KEEPS ATTRITION MILLS ON THE RUN

A few years ago the American Distilling Company installed a 26' Sprout-Waldron double runner attrition mill for the grinding of corn, milo, rye, barley malt and other ingredients used in the production of Bourbon Supreme Whiskey, corn and rye whiskeys and grain neutral spirits. The mill discharged into a mechanical handling system consisting of a screw conveyor and bucket elevator.

As the need for expansion became obvious it was decided to install an identical Sprout-Waldron attrition mill to operate in parallel with the existing machine, providing greater flow rate, reduced wear and simplified maintenance.

The key to the new system is a Sprout-Waldron Model VA-5 stream

splitter with two outlets which divides the flow equally between the two attrition mills. Four whole grain storage bins discharge to a common Sprout-Waldron 12" x 18' screw conveyor. The center outlet of the conveyor allows the grain to pass over a magnetic separator on the way to the stream splitter. As the ground grain emerges from the attrition mills it is conveyed to the roof of the building by a Sprout-Waldron 50 hp 44" Pneu-Vac negative pressure system to another ground grain storage bin where it is held for further processing into quality whiskeys. For the facts on the Sprout-Waldron line of precision stream splitters, ask for Bulletin 137-B.

CP/106

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Lubriflush***

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Today's greases have different chemical bases—lithium, sodium, calcium, barium, and other bases which your people can't be expected to keep track of. Some of these greases will not mix safely with others. Because certain chemical bases may react with each other, mixed grease may change its characteristics and become unsuitable for bearing lubrication. That is why U.S. LUBRIFLUSH—an exclusive feature

of U.S. Motors—is so important. With this transverse lubrication system, old grease is completely flushed out as new grease is forced in. There's no mixing. New grease can be put in without bothering to determine whether it's basically compatible with the old. LUBRIFLUSH, moreover, assures proper lubrication for longest bearing life. Another good reason to specify: "U.S. ELECTRICAL MOTORS."

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BRIEFS

on chlorination and sulfonation...
what to look for in muriatic specs...
a free booklet on trichlorethylene



Selective chlorination and sulfonation

It's easy to do some profitable processing tricks with Hooker sulfuryl chloride.

A simple change in temperature or in catalysts or in the proportion of reactants you use can have profound effects on the end product.

React sulfuryl chloride with the sodium salts of organic acids, for example, and you can vary the process to produce either the acid chlorides or anhydrides.

You can use sulfuryl chloride to chlorinate and sulfonate both the aromatic compounds and the aliphatic hydrocarbons and their derivatives.

What else recommends our product? It's 99% pure. It gives off much less heat during chlorination than elemental chlorine. You need relatively simple and inexpensive equipment to work with it. It has no flash or fire point.

For the rest of the story, we suggest you send the coupon for a technical data sheet and copies of Bulletin 330, *Sulfuryl Chloride in Organic Chemistry*, and Bulletin 328A, *Chlorinating Agents*. This last also gives information on our other chlorinating agents, chlorine, sulfur chlorides, thionyl chloride, muriatic acid, etc.



What to look for in muriatic acid specs

This white gummy substance is an insoluble precipitate which can form in certain reactions with muriatic acid that contains too much sulfate.

Iron, arsenic, and free chlorine can also give a process indigestion when their level in a muriatic acid is too high.

So it pays to consider these carefully when you examine any muriatic's specs.

Take Hooker White Grade muriatic, for example. Iron: a mere 0.0001% at the most. Sulfates: less than 0.003%. Free chlorine: none. Arsenic: none.

Very often your process can stand a

little higher level on these impurities. Hooker Commercial Grade offers these maximum specs: Iron: a low 0.0005%. Sulfates: 0.003%. Free chlorine: a slight trace. Arsenic: none.

Both grades come in rubber-lined tank cars. Both come in three strengths: 18°, 20°, and 22° Baumé. For more technical data, check coupon.

Free booklet on trichlorethylene

Here, in forty pages, is a wealth of material on trichlorethylene. Includes physical and chemical properties, shipping containers, handling methods, etc.

It gives complete data on all three grades of Nialk® trichlorethylene which are of interest to chemical processors:

Technical Grade Maximum acidity as HCl is 0.0005%. Alkalinity as NaOH is 0.001% at the most. This grade boils at 86.6 to 87.8°C under atmospheric pressure. On evaporation at 100°C the maximum residue is 0.005%.



Technical grade is often used as a freezing point depressant, particularly in carbon tetrachloride fire extinguishers and as a solvent in various adhesive formulations.

Extraction Grade No HCl acidity. NaOH alkalinity runs from 0.006 to 0.008%. This grade will boil between 86.6 and 87.4°C under atmospheric pressure. Used mostly for extracting fats from animal matter, and oil from raw wool, cottonseed, and flaxseed.

X-1 Special Grade This grade was developed especially for processes calling for an unusually pure product.

To get the booklet check Bulletin No. 44 on the coupon. For a résumé of important facts check Trichlorethylene on the coupon.

For more information, check coupon and mail with your name, title, and company address.

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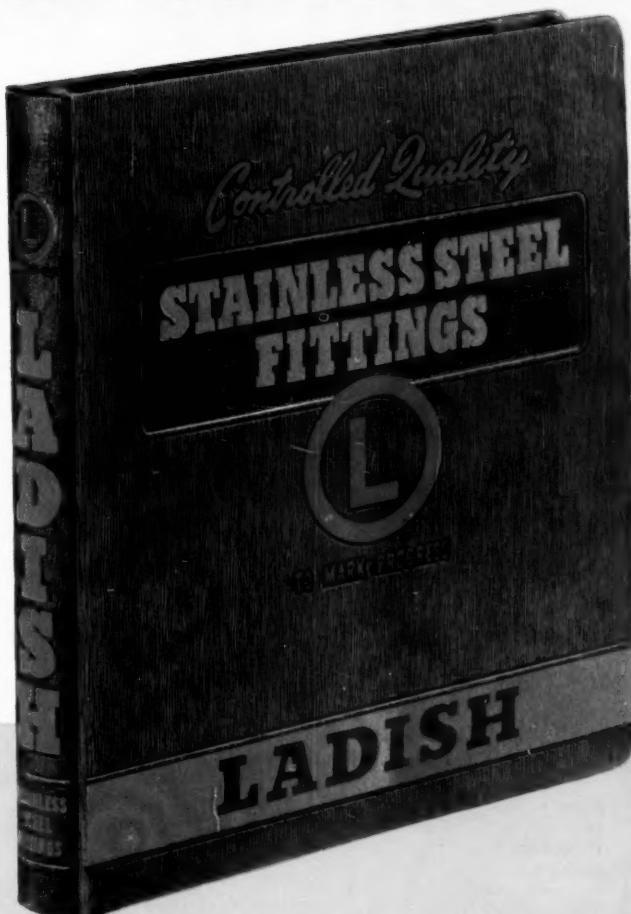
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How to beat the high cost of temperature control

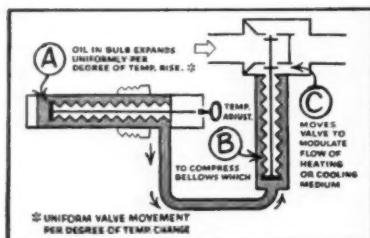
The practical approach to temperature control

By John W. Ritter, Test Engineer,
SARCO Company, Inc.

Precise temperature regulation is essential in many processing operations, not only for quality control, but for maintenance of output as well.

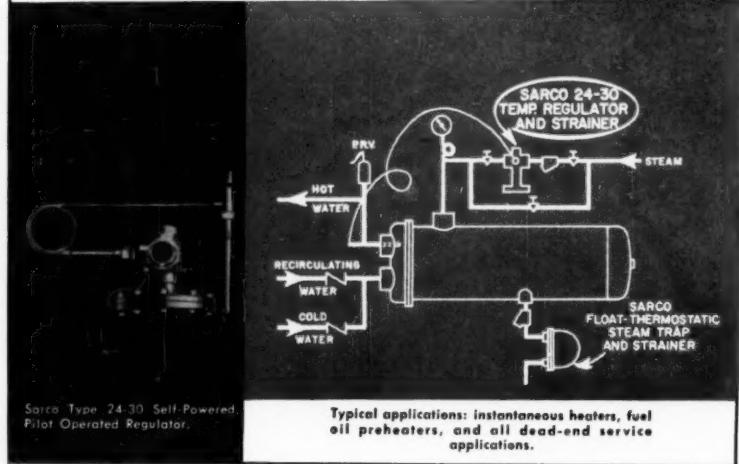
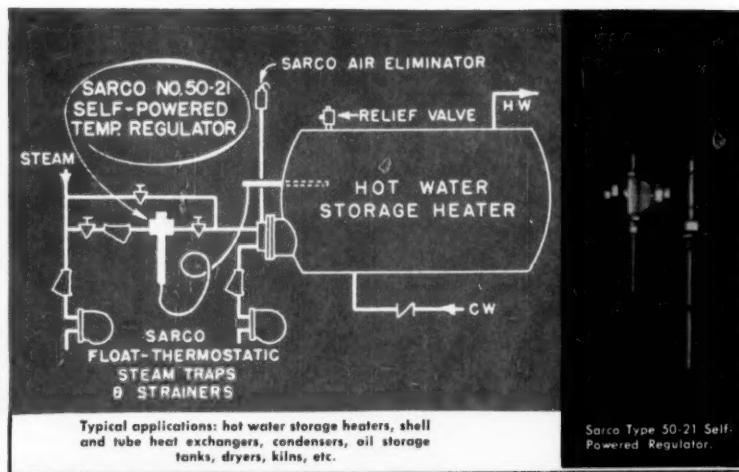
Manual temperature control is unsatisfactory because of the possibility of spoilage and loss of quality control which can result from irregular or indifferent hand regulation.

Automatic controls are available in a wide variety, including pneumatic, electronic, and self-powered. Pneumatic and electronic controls are relatively expensive to purchase and install, and may require frequent maintenance. However, in most applications, control requirements can be achieved very successfully by the use of relatively simple, economical Sarco Self-powered Regulators.



This drawing shows simplicity of operation of the Sarco 50-21 Temperature Regulator, which consists of a thermostat, capillary tubing, and a valve.

Sarco controls, like the 50-21 and the 24-30, have the required degree of sensitivity and dependability, combined with the ruggedness inherent in the sealed capillary tube construction. Because these Sarco controls do not depend on external power, such as electricity or compressed air, they have established long records of sustained, reliable operation. They are an economical and practical solution to the problem of maintaining continuous watchdog duty over processing temperatures.



Self-powered automatic temperature regulators by SARCO ...

have these 5 marked advantages: No compressed air or electrical wiring required. No delicate mechanisms to adjust or maintain. No packing glands to stick or require maintenance. No shutdown during power failure. No specialized maintenance required.

Sarco Self-Powered Controls are self-contained and can be installed by any pipe fitter. They are so reasonable in cost that you can afford Sarco automatic heating controls for every application in your plant. Write for 10-page Sarco Control Bulletin No. 620.

6346-B

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DEVELOPMENTS . . .

OCTOBER 6, 1958

Chementator

C. H. CHILTON

New iodine process is now on stream for Dow at Inglewood, Calif. Process uses ion exchange to recover iodine from oil-well brines.

Conveyor system carrying 1,000 tons/hr. of quarried rock over a distance of 5½ mi. to Ideal Cement Co.'s plant at Ada, Okla., will include world's longest individual span, says Link-Belt Co. Longest of seven spans will cover 11,920 ft., using a single 36-in.-wide rubber belt more than 4½ mi. long.

Several U. S. firms are dickering with Knapsack-Griesheim for use of the Hoechst subsidiary's new acrylonitrile process. The German process reacts HCN with acetaldehyde instead of acetylene, is said to get 10-15% better yields.

Rich air stimulates catalytic cracker

Oxygen enrichment of regeneration air has been shown in plant-scale tests this summer to permit a 15% increase in capacity of a nine-year-old fluid catalytic cracking unit.

Tests were conducted jointly by Linde Co. and Cities Service Oil Co. on a 22,500-bbl./day cat cracker at Cities Service's East Chicago refinery over a five-day period. Most of the test data were collected while using an oxygen enrichment rate of 100 tons/day, giving a final oxygen content in the regeneration air of 25.4%.

Optimum degree of air enrichment can't be determined exactly on the basis of this test, says Cities Service. However, the refinery is satisfied with test results so far and is going to continue testing for further evaluations.

A Cities Service spokesman told *CE* that other advantages of oxygen enrichment, in addition to greater regeneration capacity, might make it attractive even in new cracking units. For example, coke burning, which is ordinarily touchy, can be controlled better when using enriched air.

Oxygen for the tests came via liquid-carrying truck from Linde's East Chicago oxygen plant.

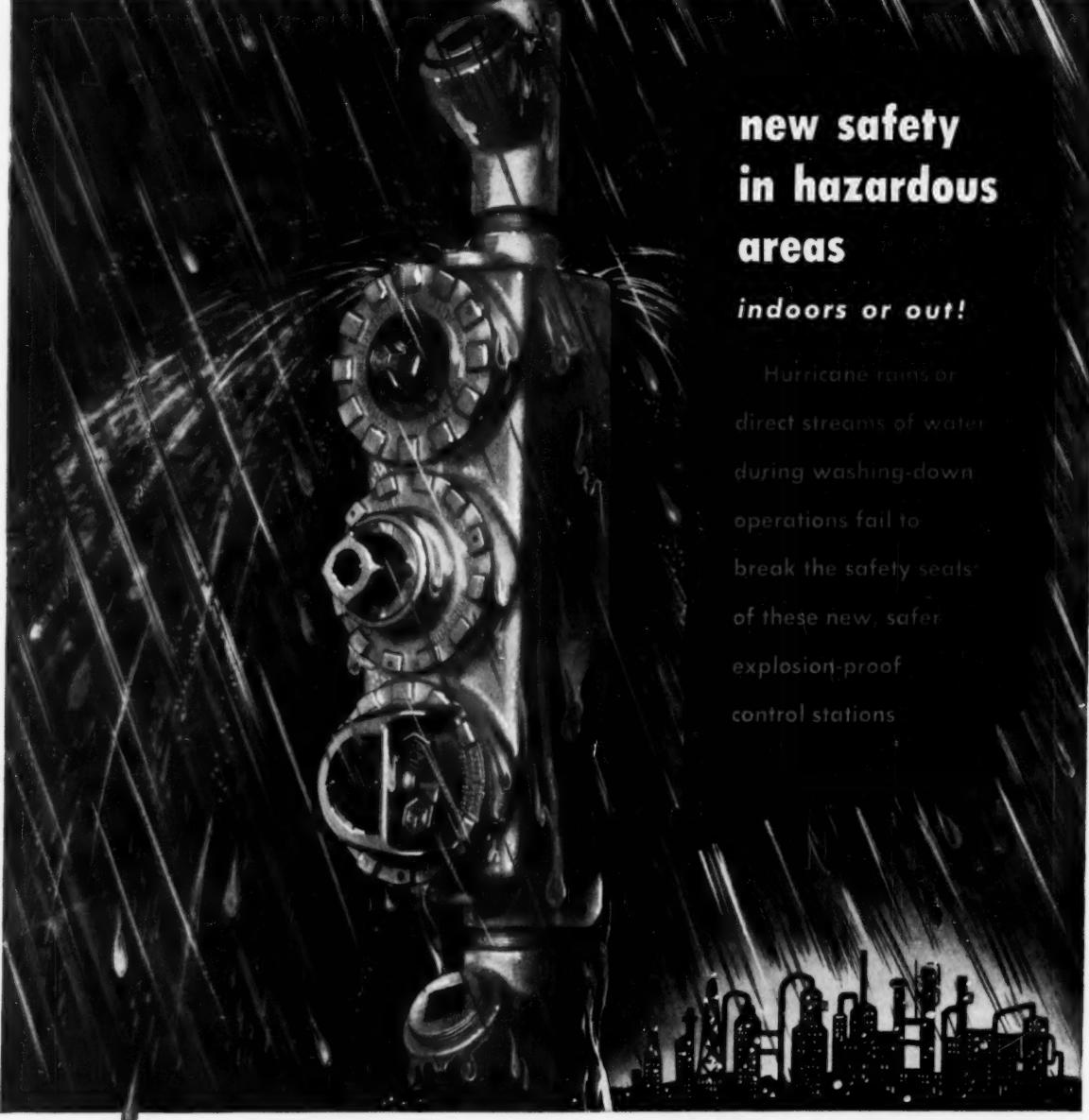
(For a description of a modern cat cracker using conventional air regeneration, see Process Flowsheet, pp. 120-123, this issue.)

New device sprays solventless epoxies

Spray application of solvent-free epoxy resin formulations is now possible with equipment being developed by Hodges Chemicals Co., Redwood City, Calif. The new machine "can accurately proportion the solventless resin with catalyst and produce a continuous film," asserts President Bill Hodges.

Right now, Hodges is doing spray application work only in the local West Coast area. Ultimate plans—still some months from realization—are to license the machine widely and

(Continued on page 45)



new safety in hazardous areas

indoors or out!

Hurricane rains or
direct streams of water
during washing-down
operations fail to
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Explosion-proof, dust-ignition-proof, weather resistant and water-tight (NEMA 4), this new Condulet® EWC series affords safety greater than ever before for pilot lights, heavy-duty push-button stations, selector

switches, or various combinations thereof in single, double or triple gangs.

Designed expressly for Class I (Groups C and D) and Class II hazardous areas, the new series features a Feraloy® housing with *threaded* cover and *threaded* operating-shafts throughout. Cover, shaft housing and pilot light jewels are tightly sealed with Neoprene O-rings, effectively shutting out fumes, dusts, all water.

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Crouse-Hinds Company of Canada, Ltd., Toronto, Ont.

Crouse-Hinds Instrument Company, Inc., Silver Spring, Maryland

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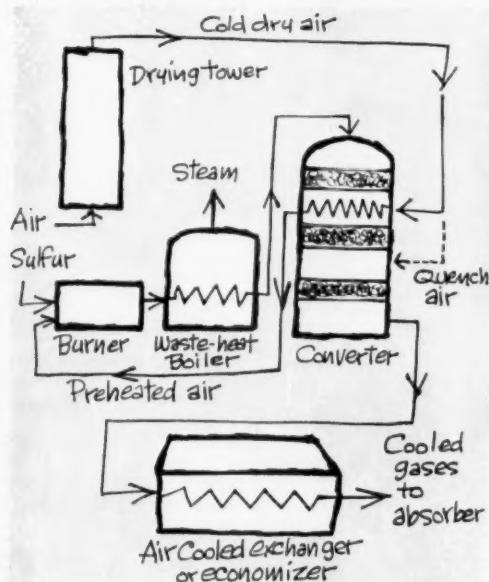
These products are sold exclusively through electrical distributors. For application engineering help, contact one of the following offices: Baton Rouge Birmingham Boston Buffalo Chicago Cincinnati Cleveland Corpus Christi Dallas Denver Detroit Houston Indianapolis Kansas City Los Angeles Milwaukee New Orleans New York Omaha Philadelphia Pittsburgh Portland, Ore. Salt Lake City St. Louis St. Paul San Francisco Seattle Tulsa Washington Jacksonville Reading, Pa. Richmond, Va.

to provide licensees with proper formulations for specific jobs.

Thickness of coating depends on service conditions. For example, on concrete floors, Hodges applies a wear-resistant epoxy coating 30-50 mils thick; chemically resistant epoxy tank linings are on the order of 10-20 mils.

Advantages of solvent-free application: Reduced fire hazard during application; elimination of the pinholing sometimes caused by solvent release; thicker coatings per pass of spray gun, permitted by high (100%) solids content.

New look in small sulfuric acid plants



As much as 20% reduction in cost of moderate-size contact-process sulfuric acid plants is claimed by D. M. Weatherly Co., Atlanta engineering firm with a successful record in building fertilizer plants (*Chem. Eng.*, Aug. 1956, pp. 128-132).

Weatherly compares its price of \$350,000 for a typical 100-ton/day acid plant with an estimated \$450,000 for a conventional plant built by old-line engineering firms.

Part of the lower cost is due to the novel system of heat transfer shown in the flow-sheet. Weatherly uses cold air, instead of hot combustion gases, for removing heat from converter gases. The much greater available temperature difference results in a two-thirds reduction in required heat-transfer surface. Along with other changes in drying and

absorption, the new flowsheet permits a simple plant layout, with further savings in cost.

Weatherly got into the acid plant business last year by building a conventional 80-ton contact unit for Southwestern Agrochemical Corp., Chandler, Ariz. Two potential customers for the new flowsheet are now on the string.

Joint approach to pollution problems

Chemical producers along the Houston Ship Channel—some 15 of them—are studying a proposal for a jointly supported pipeline and plant which would treat all their process wastes. Such a measure would get the companies off the hook with local and federal authorities who are bringing court action against some of them accused of water pollution.

Idea is being pushed by Fish Service Corp., Houston engineering firm. Fish would build the pipeline and disposal plant. Plant would be operated by a private concern, with operating costs charged to the chemical producers on a volume basis. To finance construction costs, the operating company might put up one-third of the equity, and the chemical companies would cover the other two-thirds.

Initial plant capacity would be 20,000 gpm. of wastes. Any and all effluents containing not more than 30% by volume of suspended solids will be handled. Processes being considered include flotation, aeration, sedimentation and chemical flocculation. No chemical recovery is planned.

While the project right now is concerned only with chemical producers, it is not necessarily limited to chemical plant wastes. However, no sanitary sewage will be accepted.

Advantages of joint disposal are readily apparent. One large treatment plant would be cheaper to build and operate than many individual small units. And the over-all treatment job would no doubt be easier because of the beneficial effects of combining dissimilar waste streams.

Copper: Next big "chemical" metal

Chemetals Corp.'s process for chemically converting copper scrap to powder is poised on the threshold of a doorway which could open up a new field of chemical metallurgy.

(Continued on page 48)

Aluminum

Union Oil's heat exchangers with aluminum and steel shells, placed in service in January, 1958. The aluminum shell and tubes are still in service under conditions which destroyed the steel in 30 days. Shell side handles 85% steam, 9% cyanide, 4% hydrogen sulfide, 2% water at 260°-280° F. Tube side carries Marley cooling tower water.

The Finest Products
Made with Aluminum

are made with
REYNOLDS ALUMINUM

Heat Exchangers Last Longer...

up to 7 times longer for Union Oil

Union Oil Company of California is converting several of its shell and tube heat exchangers—and parts of these exchangers—to Reynolds Aluminum. Main reason: aluminum lasts longer in many heat exchanger applications, up to 7 times longer.

For example, in Union's heat exchangers which handle waste water from a refinery cat tower, steel condenser tubes lasted only a few weeks before corrosion made them useless. Aluminum tubes, now in the same service, last 7 times as long handling the same corrosive fluids.

In the same application, steel tube sheet and baffles lasted about 5 months before they had to be replaced. Union engineers replaced these with aluminum and installed aluminum bundles in January, 1957. They are still in service.

The bare tubes of Union's heat exchangers are Reynolds Aluminum alloy 3003-H14, and the tube sheets and baffles are 6061-T6.

Union Oil's aluminum heat exchangers

really save in service cost. On a dollars per square foot of heat transfer area per year base, aluminum units are nearly *5 times lower in cost* than the same units with seamless mild steel. This does not include handling costs, which favor lightweight aluminum.

Initial cost, incidentally, is virtually the same for aluminum and steel in these uses.

Heat exchangers are just one of many places Reynolds Aluminum is cutting costs in this industry. Its resistance to corrosion, its passivity, light weight and strength make aluminum the logical material for tanks, vessels, jacketing, piping, tubing, and other applications where corrosives must be handled or stored.

To learn how aluminum can cut your costs, write the people who know aluminum and its uses in the chemical and petroleum industry—*Reynolds Metals Company, P.O. Box 2346-CJ, Richmond 18, Virginia*. Or contact your local Reynolds branch office, listed under "Aluminum" in the classified phone book.



Write today for Reynolds free bulletins—
"Aluminum for Heat Exchangers" and "Keys to Corrosion".

REYNOLDS ALUMINUM

This doorway is the recent development by E. W. Bliss Co., Canton, Ohio, of process and machinery for converting copper powder into strip. Up to now, commercial exploitation of the Chemetals process for copper was limited by the relatively small market for copper powder.

Riding herd on this development is Fluor Corp. The Los Angeles engineering firm completed design work this summer on a 50-ton/day copper powder and strip plant proposed for a Midwest location. A major copper producer is now considering installing the \$10-million plant.

The Chemetals process involves ammonia leaching of copper scrap (e.g., automobile radiators), followed by hydrogen reduction to the metal powder in autoclaves designed to operate at 375 F. and 1,200 psi. Powder will be roll-compacted into strip, continuously sintered at 50-100 F. below its melting point under a hydrogen atmosphere, then finished into specification-grade strip by rolling and annealing. Hydrogen will be made by the steam-iron route.

Fluor is leading from a position of technological strength. The firm for the past two years has been running a semicommercial plant using this process, a 7½-ton/day unit at Kansas City, Mo., owned by Whitaker Metals Corp. Fluor took over operation when the plant ran into difficulties.

A major windfall to process economics came recently when Fluor put into use at Kansas City an unidentified chemical additive discovered by Sherritt Gordon Mines, who operates a similar process to produce nickel (see Process Flowsheet, Jan. 1957, pp. 194-197). This additive boosted once-through yield of copper powder in the reduction step from 80% to virtually 100%.

Ammonia synthesis gas via LTC char

South Africa, site of the big Fischer-Tropsch oil-from-coal plant, will supply chemical engineers with a new conversation piece next year.

Subject: African Explosives & Chemical Industries' \$28-million ammonia-urea project at Modderfontein. Items of particular chemical engineering interest:

- Low-temperature carbonization of low-grade coal in two Lurgi vertical units.
- Continuous oxygen-steam gasification of LTC char, instead of cyclic gasification of

metallurgical coke in semi-water gas generators. (Several years ago Du Pont tried oxygen-steam gasification of coke at Belle, W. Va.; see *Chem. Eng.*, Oct. 1950, pp. 237-238.)

- Use of Kittel plates (see *Chem. Eng.*, Apr. 1953, pp. 242-243) instead of ring packing in the water scrubbing towers which remove CO₂ from the synthesis gas.

The AECI project is an expansion and modernization of an existing ammonia plant with a capacity of 75,000 tons/yr. Ammonia capacity will be boosted to 145,000 tons, and a 110,000-ton urea plant will be added. Project will include a 310-ton/day oxygen plant.

In line with today's thinking in U. S. and Europe (*Chemementator*, Jan. 27, 1958, p. 53), AECI is negotiating with a petroleum refiner for sale of the 20 tons/day of oil produced when carbonizing 900 tons/day of coal.

AECI is not yet certain whether LTC char can be used with the one set of cyclic water gas generators which will continue to operate. As soon as char supplies are available, plant-scale trials will be conducted.

Are secrecy contracts monopolistic?

Monsanto's right to preserve its trade secrets by means of employment contracts—a right recently upheld in Salt Lake City District Court (*Chemementator*, June 2, p. 43; Aug. 25, p. 51)—is being challenged in another court.

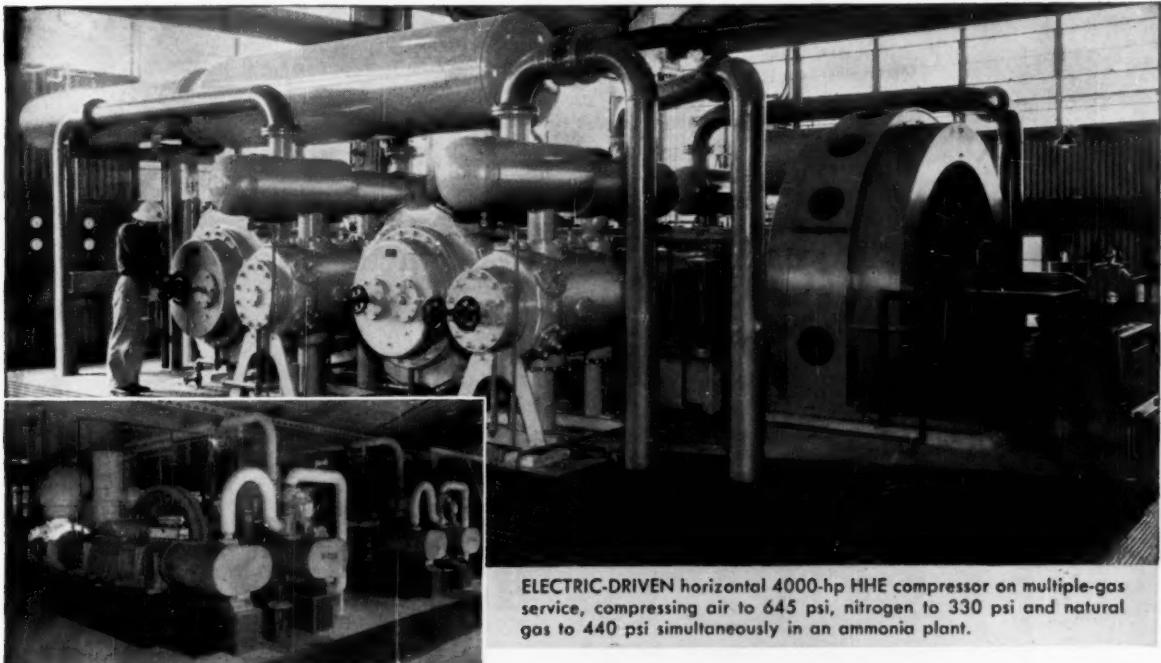
Central Farmers Fertilizer Co., defendant in a pending suit brought by Monsanto in District Court at Pocatello, Idaho, filed counter-claim on Sept. 16 in District Court at Boise.

CFFC alleges that, in making employees sign contracts not to divulge trade secrets, Monsanto has a "scheme to create a monopoly in the manufacture of elemental phosphorus." The claim also alleges that Monsanto by its lawsuits has "frustrated, retarded, injured and damaged" CFFC in its building of a phosphorus plant at Georgetown, Idaho.

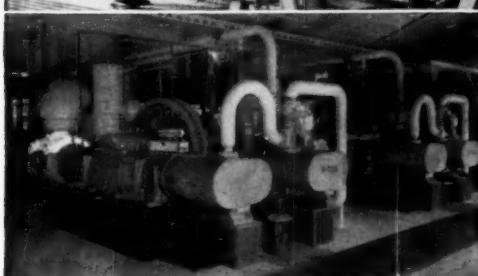
CFFC was not a defendant in the Salt Lake City trial. In that action, Monsanto obtained an injunction against former employee Charles M. Miller, restraining him from using Monsanto trade secrets in connection with CFFC's or any other phosphorus furnace.

In its charges of monopoly, CFFC is apparently taking its cue from the government's antitrust suit against Pfizer (*Chemementator*, June 30, p. 47), which alleges that Pfizer's employment contracts protecting citric acid trade secrets are monopolistic.

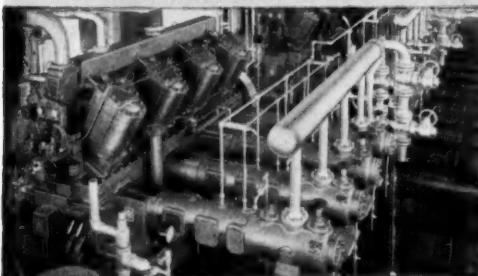
what assures a GOOD COMPRESSOR for PROCESS WORK?



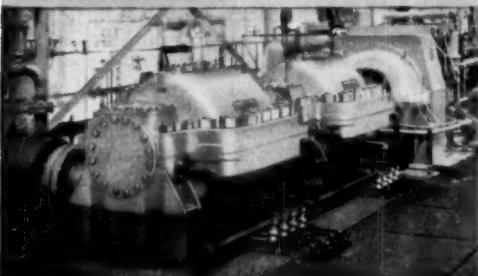
ELECTRIC-DRIVEN horizontal 4000-hp HHE compressor on multiple-gas service, compressing air to 645 psi, nitrogen to 330 psi and natural gas to 440 psi simultaneously in an ammonia plant.



STEAM-DRIVEN compressors with non-lubricated cylinders handling hydrogen chloride gas at 54 degrees below zero.



GAS-ENGINE compressors with non-lubricated compressor cylinders on hydrogen recycling duty at a Southern refinery.



CENTRIFUGAL compressors on ethylene refrigeration; these are tandem units driven by steam turbine.

In process jobs, any interruption of the cycle often means large loss of production, expensive repairs, and introduction of hazardous conditions. In manufacturing compressors for these jobs, there is one ingredient most vital.

That ingredient is knowledge. The compressor manufacturer must know how to predict conditions in the process which might force a shutdown, and must know how to meet those conditions with a compressor which will minimize the possibility of a shutdown.

Such knowledge is obtained only through years of actual experience in designing, building and applying compressors for all sorts of processes, for handling all kinds of gases, and for any range of pressures.

Ingersoll-Rand has more of that kind of experience than any other compressor builder. For information on process compressors for pressures up to 35,000 psi, contact your I-R representative or write direct. Ask for your copy of Form 3132A.

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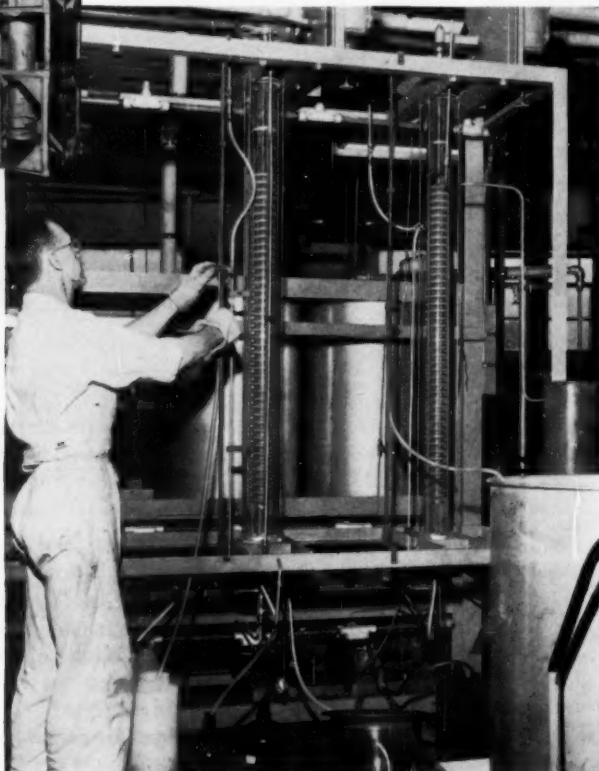
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DEVELOPMENTS . . .

PROCESSES & TECHNOLOGY C. S. CRONAN

FEED comes from nuclear-fuel fabrication via "non-critical" containers.

PRODUCT owes its purity to solvent extraction and stripping.



Valued at \$2,500/lb., nuclear fuel scrap forces reprocessor to operate tight system to show high recovery and profit.

Reprocessor Wrings Profit From Cold Scrap

There's money in "cold" uranium scrap,* despite recent general feeling among private companies that reprocessing fails to return adequate profits. So reports Irvington-Baker Refining Div. of Engelhard Industries about its reprocessing plant at Newark, N. J.

First to enter the field of privately financed scrap reprocessing, Irvington-Baker's \$200,000 capital investment in reprocessing facilities has returned

adequate profits during 18-months' operation under license from the Atomic Energy Commission.

► **To Profit: Take Any Scrap**—Key to plant's economic success is process flexibility: Plant can handle almost any form of cold uranium scrap (most facilities are limited to a single type).

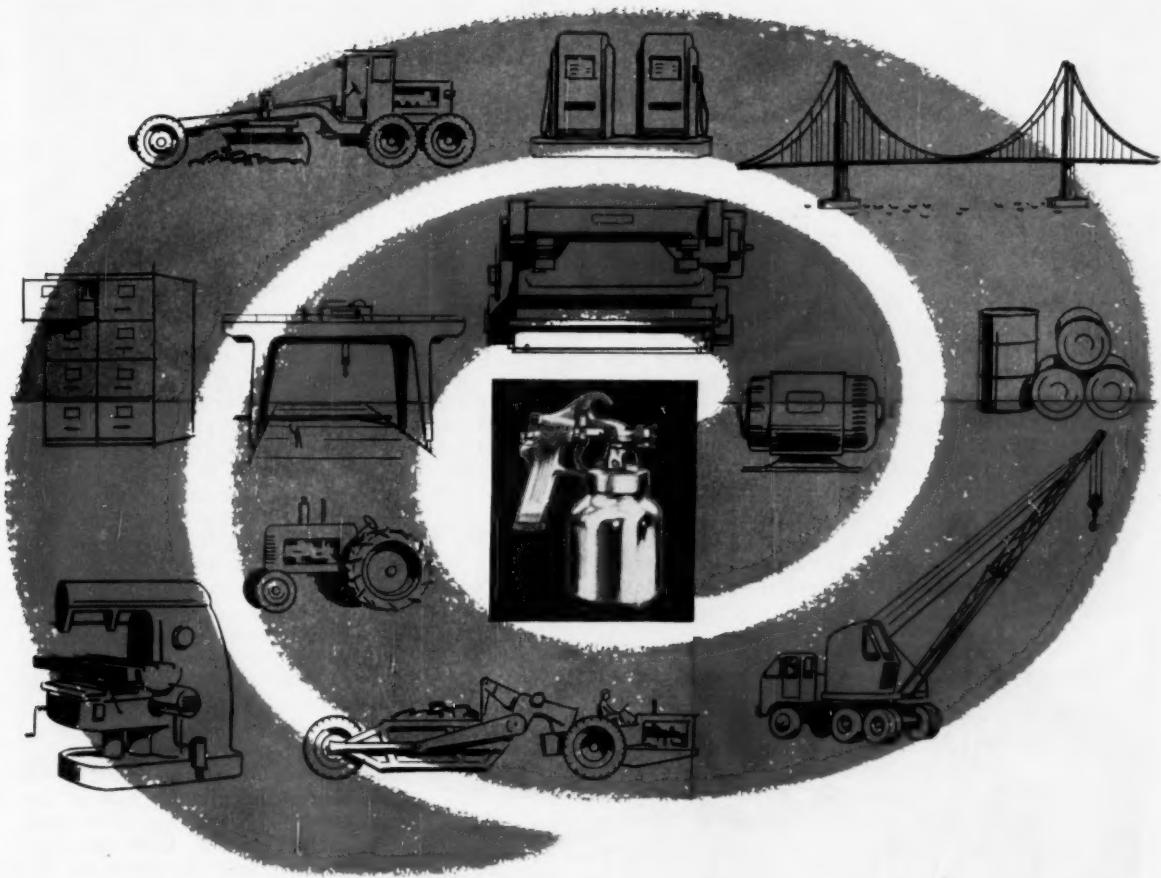
A typical week may find plant processing such diverse scrap as ingot ends, spoiled fuel plates, machine turnings, shavings, contaminated oxide powders and solutions. Baker converts all this scrap into U_3O_8

powder which goes back to the AEC for crediting to original customer's "uranium account" with the Commission.

Present plant capacity runs around 5 kg./day of 20% enriched uranium with provision for expansion as demand increases. Recovery of uranium averages over 98%.

► **Customer List**—Most of Baker's customers are fuel element fabricators in the U. S. who generate scrap worth about \$2,500/lb. during extrusion, swaging and drawing of metals into final fuel elements. Plant also pro-

* "Cold scrap" hasn't been irradiated in nuclear reactor, doesn't contain highly radioactive decay products.



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PROCESSES & TECHNOLOGY . . .

cesses scrap from some Canadian firms and currently is negotiating for AEC scrap.

Baker reprocesses scrap as a contract service, doesn't actually buy and sell uranium because it belongs to the U. S. government.

► **Ingenuity Helps**—Practically every batch of scrap shipped to the Baker plant presents a unique problem. Complicating factors include form of scrap, impurities and alloying agents.

Choice of processing attack on a particular batch rests to a large extent on the ingenu-

ity of production supervisor Eugene Nurmi. A chemical engineer with nine years' experience at Oak Ridge, Nurmi uses a combination of techniques developed originally by the AEC.

And every batch must be handled with care reminiscent of that college course in quantitative analysis. When you're handling a few kilograms of stock worth thousands of dollars, even small losses can be costly.

► **Varied Approach**—First step in recovery process is to get scrap into solution. Choice of

reagent is influenced by presence in scrap of molybdenum, aluminum, zirconium or stainless steel alloying or cladding materials.

Depending on which of these different materials are in the scrap, Baker uses nitric acid, aqua regia or hydrofluoric acid as dissolving agent. Oxide powders call for use of nitric acid.

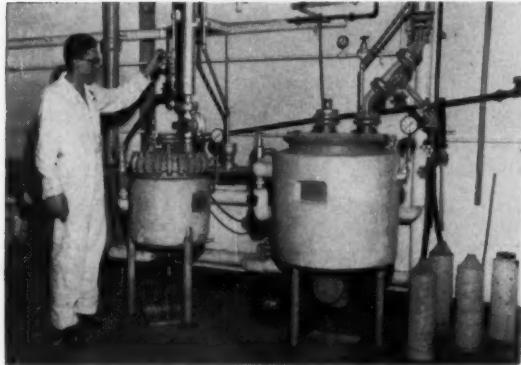
Dissolution takes place batch-wise in stainless-steel or glass-lined kettles. To prevent radiation hazard from critical mass buildup, operators limit batches to 300-350 g. enriched uranium.

Next, chemical assaying gives uranium content of solution and this value is checked out with sender of the scrap for final agreement on amount of uranium to be returned.

Operators then adjust solution chemically for solvent extraction: Nitric acid brings acid content to 3N level and aluminum nitrate furnishes salt requirement during extraction.

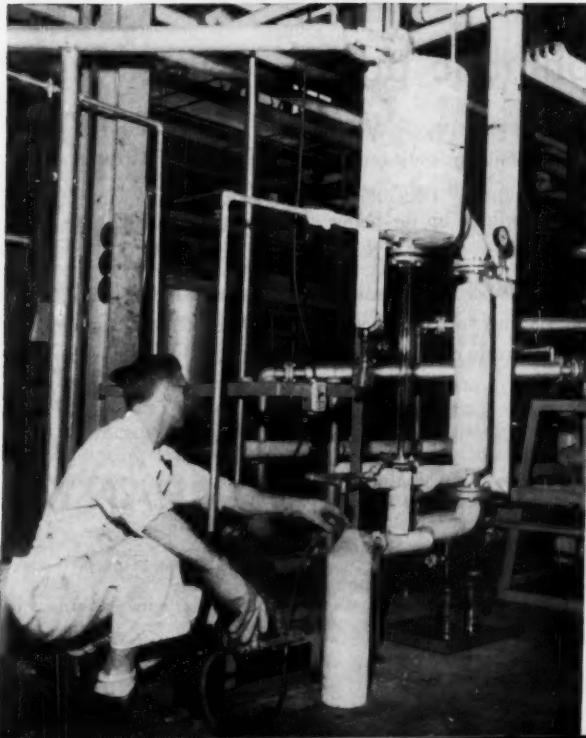
► **Uranium, Kerosene & TBP**—After adjusting solution, operator runs it through a York-Scheibel column where a 30% mixture of tributyl phosphate (TBP) in kerosene extracts uranium values. In a second column, dilute HNO_3 strips uranium from TBP. Both columns stand 5 ft. high, have 3-in. dia. and 42 contacting stages.

Dilute aqueous solution from stripping column goes to a thermal siphon evaporator (fabricated by Baker for this

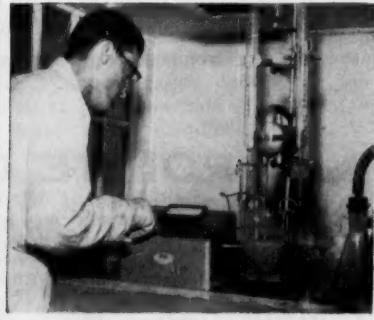


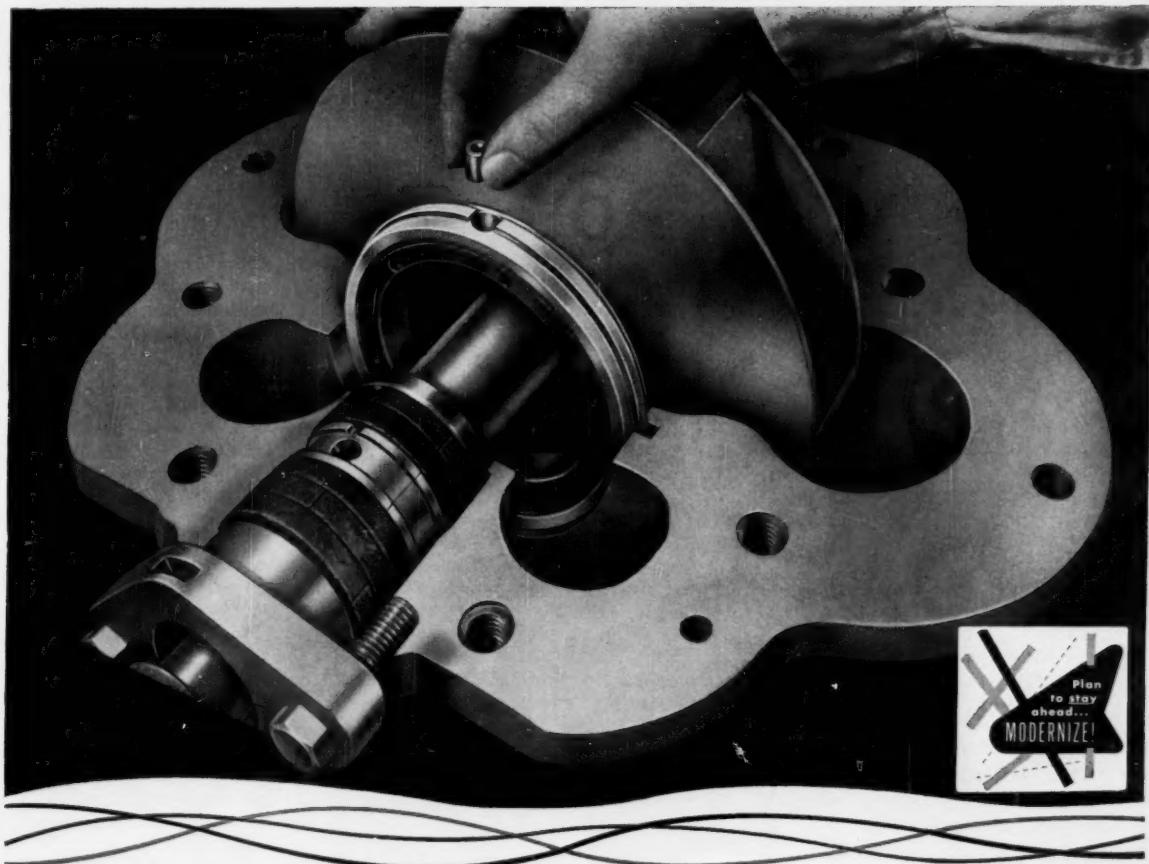
DISSOLUTION in glass-lined or stainless kettles readies scrap for extraction.

CONCENTRATION by thermal siphon evaporator precedes precipitation of UO_4 .



PRECIPITATION of UO_4 by H_2O_2 takes place at pH 2 to keep impurities in solution.





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specific application) for concentration from 0.25 to 1.0 N.

Operator then precipitates uranium peroxide (UO_2) from concentrate by controlled addition of hydrogen peroxide at pH 2. Precipitating at pH 2 ensures that impurities such as Fe and Al are left in solution, whereas with NH_4OH precipitation used formerly they would come down.

In final step, the UO_2 precipitate undergoes firing at 1,650 F. for conversion to black U_3O_8 powder. Again solid mass is limited to 350 g. to prevent radiation hazards. Fired product is ground in small ball mill to -200 mesh before shipment back to AEC.

► **Not Much Hazard**—Dangers involved in processing unirradiated uranium scrap are no greater than in handling any other poisonous material. Observes one Baker official, "You just have to be sure that no one spreads it on their sandwiches."

Certain precautions, however, are designed into process to

thwart any radiation buildup in enriched scrap which contains around 20% U_{235} .

As noted, operators limit batch operations to 300-350 g. And vessels containing enriched uranium solutions are limited to 5-in. maximum diameter with a minimum of 2 ft. between centers. Concentrated solutions, for example, are stored in 5-in. plastic bottles, each equipped with its own special cart to keep it at least 2 ft. away from any other bottle.

Every operator wears a film badge that is checked periodically to make sure that he hasn't been exposed to excessive radiation over extended intervals.

As another precaution, all exhaust fumes from plant pass through absolute filters that catch all particles down to 0.3 microns, preventing possible discharge of radioactive material to the atmosphere.

Waste disposal isn't much of a problem. All solutions are collected in drums and checked for contamination prior to dumping.

No special sewage system is needed.

► **Hot Scrap Next?** Baker officials admit they are interested in possibility of expanding into hot scrap reprocessing field (see p. 62).

But they are quick to point out that the technical and economic problems are multiplied manyfold when handling irradiated uranium. Process remains essentially the same, but shielding, remote-control handling, operation, maintenance and waste disposal problems all complicate the economics.

It's admittedly a far touchier situation than the relatively clear-cut cold-scrap picture. And so far, all private firms are maintaining a wait-and-see attitude, leaving hot reprocessing to the AEC.

Pressurized Electrolyzer Produces Hydrogen

Commercial production of hydrogen by high-pressure electrolysis of water is now feasible with cells built by Lurgi Gesellschaft, Frankfurt, Germany.

Designed for 425 psig. operation, the units require lower specific power consumption than conventional atmospheric pressure units, and compression of the final product is reduced or eliminated completely. For 1,000 cu. ft. of hydrogen and 500 cu. ft. of oxygen, at standard conditions, 123-129 kwh. of power is required as compared to 140-160 kwh. for atmospheric process.

► **How It Works**—A modification of the bipolar (filter-press type) cell construction popular in Europe, the Lurgi electrolyzer consists of 400-600 diaphragm-separated cells connected in series. A potential of up to 1,200 d.c. volts is applied across the unit.

Caustic potash electrolyte (sp. gr. 1.25) circulates through anodic and cathodic chambers of each cell. Gases travel with electrolyte to separators after which the solution recycles. Distilled water makeup washes collected gases, then joins electrolyte.

Available units produce 7,000-21,000 cu. ft. of hydrogen per hour, but the company sees no technical hindrance to larger installations.



Slurrying Setup Readies Coal for Pipeline

Pittsburgh Consolidation Coal Co.'s facilities at Georgetown, Ohio, prepare coal slurry for its 108-mi. pipeline journey to Cleveland Electric Illuminating Co.'s

Eastlake, Ohio, plant. Now in full operation, pipeline has capacity of 150 tons/hr. of slurry which contains 50%, by weight, of coal.



open motors for extreme conditions
Save up to 60%!

Here's an amazing advance in motor technology! It's the *Super-Seal* motor line — an open motor design so completely unaffected by moisture, dust, dirt, oil, acids and alkalis that it can be used in many applications previously requiring more costly enclosed motors. *Savings range from 15 to 60%.*

Super-Seal motor superiority results from revolutionary insulating techniques. Available in any integral horsepower size, smaller *Super-Seal* motors incorporate an encapsulated stator. A durable epoxy resin encloses the stator, creating an electrical system impervious to outside elements.

In larger sizes, *Silco-Flex* insulation is used. In this system, silicone rubber is vulcanized into a homogeneous mass to form a flexible, moisture and heat resistant, void-free dielectric barrier around coils and leads.

Both of these insulation systems are unsurpassed. Proof? An encapsulated motor ran for hundreds of hours at full load in a 4% brine solution.

Find out more about new economies in motors from your A-C representative or distributor, or write Allis-Chalmers, General Products Division, Milwaukee 1, Wisconsin. *Silco-Flex* and *Super-Seal* are Allis-Chalmers trademarks.

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BARIUM OXIDE product mixed with unreacted carbon flows from primary reactor.

Lower Process Temperature Ups BaO Quality

By rigid control of operating tricks, new barium-oxide process avoids temperature level where purity-robbing eutectic forms.

In the face of rising interest in high temperature processing techniques, Barium Reduction Co., South Charleston, W. Va., reports a notable advance toward lower temperatures.

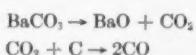
Using a new fluid-bed process, Barium Reduction Co. reduces BaCO_3 to BaO at a temperature level of 1,680 F., some 500-800 deg. below conventional reduction level in arc furnaces.

Product reaches 97-99% purity, 8% higher than average purity of the arc-furnace product. Even with a premium price tag, this high-purity material is claimed more economical than

barium hydrates as an additive in lubricating oils.

Process was developed on a small pilot scale and patented by Columbia-Southern Chemical Corp. Commercialization by the Barium Reduction Co. required two more years of development under Barium Reduction's Technical Director, Mr. L. Preisman, recognized barium authority.

► Eutectic Hampers Reduction —At the temperature required to reduce BaCO_3 by electric arc, according to reactions:



a $\text{BaCO}_3\text{-BaO}$ eutectic mixture forms localized fused spots which prevent complete reduction of the charge. At best, product purity is about 90%. And even this purity level rests on careful sorting to eliminate fused pieces.

► Prevent Fusion — Through careful control of operating conditions, Barium's fluid-bed reactor avoids this pitfall. By maintaining bed assay above 90-92% BaO and holding temperature close to 1,680 F., Barium Reduction avoids formation of a eutectic mixture. Thus, each particle is free to undergo virtually complete reduction.

To achieve a reaction at this low temperature, Barium Reduction lowers the partial pressure of CO by using nitrogen sweep gas to fluidize the bed and re-

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move gaseous reaction products.

► **Hold Uniform Temperature**—Barium Reduction Co. produces 20 tons/day of product with six reactors. Standing 20 ft. high, these reactors operate as two stages: a primary reduction stage and a secondary stage to burn off excess carbon reducing agent. Each reactor is enclosed by a gas-fired furnace having 35 burners positioned to distribute heat uniformly to the reactor.

Thermocouples at 13 different locations on reactor shell control firing rate and shell temperature. Two thermocouples in bed control feed rate. Acting together these controls hold bed temperature within 5 deg. of set point.

► **Start With Ore**—Manufacture of BaO starts with reduction of barite ore (BaSO_4) in rotary kiln, using coal with high fixed carbon content as the reducing agent. The BaS black ash, leached with water, yields solution which is carbonated with either Na_2CO_3 or CO_2 to form BaCO_3 .

Under carefully controlled conditions, Barium Reduction dewaterers and washes the barium

SCRUBBERS guard purity of N_2 sweep gas flowing to reactors.



carbonate in a continuous centrifugal to a specified moisture content. Wet cake goes to a pug mill where it mixes with carbon black to a final consistency of 65-68% solids. On a dry basis, mixture contains 6.3% carbon.

► **Pelletize to Fluidize**—From the pug mill, mixture feeds into rotary dryer-agglomerator which delivers dry pellets to reactors. Moisture content in feed to agglomerator, gas temperature and bed temperature must be controlled closely to obtain satisfactory pellets.

Pellets feed onto the surface of the fluidized bed in reactor. After several hours in the reactor, fully reduced BaO pellets discharge intermittently from bottom by manual control.

Because discharge from fluid bed contains excess carbon, it goes to "whitener" reactor for processing at slightly higher temperature. Final shot of oxygen burns off the remaining carbon. Operating batchwise, this step in process takes $\frac{1}{2}$ - $\frac{3}{4}$ hr.

► **Keeping Solids Fluid**—Nitrogen at 2,000 cfm. enters the bottom of the reduction reactor. Distributor delivers gas uniformly over tower cross section to fluidize charge uniformly and minimize slugging. Gas leaves reactor through cyclone which removes entrained dust and returns it to reactor.

Nitrogen comes from combustion generator via monoethanolamine and caustic-soda CO_2 scrubbers, followed by cooler and silica gel dryer which remove water.

At point of entry to reactor, nitrogen is completely free of CO_2 and O_2 , with only a trace of CO. Moisture content of the nitrogen must be less than 0.0009 lb./1,000 cu. ft. at -80 F. to avoid formation of barium hydrates.

An oxygen analyzer continuously checks the nitrogen stream to detect any variation from the specified 0.00% O_2 content. A continuous bleed bubbles through $\text{Ba}(\text{OH})_2$ solution to signal any presence of CO_2 .

While Barium Reduction now reaps the fruits of this modern process, Preisman and his associates attest that only through their combined talents could they reduce it to practice.

Reds Emphasizing Chemical Expansion

From the amount of chemical activity going on behind the Iron Curtain, it's evident that the Reds aren't waiting around for the West to act on Nikita Khrushchev's bid for increased flow of Western chemical know-how to Communist countries. Reports seeping under the Iron (and Bamboo) Curtain show the Reds' widespread emphasis on chemical processing:

Soviets are reportedly erecting an oil-shale plant at Kochtla Jarwe, Estonia, that will process 4 million tons shale annually.

And Russians are supplying equipment for a coal hydrogenation plant that is under construction at Fushun, China, 100 mi. from North Korea.

Peking Radio reports that Red China plans to start seven synthetic fiber plants in Shanghai this year; among products will be Terylene, nylon 66 and pilot quantities of Orlon.

Red China has also ordered six oxygen plants and four nitrogen fixation plants from Czechoslovakia and is planning a plant for recovery of sodium, potassium and magnesium chlorides and magnesium bromide from sea water. Construction is already under way at Tientsin on catalytic sulfuric acid works with annual capacity of 40,000 tons.

Fluorine Harnessed for Rocket Propellant Use

Crowning intensive research into handling properties of liquid fluorine, Bell Aircraft Corp., Buffalo, N. Y., has now successfully used it as a chemical oxidizer in large-scale rocket thrust-chamber firings.

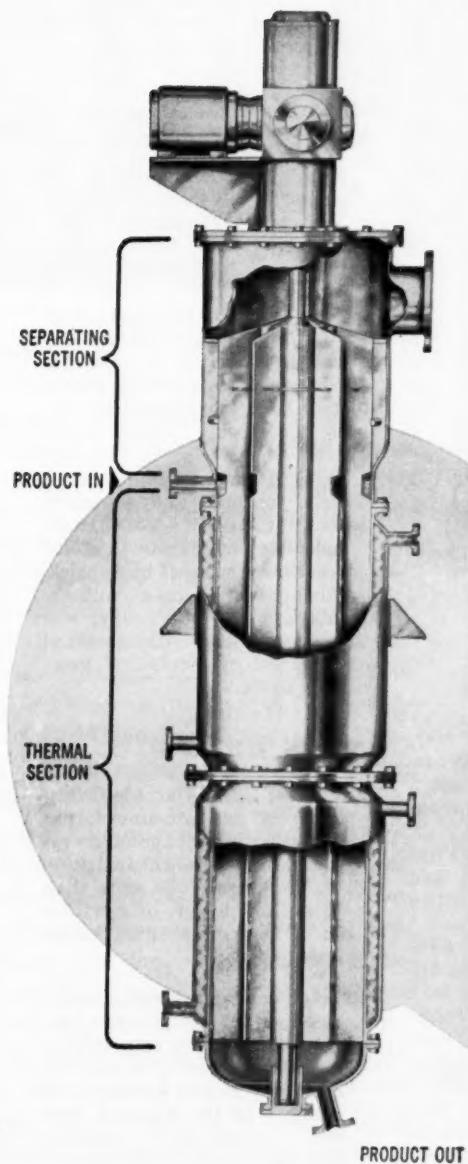
Significance of this, Bell points out, is that specific impulse of rocket propellants can be hiked, through use of liquid fluorine, to 300-345 lb./sec., compared to 245 lb./sec. thrust of liquid oxygen-kerosene propellants. Rockets can carry bigger payload.

Bell developed special techniques in handling, metal treatment and welding for all rocket thrust-chamber components. Special test facility holds liquid fluorine at -306 F.

Solve Difficult Liquid Processing Problems with the New

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TURBA-FILM® MARK II PROCESSOR



When viscous fluid processing is "bugged" by complex procedures, time-at-temperature-sensitive materials, sluggish control of product quality... look to the new Rodney Hunt Turba-Film Mark II Processor to simplify your problems.

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dehydration... evaporation...
heat transfer... reaction...
stripping... and other processes.**

Short-time exposure and minimum hold-up of the process fluid in the thermal section assures uniform heat and mass transfer, even at high temperature. Foaming is controlled by a mechanical separator and the formation of crust is minimized permitting continuous operation for long periods.

A large number of installations have proved conclusively the superiority of the Turba-Film Processor for processing chemicals, pharmaceuticals, latices, solvents, foods and many other products.

An Invitation

Rodney Hunt will be happy to work with you in solving your process problems, utilizing its extensive engineering, laboratory and pilot plant facilities. Address your inquiry to the Rodney Hunt Process Equipment Division or write for Catalog 117, the story of the Turba-Film Processor.

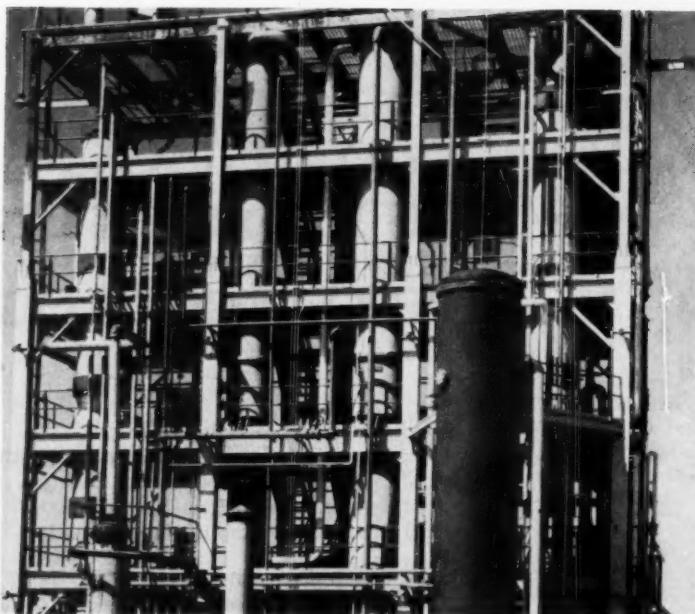


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SERVING THE PROCESS INDUSTRIES WITH EQUIPMENT AND ENGINEERING

CHEMICAL ENGINEERING—October 6, 1958

UNIT shows absorbers and strippers for CCl_4 (left) and Cl_2 (right).

New Scheme Cuts HCl Purifying Cost

Hooker Chemical Corp. has come up with a process which it claims gives an economical answer to that old problem of purifying byproduct HCl from organic chlorinations.

Just-patented process (U. S. 2,841,243) is installed at Hooker's Montague, Mich., plant to clean up anhydrous HCl which is piped on a large scale to Du Pont's nearby neoprene facility.

Hooker claims that capital investment for its two-solvent process is about one-half as much as for the older hydrochloric acid absorption-desorption procedure. ► **Old Versus New**—Hydrochloric acid process is in most common use today. Gas stream containing HCl and impurities is scrubbed with aqueous hydrochloric acid, dissolving HCl. Anhydrous HCl is distilled out of the solution and azeotropic HCl mixture is recycled. This system has two drawbacks: Corrosion is a serious problem and chlorine recovery is tricky.

Hooker's route takes the opposite approach. Instead of absorbing HCl and leaving impurities behind, impurities are stripped out leaving product HCl with less

than 10 ppm. Cl_2 . In this way, utility costs are lowered and corrosion headaches are eliminated—mild steel is used throughout Hooker's setup.

► **Two-Zone Stripping**—First step is to absorb chlorine and most of the organic impurities from the chlorination off-gas.

Gas, containing about 88% HCl (by weight), 9% Cl_2 and 3% organic impurities, flows to a packed tower and is scrubbed with carbon tetrachloride. Overhead fraction leaving absorber contains around 50% CCl_4 , 49.5% HCl and only 0.02% Cl_2 . This stream then flows to carbon tet absorber at 95 F. and is scrubbed with hexachloro-butadiene; effluent HCl from top of tower is further purified by compressing and recycling through a third scrubbing column where it contacts more hexachloro-butadiene at 5 F. Final anhydrous HCl product contains virtually no chlorine or carbon tet and only 0.01% hexachloro-butadiene.

Chlorine and dissolved HCl in bottoms from first absorber can be boiled out and recycled to chlorination unit. Carbon tet dissolved in hexachloro-butadiene is

recovered by distillation and recycled to first scrubbing zone.

Hooker is currently studying plans to license the process.

More Seawater Magnesia Slated for Production

Now nearing completion at Pascagoula, Miss., multimillion-dollar seawater magnesia plant of H. K. Porter Co.'s Refractories Div. will be on stream late this year.

And away to the east—Port St. Joe, Fla.—will be the site of Michigan Chemical Corp.'s 125-150-ton/day seawater magnesia plant. Michigan Chemical has now completed construction plans.

H. K. Porter will produce a line of chrome and periclase specialties in addition to chrome-magnesite, magnesite-chrome and periclase types of basic brick.

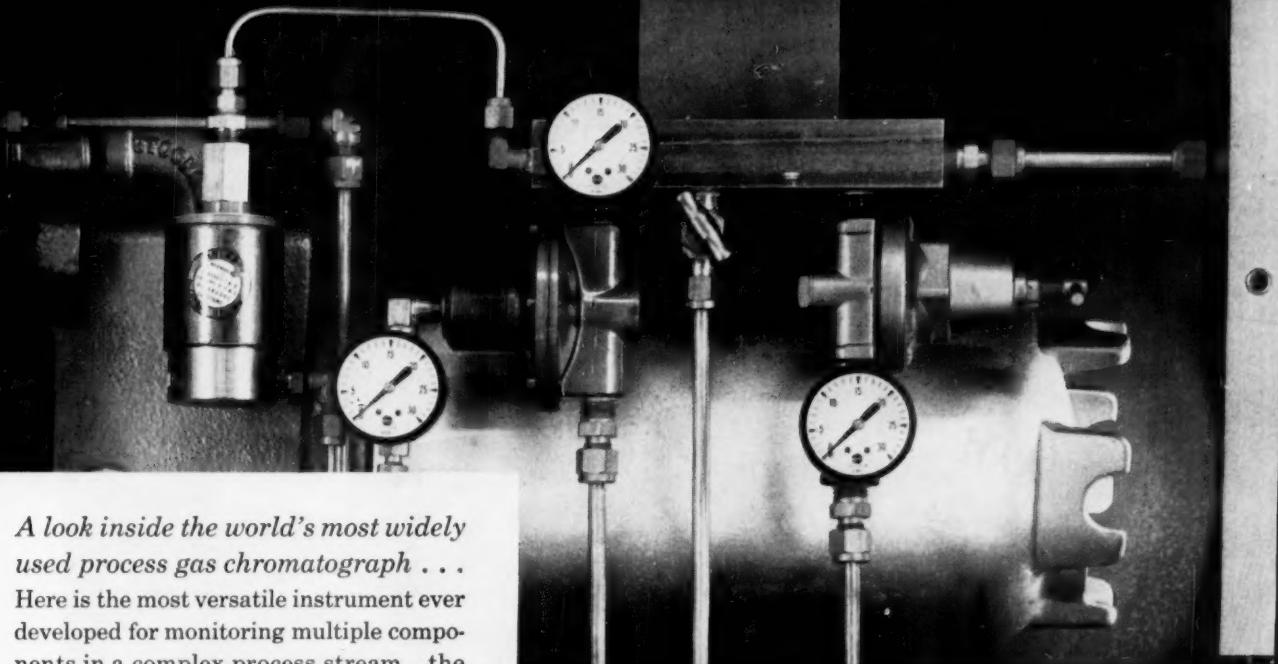
Michigan Chemical's plant, expandable to 300 tons/day, will turn out high-purity chemical and refractory grades of magnesium oxide.

NEWS BRIEFS

Epoxies: Union Carbide Chemicals Co. has announced that it will build an expanded version of a new unit at Institute, W. Va., to produce more than 10 million lb./yr. of epoxides and other oxygenated chemicals.

Reactor coolant: Siemens-Schuckertwerke, A. G., has developed nitrogen tetroxide as gaseous coolant for nuclear reactors. In two temperature ranges—50-150 C. and 300-600 C.—nitrogen tetroxide dissociates into products with high specific heats.

Acetylene process: Tennessee Eastman is making available for license its flame cracking process for simultaneous production of ethylene and acetylene (*Chem. Eng.*, Jan. 27 1958, p. 58). Under license contract, Stone & Webster Engineering Corp., Boston, Mass., will design and build plants in the U. S. and will represent Eastman in foreign licensing.

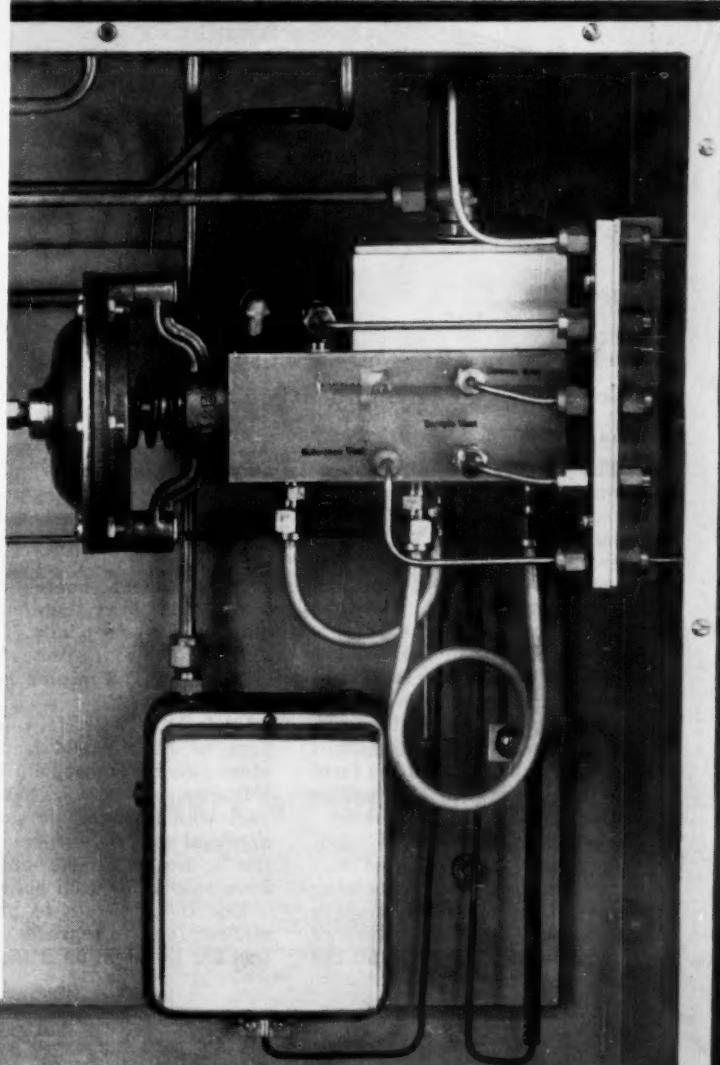


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DEVELOPMENTS ...

CHEMICAL ECONOMICS

EDITED BY D. R. CANNON



... Cue for Atom-Fuel Processing by Industry?

Chemical processors, long wary of going it alone in nuclear fuel processing, have new reasons for giving the role another, more confident look.

John A. King, Assistant Editor

The case for chemical processing in nuclear-fuel recovery got a mighty boost recently when the outgoing 85th Congress ratified the U. S.-Euratom plan for developing atomic power abroad.

True, the paths to fuel-service markets are still not strewn with rose petals. But the Euratom (European Atomic Energy Community) agreement promises that new, firm markets will be a reality by 1963, in the form of 1 million kw. of nuclear power capacity in Europe.

Serving to further whet chemical-industry interest: the lode of nuclear-fuel processing know-how disclosed last month at the U. N. Atomic Energy Conference in Geneva; and the

news now that private industry is already nibbling at the nuclear-fuel processing business (see pp. 50-54 this issue).

Euratom's capacity goal may prove a bigger, nearer target for U. S. industry than our own planned power capacity. This is scheduled to reach only 700,000 kw. by 1961, 1.3 million kw. by about 1965.

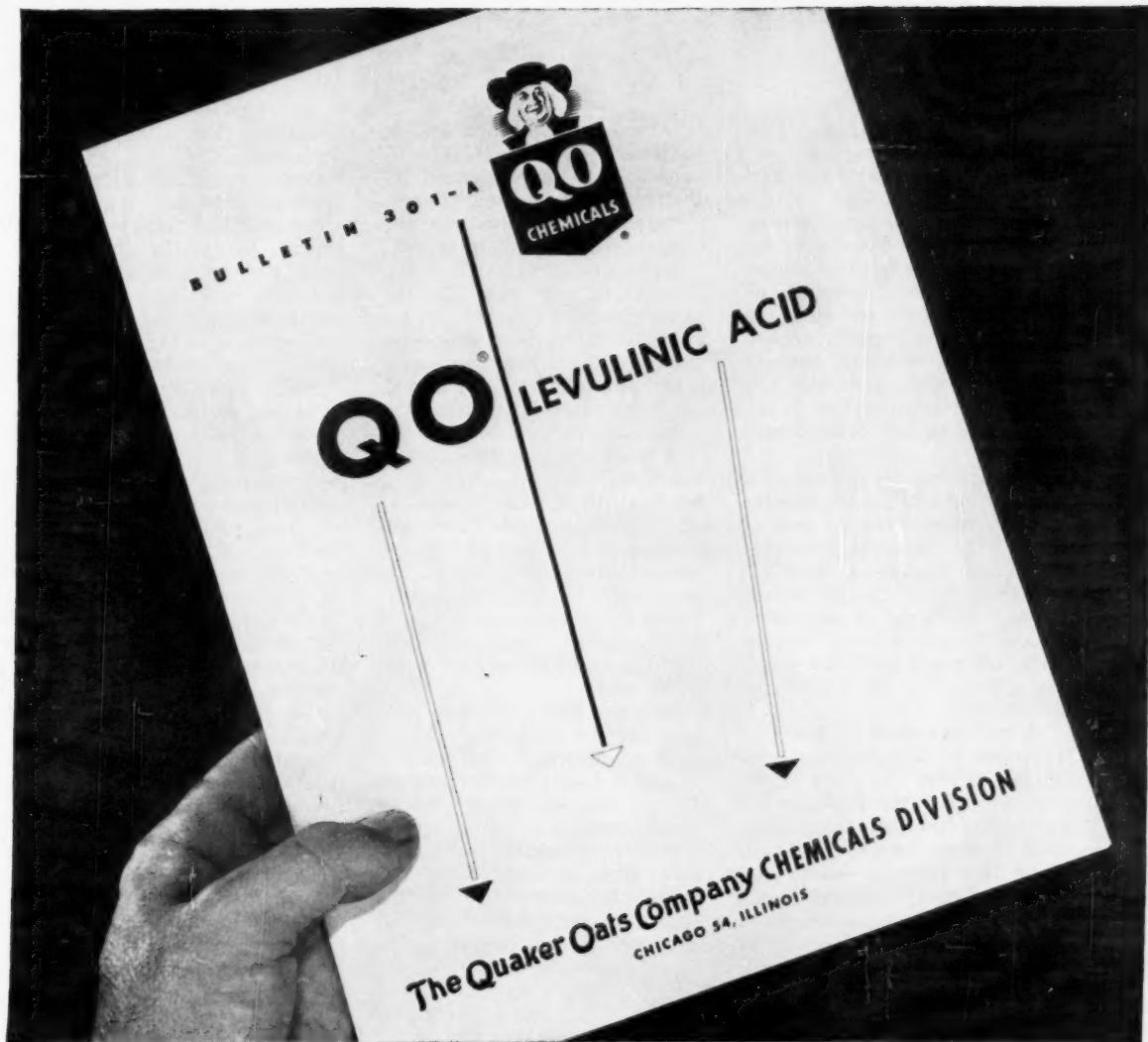
► **Uncle Sam Will Help**—Uncle Sam, as Free World leader in atomic energy, must help if this Euratom goal is to be met. The pact which won Congressional approval says he will help. And that's something no one has been able to bank on before.

The U. S. agrees to provide nuclear fuel; to reprocess spent fuel for Euratom until facilities

are available in Europe or on a commercial basis in this country; to guarantee a maximum fuel-cycle cost to Euratom buyers of 4.2 mills/kwh., unless equivalent or better offers are forthcoming from industry.*

► **Fuel-Cost Pledge**—If U. S. private industry is unable to maintain products and services below the guaranteed maximum fuel-cycle cost, the government will underwrite the difference (up to \$90 million between now and 1973). This government backing puts a ceiling on the European buyer's potential fuel costs and provides incentive for

* U. S. government and industry agree to do many other things under the U.S.-Euratom pact. They will fabricate and sell fuel elements containing 30,000 kg. of U-235; and purchase all plutonium produced in the course of reactor operation. Euratom and the U.S. will each invest \$50 million over the next five years on research and development to reduce present fuel-cycle costs and improve reactor technology. And the U.S. will lend up to \$135 million of the total \$250 million estimated to be the capital cost of the 1-million-kw. Euratom program.



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ECONOMICS . . .

private-industry entrance into the business.

For uranium processors and fuel-element fabricators, Euratom power means expansion of business already devoted to domestic operations. For those companies which already, or might, sell services—such as fuel-fabrication-scrap recovery and radioactive-waste disposal—to the nuclear industry, the government help implied in the U. S.-Euratom pact is an attraction.

► **Reprocessing Chancy**—But a great uncertainty still obscures the ripest, most logical field of all for the chemical industry: spent-fuel processing. Now exclusively the responsibility of Atomic Energy Commission plants, this operation is fraught with both profit peril and potential (*Chem. Eng.*, July 1957, pp. 202-206).

With the volume of business proposed by the Euratom program, private industry could conceivably enter fuel reprocessing for the first time. However, fuel-reprocessing's share (and this includes waste disposal) of total fuel-cycle costs of 4.2 mills/kwh. is estimated to be a slim 0.3 mills. Such an allowance surely calls for the most economical method that's technically feasible.

Which fuel-reprocessing method is technically and economically the best? Or is there any technology now which will permit any other than the AEC-husbanded setup we have today?

► **Try "Cold" Scrap First**—Perhaps the most likely candidate to pioneer private spent-nuclear-fuel reprocessing is some company which first recovers "cold", or non-radioactive, fuel-

fabrication scrap. Such a company is the Irvington-Baker Refining Div. of Englehard Industries, which operates the first privately owned plant in the scrap-reprocessing field (p. 50).

Scrap recovery is much like spent-fuel reprocessing; the same solvent extraction process is employed. Only the shielding, waste disposal and remote operation and maintenance necessary with hot, or irradiated, fuel is missing (as well as a mighty stiff additional capital investment).

► **Versatility Comes First**—Today nuclear fuels are reprocessed domestically by the solvent extraction process. Its principal virtue is versatility. Solvent extraction can handle all types of irradiated fuel, metallic and non-metallic (uranium oxide).

It is the only technique suitable for the oxide fuels which are the choice in Europe because of their low enrichment (3% U-235) and modest inventory charge.

Solvent extraction, though, is rife with economic disadvantages. Inherently a complex operation with many steps, it requires a high capital outlay—as much as \$11,000/kg. of daily uranium capacity—even for a small capacity. Large throughput has been the answer in AEC facilities and is the reason why private industry, if it is to compete, must do so in large, centrally located plants.

And the reason why Eurochemic, the company formed by 12 European countries, will finish building in 1961 a pilot plant at Mol, Belgium—the model for future, and much larger, facilities—to handle

spent fuel from all six Euratom countries.

► **Costly Shipping**—Solvent extraction requires shipment of irradiated fuel from reactors to central processing sites. Shipping hot fuels involves lead-shielded containers. Container costs can run, for highly enriched fuels, as high as \$25,000/kg. of uranium contained.

One possible solution is interim "cooling" before shipment so that shielding can be lighter. An economic balance must be reached between cost of shipping hot fuel and cost of carrying cooling fuel in inventory.

For inventory is a vital factor in the overall economic picture. With highly enriched fuel worth \$15,000/kg., the less material tied up in nuclear fuel-cycle inventory the better.

Unfortunately the fuel cycle in solvent-extraction processing carries the equivalent of several reactor charges: one charge undergoing fission in the reactor, another in transit between reactor and reprocessing plant, another being reprocessed.

► **Nasty Wastes**—Another fly in the ointment for solvent extraction is waste disposal. As much as 800 gal. of high-level wastes/kg. of uranium reprocessed gush from the process plant.

Now we can only cool, or deactivate, them for a period, concentrate them by evaporation, and store them in massive underground tanks, shielded by concrete and equipped with miles of stainless-steel coils to remove heat of radioactive decay (photo, this page). Here hot wastes decay before sea burial in concrete containers.

We do this because we know of no other sure way to handle these materials.

First steps alone run from \$2 to \$10/gal.; ocean burial, about \$1/gal. concentrate. These costs are far in excess of recommended costs for Euratom, which allow only about one-tenth of total reprocessing costs, or 0.03 mills/kwh.

Fluor Corp. is working on a method whereby liquid wastes are calcined and converted to compact, easily stored waste. At Hutchinson, Kan., the AEC,

DISPOSAL COSTS abound at Idaho Falls tank farm for radioactive waste.





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assisted by the American Petroleum Institute, is seeking ultimate storage of low-level wastes in the depths of salt domes. And Nuclear Engineering of Walnut Creek, Calif., is developing lower-cost ocean burial of the same wastes.

In spite of high costs of waste disposal—inventory, transportation, capital outlay—solvent extraction will live on as an important method of reprocessing. The trend in Europe toward non-metallic, uranium oxide fuels will help see to that.

► **Special Methods**—There are other methods of fuel reprocessing which have few of solvent extraction's economic ailments. Although not yet in production, they will compete on suitable, metallic fuel.

In the pyrometallurgical method, decanned fuel elements are melt-refined. Fission products are absorbed in furnace walls, in an oxide slag, or are volatilized.

Advantages are short interim cooling periods, easy-to-handle wastes, compact on-reactor-site processing. Inventory costs are cut, shipping costs eliminated.

Atomics International and Argonne National Lab are trying to integrate a pyrometallurgical process in a single reactor's fuel cycle. Argonne's fuel-processing work with Experimental Boiling Water Reactors may pay off in Europe where the first reactors are of the same types—probably pressurized and boiling water types—as those already checked out in the U. S.

► **For Metallic Fuel Only**—Pyrometallurgical processing, it should be repeated, can handle only metallic fuels; blanket fuel elements will have to be processed at central solvent extraction plants.

Fluoride volatilization is another proposed integrated processing scheme for metallic fuel. It boasts the same virtues as pyrometallurgy, but involves more steps. Fuel elements are decanned, and fluorinated. Volatile uranium hexafluoride is distilled and reduced to metal for refabrication into fuel elements.

For work Argonne is doing on these and other projects—

extraction with molten metal or salts, fractional crystallization of uranium-zinc complexes, electrodeposition—see *Chem. Eng.*, Sept. 22, 1958, p. 69. These new techniques have yet to be proven feasible, let alone economical.

Computer to Probe Methanol-Formalin Future

Chemical market forecasting will never be an exact science. But electronic data-processing machines now promise an extended coverage never before approachable.

Taking the cue, Celanese plans to turn its medium-sized computer at Corpus Christi, Tex., loose on the market future—first on close-range sales forecasts, then on longer-view evaluations of chemical potential.

High on the list for Celanese researchers will be methanol and formaldehyde—two interrelated chemicals whose national capacities have continued to grow substantially during the past several years despite a leveling off in demand.

Today's capacities for both products are sufficient, if totally utilized, to satisfy projected U.S. requirements for the next 5-8 yr. or longer.

► **Captive Capacity**—One of the problems in these two basic chemicals has been the large portion of new capacity that is captive. This, in effect, has worsened marketing problems of established merchant producers. For it's one thing to have new competitors for your customers, and quite another thing to find your former customers supplying their own needs.

This overcapacity of merchant producers of formaldehyde and methanol has produced a highly competitive marketing situation the past year. Recent price reductions in both chemicals were a direct reflection of this imbalance.

► **Looking Ahead**—In a year which has been a rough one for many producers, Celanese claims it has managed to keep formaldehyde and methanol inventories within desired limits, has, in fact, been operating at capacity.

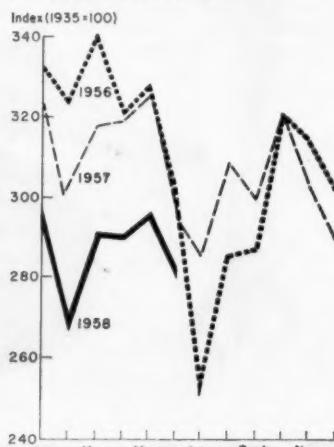
For this the company thanks

its internal efforts to build methanol and formaldehyde into highly marketable derivatives like paraformaldehyde, trimethylolpropane, trioxane and acrylic esters. Even so, Celanese is looking to the future and wants even better tools with which to do it.

Celanese knows full well that no one factor—be it raw materials cost, freight charges, product price, technology changes, plant size, or even end-product breakdown and volume—wags the whole market setup. So dovetailing all these factors together in a computer will give new insight as to how they combine to describe the profitability pattern of any chemical.

Biggest benefit, perhaps, will accrue from being able to better anticipate effect, on chemical demand, of trends in the ultimate chemical-consuming industries, however remote.

Chemical Consumption



Consumption by Industries

	May (Final)	June (Est.)
Coal products	7.3	7.4
Explosives	9.5	9.8
Fertilizer	77.7	57.6
Glass	28.3	29.3
Iron & steel	11.6	13.1
Leather	3.9	4.0
Paint & varnish	38.1	37.0
Petroleum refining	28.9	28.7
Plastics	22.5	22.2
Pulp & paper	35.4	35.2
Rayon	21.0	20.7
Rubber	5.8	6.0
Textiles	8.8	8.5
Total	298	280

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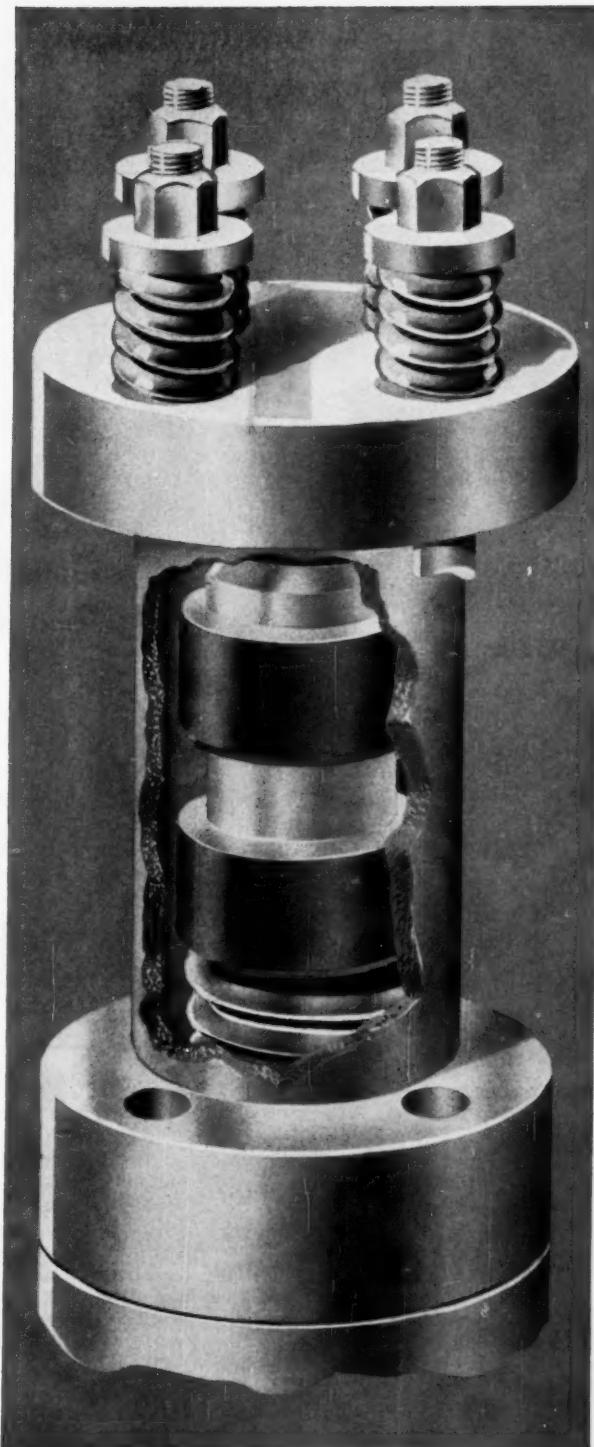
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tive high pressure plastics and wood has been introduced.

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Chlorinated Xylenes

Three new ones show promise as intermediates.

Already in pilot plant production of six chlorinated xylene compounds, Diamond Alkali is adding three more. One of the new products is derived from p-xylene, while the other two are m-xylene derivatives and represent the first chemicals to be offered by Diamond from this raw material.

They are terephthaloyl chloride, a derivative of γ, γ' -hexachloro-p-xylene, γ, γ' -hexachloro-m-xylene and its derivative isophthaloyl chloride. γ, γ' -hexachloro-m-xylene hydrolyzes to isophthalic acid, forms isophthalic esters through alcoholysis,

sis, and can be halogenated in the ring.

Both terephthaloyl chloride and isophthaloyl chloride can be reduced to dialdehydes and dibasic acids, can be oxidized to acids, and can be esterified easily with alcohols. They react readily with ammonia, amines and amino compounds. These acid chlorides will undergo the Friedel-Crafts reaction, will react with organic sodium compounds, with Grignard reagents, and can be chlorinated.

The high reactivity of the terephthaloyl and isophthaloyl chlorides makes them especially interesting as raw materials for interfacial polycondensation for preparation of polyamides and polyphenylesters.—Diamond Alkali Co., Cleveland, Ohio. 68B

Epoxides

Series of oxygenated chemicals not available before in commercial quantities.

More than 10 million lbs./yr. of new epoxides and other oxygenated chemicals will be produced in a new Institute, W. Va., unit to be completed by mid-1959.

Among the new products are Epoxide 201, vinylcyclohexene dioxide, vinylcyclohexene monoxide, dicyclopentadiene dioxide, styrene oxide, allyl epoxystearate, and caprolactone. These products are expected to play an important part in resin technology and to serve as chemical intermediates as well.

Special emphasis is to be placed on Epoxide 201 which forms plastics and coating resins of outstanding color stability and resistance to heat distortion. Chemically 3,4-epoxy-6-methylcyclohexylmethyl-3,4-epoxy-6-methylcyclohexane-carboxylate, it is more reactive to acid and anhydride hardeners than any other diepoxyde.

Vinyl cyclohexene dioxide is a viscosity reducing agent for epoxy resins and performs its function without lowering the heat distortion temperature of conventional epoxy resins. Dicyclopentadiene dioxide forms resins of exceptionally high heat distortion temperature. Allyl epoxystearate can be used as a monomer.

In addition, two combination plasticizer-stabilizers for vinyl resins will be marketed. This marks the first time that all-synthetic materials have been available for this purpose. The new materials are di-2-ethylhexyl epoxy tetrahydrophthalate and di-isodecyl epoxytetrahydrophthalate. These materials are characterized by excellent stability and complete compatibility with vinyl chloride resins.—Union Carbide Chemicals Co., New York, N. Y. 68C



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Alcohols exist as free alcohols, fatty acids as free acids. Free alcohols can be reacted independent of the free fatty acids. Free fatty acids can be easily neutralized or reacted independent of the free alcohols.

In some reactions such as with ethylene oxide, both the fatty alcohols and the fatty acids react. It is possible to produce adducts with very low mole content of oxide and very low acid numbers, even less than 4.0.

Emulsifiers, lubricants, surfactants, detergents, amines are among the reaction products of interest.—Werner G. Smith, Inc., Cleveland. 70A

Aircraft Paints

Five times brighter than conventional paint, eases plane spotting.

The Air Force plans to paint daylight-fluorescent markings on some 13,000 aircraft to increase their visibility. This is expected to lessen danger of mid-air collisions and make it easier to spot a plane that is forced down.

The bright orange markings—five times brighter than conventional color—will cover about 30% of a plane's surface.

The coating contains a resinous type of pigment in an acrylic binder, and the clear protective acrylic overcoating is fortified with materials that resist sun fading.

Reason for the brilliance of the paint is that it is a source as well as a reflector of color. The color absorbs shorter wave lengths and emits them as amplified color of a higher wave length. And light passes through the translucent paint and is re-

flected back through the film by the white undercoat.

The paint will stay bright for up to a year of outdoor exposure. It can be seen at distances up to 30,000 ft., unlike conventional color, which blends into gray or white at a great distance.

Fluorescent markings have proved successful in tests conducted by the Civil Aeronautics Administration, the Air Force and Navy. The CAA has adopted the color patches on all its planes.

The manufacturer foresees other applications for the paint, such as visibility markings on autos and speedboats. The paint has also been used on guided missiles, tow-targets, torpedoes and safety signs.—Radian Color Co., Oakland, Calif. 70B

Paints

New metal protective compound, new chlorinated rubber paint.

A new metal protective paint that doesn't contain pigments or resins is now being manufactured.

With a zinc-silicate base, it will protect metals from atmospheric, sea water, fresh water, electrolytic, galvanic and carbon chemical corrosion.

The paint is said to resist a temperature as high as 1,000 F., and only two coats are necessary.—MacLeaster Chemical Co., 16 Mill Lane, Carshalton, Surrey, England. 70C

New chlorinated rubber paints which resist chemicals, water and fungus have been developed. They are superior to conventional chloride rubber paints because they can be applied as easily as oil bound colors. Drying time is about an hour.—Corrosion Ltd., 16 Gloucester Pl., London W. 1, England. 70D

BRIEFS

New use for Gilsonite, the natural hydrocarbon found in Utah, is a cold bituminous concrete for road surfacing. Called Gilsapave, it can be laid cold, even after the tem-

perature drops below 35 F., the normal cutoff point for spreading hot-mix asphalt.—American Gilsonite Co., Salt Lake City, Utah. 70E

Bacterial inhibitor that will extend the life of soluble oil emulsions has been developed for the metal working industry. Called Elcide 75, it is a combination of thimerosal and sodium-o-phenylphenate and is effective in all standard duty soluble oil emulsions.—Eli Lilly & Co., Indianapolis, Ind. 70F

Amphoteric surfactant called Miranol C2M Conc. is now available for both new steel drum manufacture and reconditioning of old drums. It is stable over the entire pH range in both muriatic acid and caustic soda as well as in other acids and alkalies.—Miranol Chemical Co., Irvington, N. J. 70G

Polypropylene price has been reduced by 7¢/lb. by both companies now supplying United States markets: Hercules and Italy's Montecatini. Price for natural resin is now 49¢ in truckload quantities.—Hercules Powder Co., Wilmington, Del.; Chemore Corp., New York, N. Y. 70H

New Dacron Type 64 is especially suited to blending with wool. Whereas standard Dacron Type 54 fiber is primarily in tightly constructed fabrics that have little surface nap, Type 64 makes possible the more loosely constructed fabrics. Resistance to pilling is an important area in which the new fiber shows marked improvement.—Du Pont Co., Wilmington, Del. 70I

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about any item in this department, circle its code number on the

Reader Service
postcard (p. 197)

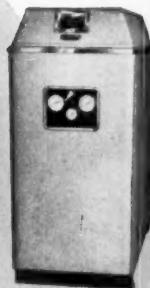
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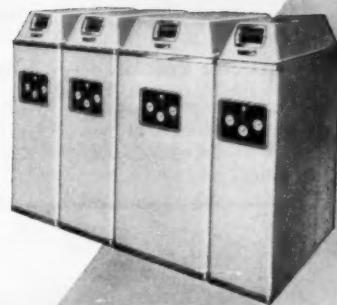
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Automate your metering, batching or blending operation with a Bowser liquid control SYSTEM . . . and get these BENEFITS . . . lower initial investment . . . completely automatic control . . . unsurpassed accuracy . . . increased efficiency . . . single source of supply . . . and system performance guaranteed by Bowser, Inc.



Rate of Flow Controlling System

The Figure 417 Rate of Flow Controller is a completely self-contained system enabling fully automatic and accurate CONTROL of the rate of liquid in flow . . . to better than $\frac{1}{4}$ of 1% accuracy. Handles flow rates from $\frac{1}{2}$ G.P.M. to 250 G.P.M.



Liquid Blending System

The Figure 413 Precision Blending System automatically and accurately blends two or more liquids in closed, continuous production. Accuracy within $\frac{1}{4}$ of 1% and completely automatic operation . . . assures uniform blend . . . reduces blending costs by 50%.

BOWSER METERS AND ACCESSORIES . . . offer complete systems for every type of liquid control requirement



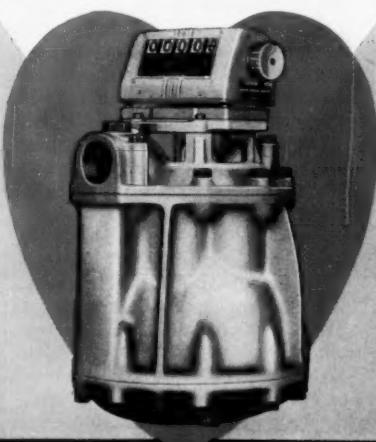
MODEL L . . . straight-reading dial records liquid metered up to 100,000 gallons.



IMPULSE TRANSMITTER . . . transmits electrical impulses to a remote counter which records quantities, controls automatic batching.



MODEL K . . . Printing Dial provides printed records of quantities metered for inventory control, etc.



MODEL F . . . relays voltage signal to a remote flow indicator or controller permitting remote observation and control of the flow rate.



MODEL RP . . . automatically delivers repeated predetermined quantities of liquids.



REMOTE PREDETERMINING COUNTER . . . records electrical impulses from meter permitting automatic delivery and shutoff control for predetermined quantities.

XACTO METER . . . the HEART of Bowser liquid handling systems

Mail to BOWSER, Inc.

1375 E. Creighton Ave., Fort Wayne, Indiana
Please send complete information illustrating the many types of Bowser systems available.

NAME _____
TITLE _____
COMPANY _____
STREET _____
CITY _____ STATE _____

XACTO . . . meters assure precision accuracy. Available in bronze, iron and all stainless steel construction.

Bowser's full line of meters, accessories and controls combine to offer you today's most automatic, economical and modern liquid handling systems.

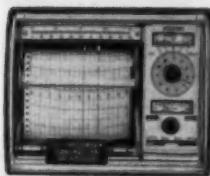
BOWSER
ESTABLISHED 1885

DEVELOPMENTS . . .

PROCESS EQUIPMENT

EDITED BY C. C. VAN SOYE

Latest Developments



Electronic Controls

Manufacturer introduces all components of new line at ISA show. **72A**



Glass Tester

Checks for flaws in surface of glassed-steel equipment. **176A**



Fire Fighter

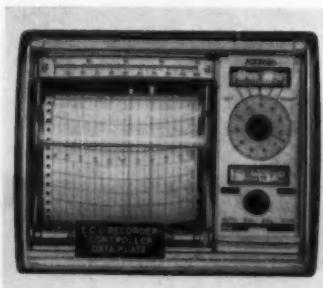
System remotely quenches dangerous blazes. **177A**



Throttling Valve

Incorporates several desirable features. **74A**

Page number is also Reader Service Code Number



Electronic Controls

Feature use of magnetic amplifiers, transistors.

Making its debut just three weeks ago at the Instrument-Automation Conference and Exhibit, Foxboro's Electronic Control Instrumentation line consists of advanced-design transmitters, recorders, controllers and valve operators. Some of the line's features include: use of transistors and magnetic amplifiers; choice of motion-balance or force-balance transmitters; tubeless electrical measurement converters; and modified, semi-graphic control-station design. System explosion-proofing is optional.

In operation, pressure, flow and level measurements, converted at the transmitters to proportional d.c. signals, flow along unshielded lines to the control

center. Converters for emf. and resistance measurements also feed signals to the small-case, panel-mounted receivers. Electrical controllers and final operators complete the loop.

Two-wire installation, narrow elevated ranges and compact construction characterize the force-balance transmitter. The motion-balance instrument provides field indication of measurement plus the opportunity to incorporate alarms, independent of transmitter power supply.

At the control-panel end of the loop, the line's one- and two-pen recorders with 4-in. strip charts offer compact, low-space design. Slide-out chassis with stretch-out cord permits recorder withdrawal without interruption of service. Deflection motors operate directly from the 10-50 ma. transmitted signals to drive the pens. Liquid dash pots limit pen disturbance and insure true average measurement.

Two controller stations are available. Model 62 universal controller has extra-wide adjustment ranges, while Model 61 is a simplified unit with adjustable proportional-plus-reset action especially suited to flow control. Neither unit uses vacuum tubes; both incorporate plug-in subassemblies for simplified maintenance.—The Foxboro Co., Foxboro, Mass. **72A**

Underground Insulation

Cost of underground steam lines cut by new method.

Savings of up to 50% over the cost of constructing buried steam lines by conventional methods are possible with a new system that eliminates need for concrete conduit and manholes. Key to successful application is the use of a compact expansion joint that excludes entry of the insulation material.

Installation procedure is as follows: once the trench is dug and pipe, expansion joints and fittings are laid, the work crew packs the line with a poured-in-place hydrocarbon insulation. As the line heats, the insulation cures to give a three-layer covering—plastic at the pipe, a sintered-consistency middle layer, and outer layer of loose granules.—Badger Mfg. Co., Cambridge, Mass. **72B**

Battery Charger

Vertical units require two-thirds less space.

Saving about two-thirds of the floor space needed by comparable horizontal models, a new, fully-automatic line of battery chargers provides users with a wide choice of electrical ratings. The

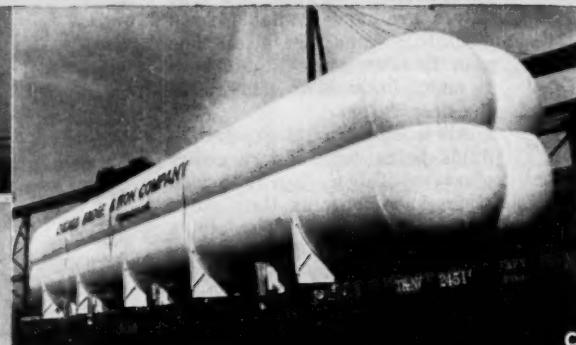
The containment of modern fuels and materials
is both a business and an art with . . .



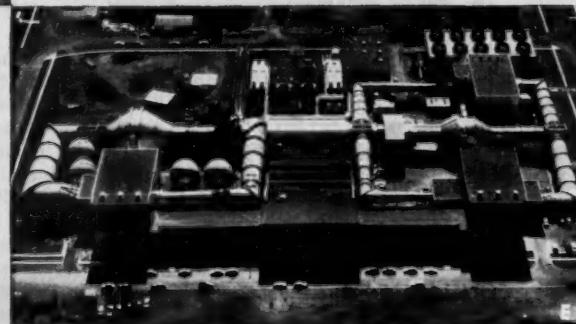
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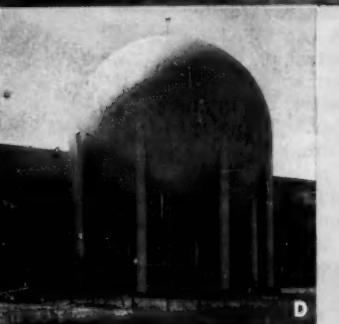
for Creative CRAFTSMANSHIP IN STEEL



C



E



TOP, LEFT—14-lobe MULTISPHERE designed, fabricated and erected by CB&I to store 100,000 gallons of liquid methyl chloride at 150 lbs. working pressure. Design offers optimum versatility for pressure vessels.

A—5052 ALUMINUM was used for these ammonium nitrate storage tanks.

B—LIQUID PROPANE is stored by refrigeration at 1½ lbs. working pressure at minus 44° F in this unique 70-ft. diameter tank, designed and built by CB&I.

C—MULTICYLINDER Multi-lobe pressure vessels such as this offer advantage of high pressure storage where space is limited. Vessel is designed for 250 lbs. working pressure.

D—VACUUM SERVICE is provided by Hortonsphere® at a University of Toronto wind tunnel installation.

E—TUNNEL SECTIONS for wind tunnel were fabricated and erected by CB&I. A supersonic wind tunnel for Convair Division of General Dynamics was recently completed by CB&I as a "turnkey" project.

PRESSURE VESSELS • REFRIGERATED STORAGE • VACUUM SERVICE • HORTONCLAD® •
ENGINEERING • FABRICATION • ERECTION IN ALL METALS AND COMBINATION METALS

Chicago Bridge & Iron Company

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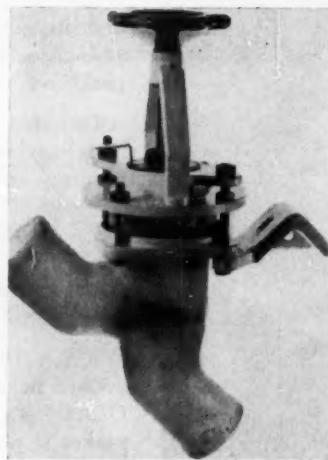
Plants in: BIRMINGHAM, CHICAGO, SALT LAKE CITY, GREENVILLE, PENNSYLVANIA and at NEW CASTLE, DELAWARE
In Canada: HORTON STEEL WORKS LTD., TORONTO, ONTARIO

Representatives and Licensees: Australia, Cuba, England, France, Germany, Italy, Japan, Netherlands, Scotland



vertical motor-generator sets, also adaptable to off-floor mounting, feature parts standardization and simplification of design to produce substantial maintenance economies.

The units come in four different physical sizes, with a choice of 25 different ratings varying from 0 to 800 amp.-hr. Having 2-, 3- and $7\frac{1}{2}$ -hp. ratings, the chargers operate from a 2- or 3-phase, 60 cycle source at 220, 440 or 550 v.—Exide Industrial Div., Electric Storage Battery Co., Philadelphia, Pa. 72C



All-Glass Valve

Handles acidic fluids, all concentrations to 250 F.

Recommended for processing all acidic metallic salts, various crystalline slurries and all acids other than hydrofluoric and raw phosphoric, all-glass Y-type valves are now available from stock in 1½- and 2-in. sizes. The manufacturer plans to add both 1- and 3-in. sizes to the line in the near future.

All working parts exposed to fluids being handled are either glass or Teflon. Spring-loaded stems keep the plug tight when closed. For additional safety, a fiber glass sleeve forms a protective armor over the tempered glass body.

Low thermal expansion of the borosilicate glass allows sudden temperature differentials as high as 200 F. Maximum working temperature is 250 F.; maximum line pressure is 50 psi.—Corning Glass Works, Corning, N. Y. 74B

Throttling Valve

Oil-tool firm introduces valve for process use.

Ideal for accurate liquid or gas control, a new high-pressure throttling valve comes in sizes from 1 to 6 in. with flanged or threaded connections. Pressure ratings for all sizes vary to 10,000 psi. Automatic actuation by hydraulic or air pressure is available as an accessory for all valves.

Featuring outside threads for corrosion resistance, and a stem that locks at any setting, the valve also has a pointer and calibration plate to indicate orifice opening. Tapered throats give a venturi effect that results in excellent flow characteristics.

Several interchangeable tips provide service versatility: conical, micro tip (for linear change of orifice area), thermo tip (tip has internal heating element), and hardened tip for abrasion service. — Shaffer Tool Works, Brea, Calif. 74A

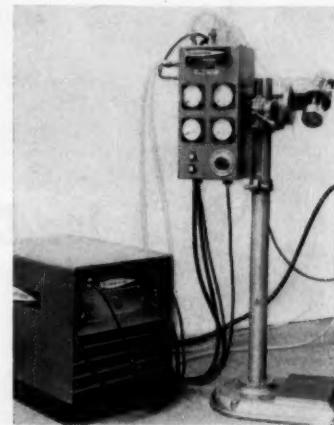
Conveyor Scale

Pneumatic signals automate flow control.

Adaptable to either fixed- or variable-speed conveyors, a new unitized, pneumatic scale is available in a variety of sizes to handle a large range of capacities. Used in conjunction with the manufacturer's other weighing components, the scale can indicate, record, totalize, propor-

tion or program material flow rate. Pneumatic signals from a transmitter control operation.

Unit installs easily on existing flat-belt or trough-type conveyors with a minimum of downtime and only slight conveyor modification. Instead of knife edges, pivots or bearings, the new scale employs a flexural frame arrangement. This eliminates all effects of side thrust and eccentric loading on the conveyor, delivering a single component of force. — Weighing & Control Components, Hatboro, Pa. 74C



Plasma Producer

Resultant temperature can vaporize any element.

Designed for creating and sustaining temperatures in excess of 22,000 F., the Plasmatron may prove to be a valuable new tool for research and, eventually, for production. A controlled jet of electrically neutral, partially ionized gas forms on passage through an electric arc in an enclosed chamber. Transfer of energy in the arc, accelerated by thermal and magnetic "pinch" effects, results in random motion among the ions and electrons, thus causing intense heat generation and the resultant high temperatures.

Plasmatron systems come in various power levels from 12.5 to 160 kw.—Giannini Plasma-dyne, Santa Ana, Calif. 74D

Glass Tester
and other equipment news
on page 176.

BIG-DIAMETER PLASTIC PIPE?

YES...PLASTIC PIPE

FOR YOUR PLANT UP TO 8"

IN DIAMETER IS NOW AVAILABLE MADE FROM

A-C POLYETHYLENE PIPE COMPOUND.

Now your plant can realize the advantages of plastic piping in large-diameter sizes as well as small. Plastic pipe—light, flexible, long lasting—can now be made up to 8" or more in diameter...with A-C Polyethylene Pipe Compound, the ultra-high-molecular-weight polyethylene.

More than 200,000 feet of this new pipe are already in use in chemical plants. Reports indicate substantial savings in installation, compared with metal pipe. Projected maintenance costs are phenomenally low. Unlike pipe made from conventional polyethylene, this new piping is completely free of stress cracking, splitting or pinholing. It has exceptional resistance to temperature variation, abrasion and corrosive chemicals.

The great strength of polyethylene pipe makes it ideal for maintenance applications. The smooth bore reduces flow resistance and prevents accumulation of deposits. How strong is it? In a typical test involving sudden surges of pressure, this pipe has withstood surges from 100-300 pounds per square inch for more than 90,000 cycles without failing.

Sample lengths available to those who

Clip Coupon
to company letterhead.

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PETROCHEMICAL
DIVISION**

40 Rector Street, New York 6, N.Y.

ADVANTAGES of piping made with A-C Polyethylene Pipe Compound

Extraordinary chemical resistance. Withstands acids, alkalies, salts and detergents. Pure and inert for use with potable water.

Long service life. Will not rot, rust or corrode. Impervious to electrolytic environment. Good weather resistance.

Easy installation. Much lighter in weight than metal (about $\frac{1}{6}$ the weight of steel). Long lengths readily joined by flanging, welding or Victaulic fittings.

No stress cracking. The only plastic pipe completely free from environmental stress cracking. Impact resistance of pipe compound is 13 ft-lb/in notch.

Surge resistance. Withstands pressures from 100-300 psi for over 90,000 cycles.

Good heat resistance. Greater resistance to temperature variation, hot or cold, than any comparable material.

Low cost. Below that of any metal pipe.

**Allied
Chemical**

BUILT-IN ASSURANCE

To Help Make Your Plans Work As Specified...

F-M BUILTOGETHER CENTRIFUGAL PUMPS

hot and cold liquids
liquid circulation
low-viscosity liquids
boiler feed
cooling towers, etc.



Up to 900 gpm., pressures to 525 ft. Close-coupled pump and motor units mount horizontal, vertical or angular. Sizes $\frac{3}{4}$ " through 5".

F-M NON-CLOG PUMPS

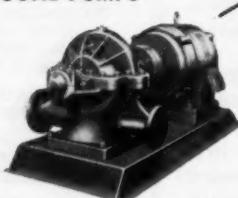
plant waste
slurries
paper stock
fruit
fish
vegetables, etc.



Up to 30,000 gpm., pressures to 175 ft. Sizes 2" through 20". Vertical or horizontal. Bladeless or conventional.

F-M SPLIT-CASE CENTRIFUGAL PUMPS

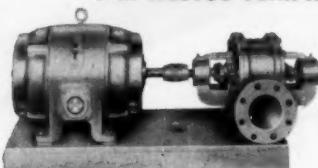
water supply; plant service
booster; circulating
air conditioning
refrigeration
chemical liquids
boiler feeds, etc.



Up to 50,000 gpm., pressures to 700 ft. Sizes $1\frac{1}{2}$ " through 36". Single stage or multistage.

For full information about Fairbanks-Morse pumps, call your F-M Sales Engineer or write F-M Sales & Co., 600 S. Michigan Ave., Chicago 5, Ill.

F-M WESTCO PERIPHERAL PUMPS



boiler feed
condensate return
hot and cold liquids
chemicals
refrigerants, etc.

Up to 200 gpm., pressures to 900 ft. High pressure at normal operating speeds. Handle widely varying heads with little change in capacity. Sizes $1\frac{1}{4}$ " through $2\frac{1}{2}$ ".

The best-laid plans can go astray when mechanical equipment fails to deliver according to expectations or fails to give sustained peak performance. That's why Fairbanks-Morse builds something extra into all pumps so your plans work as specified.

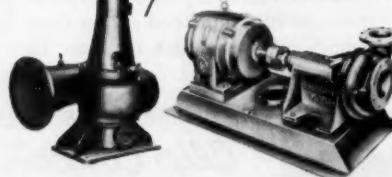
F-M PUMPS You Can Rely Upon

Full-rated capacity guaranteed...with built-in safety margin to assure maximum efficiency under most severe use. Rugged, durable, precision-made to maintain efficiency with minimum service.

Expert Help When You Want It

F-M Engineers are ready to work with you on any of your pump problems.

F-M END-SUCTION PUMPS



hot and cold liquids
chemicals
circulating liquids
low-viscosity liquids
cooling towers
condenser circulation, etc.

Up to 100,000 gpm., pressures to 250 ft. Sizes $\frac{3}{4}$ " through 54". Horizontal or vertical.

FAIRBANKS-MORSE

a name worth remembering when you want the BEST

PUMPS • SCALES • DIESEL LOCOMOTIVES AND ENGINES • ELECTRICAL MACHINERY RAIL CARS • HOME WATER SERVICE EQUIPMENT • MAGNETOS



WHAT PROPERTIES DO YOU NEED IN VINYL PLASTICS?

Build them in with FLEXOL plasticizers!

The many different end uses for vinyl plastics each demand special properties. Each of CARBIDE's 15 FLEXOL plasticizers is designed to contribute one or more distinctive properties. Our technical representatives can help you select the plasticizer that will do your job best!

FLEXOL plasticizers DOP, 426, and 810 are designed to give an excellent balance of properties—good compatibility, low volatility, low-temperature flexibility, and superior electrical qualities. Other FLEXOL primary plasticizers have specialized properties. FLEXOL 10-10 possesses low volatility and good extraction resistance; FLEXOL 380 imparts outstanding lacquer mar resistance; and FLEXOL CC-55 has good viscosity characteristics and excellent fusing action in plastisol.

For vinyl plastics that must perform at extremely low temperatures, there are three special plasticizers, FLEXOL A-26, 10-A, and TOF. These are used to make vinyl plastics that are both impact resistant and flexible at temperatures as low as -70°C .

In some cases, CARBIDE has developed a plasticizer for a single use. For example, FLEXOL Plasticizer 3GH is used for the polyvinyl butyral interlayer in safety glass. This plasticizer increases adhesion and eliminates the need for edge sealing. Besides FLEXOL 3GH, CARBIDE produces six other special-purpose plasticizers, FLEXOL 3GO, 4GO, 8N8, R-2H, and B-400.

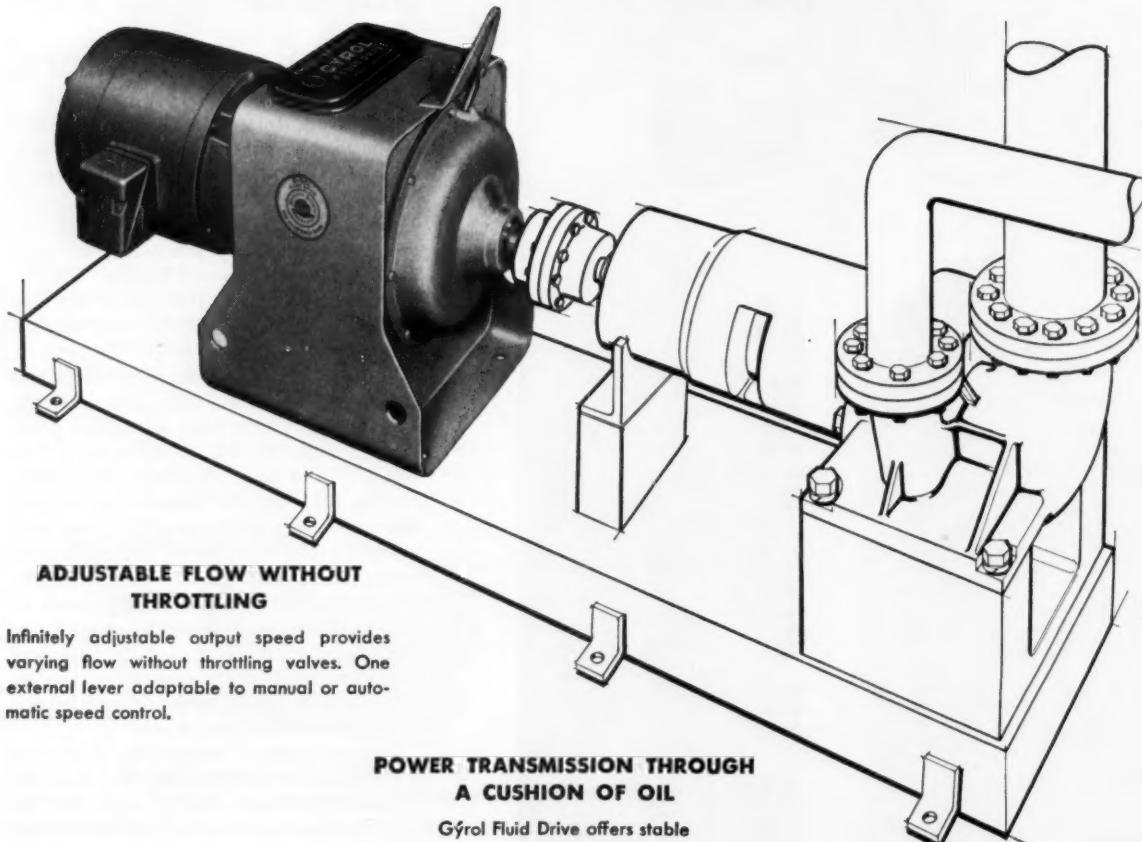
All 15 FLEXOL plasticizers are available from distribution points throughout the country. And, because of CARBIDE's wide variety of plasticizers, you can take advantage of the savings from combination tank car, tank wagon, and drum orders in LCL or carload orders. For more information on FLEXOL plasticizers, call the nearest CARBIDE office or write Department B, Union Carbide Chemicals Company, Division of Union Carbide Corporation, 30 East 42nd Street, New York 17, New York.

UNION CARBIDE CHEMICALS COMPANY

DIVISION OF  CORPORATION

"Flexol" and "Union Carbide" are registered trade marks of UCC.

American Blower Gyrol® Fluid Drive makes pumps more productive!



ADJUSTABLE FLOW WITHOUT THROTTLING

Infinitely adjustable output speed provides varying flow without throttling valves. One external lever adaptable to manual or automatic speed control.

**POWER TRANSMISSION THROUGH
A CUSHION OF OIL**

Gyrol Fluid Drive offers stable speed control unaffected by wear.

Fact is, a Gyrol Fluid Drive can benefit any process requiring adjustable control of pump flow and pressure.

By providing *stepless speed control* without wasteful throttling, it reduces power consumption and pump work-load, keeps maintenance costs to a minimum. The problem of handling liquids at varying viscosity and density is greatly simplified.

With no mechanical connection between driving and driven shafts, adjustable speed is obtained without friction or wear. The smooth cushion of power-transmitting oil protects both driving and driven machines from shock. Torque-limiting capacity guards against overload.

Any standard pump driven by a constant-speed motor can be equipped with Gyrol Fluid Drive. Type VS, Class 2 Unit (shown here) comes in a complete range of sizes from 1 to 800 hp. Other designs handle up to 12,000 hp. So if you want to save power and reduce equipment and maintenance costs on pumping jobs that involve varying capacities . . . consider American Blower Gyrol Fluid Drive.

For full information, contact one of our 73 branch offices. Or write: American-Standard,* American Blower Division, Detroit 32, Michigan. In Canada: Canadian Sirocco products, Windsor, Ontario.

*AMERICAN-STANDARD and Standard® are trademarks of American Radiator & Standard Sanitary Corporation.



AMERICAN-STANDARD

AMERICAN BLOWER DIVISION

YEAR 'ROUND BONUS!

You Get More Than Just a
Valve When You Buy BS&B's

Super 70

Specification of BS&B Super 70 Diaphragm Control Valves on your next job will assure you of getting all of the following:

1. High Quality Product . . . The BS&B Super 70 Diaphragm Control Valve has high efficiency and stability. In addition to thousands of hydraulic flow tests performed in the laboratory, analysis of operating data gathered from Super 70's on stream in customer plants substantiate their excellent performance.

2. Application Engineering . . . Today's complex processing problems require detailed analysis to determine proper instrumentation and control applications . . . accurate control valve sizing. This is a regular service to Super 70 customers.

3. Start-up Assistance . . . After helping customers select the right valve for a specific job, BS&B follows thru by assisting at plant start-up time.

4. Time-saving Scheduled Maintenance . . . With the patented clamp ring—float ring closure, valve maintenance can be done in a fraction of the time required by conventional type valves . . . an economic must in future valve specifications.

Clamp Ring —
Float Ring Closure

Flanged —
Gasket Closure



BS&B Super 70 Valves are available in either clamp ring—float ring, sealed bonnet or flanged-gasketed body closures. Whichever type you choose, when they're "on stream" you'll know that they're exactly right for the job.

Call your nearest BS&B office or representative now to discuss your present and future valve requirements. Or if you prefer, write for detailed information.

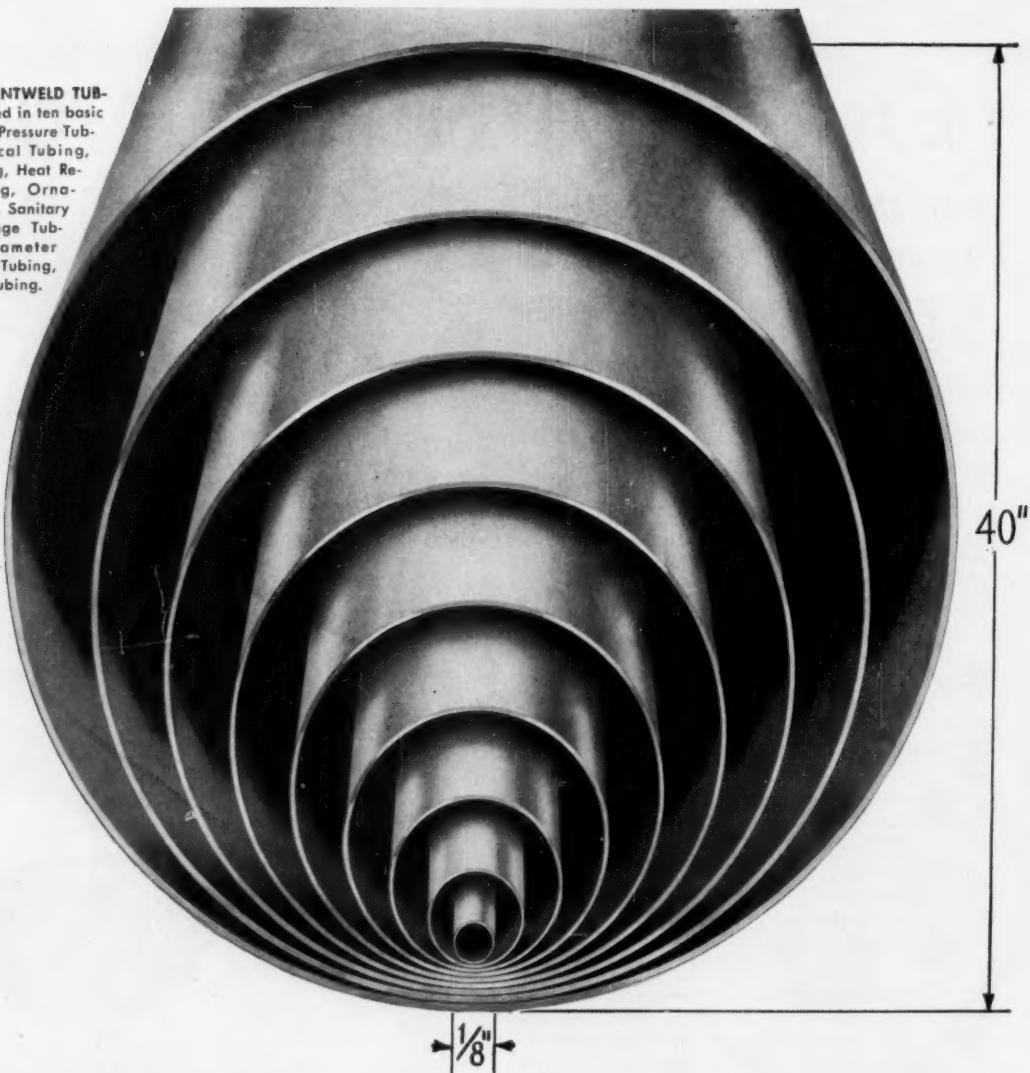
BLACK, SIVALLS & BRYSON, INC.

7500 East 12th Street

Controls Division, Dept. 4-N10

Kansas City 26, Missouri.

CONTOUR TRENTWELD TUBING is furnished in ten basic classifications: Pressure Tubing, Mechanical Tubing, Aircraft Tubing, Heat Resistant Tubing, Ornamental Tubing, Sanitary Tubing, Beverage Tubing, Large Diameter Tubing, Shaped Tubing, and Formed Tubing.



TRENTWELD tubing is equal in strength and has more uniformity than tubing made by any other method of manufacture

Trent offers tubing in sizes ranging from $\frac{1}{8}$ " to 40" O.D. and in a wide range of grades. These include: Hastelloy,* Zirconium, Zircaloy, Titanium and 19-9-DL grades. All are made by an exclusive welding process—Contour Trentweld®—which virtually eliminates the bead. Furthermore, by cold working and annealing after welding, Trent makes the weld equal in strength and corrosion resistance to the parent metal.

To insure that Trentweld tubing

is of the highest quality attainable, a rigorous quality control program is carried out. Samples of each lot are tensile tested. Periodic tests—flattening, reverse bend, flare and flange, coil, and pressure—are conducted. Rigid corrosion tests are made on all lots intended for corrosive applications. When requested, a unique "single-wall" X-ray inspection is made as your final assurance of a sound, uniform product.

Why not take advantage of Trent

quality when you order stainless or high alloy tubing? For further information, write for the Trent tubing handbook, Trent Tube Company, East Troy, Wisconsin.

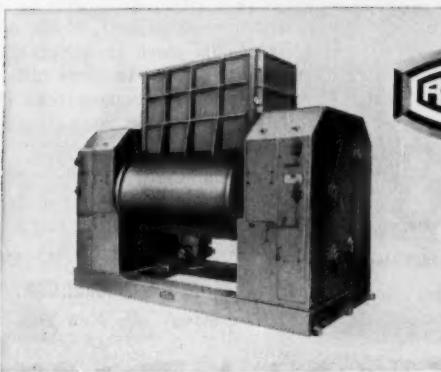
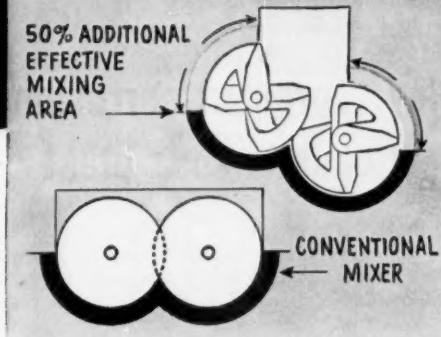
*Trademark of Haynes, Stellite Co.

**CONTOUR
TRENTWELD**

**TRENT
TUBE
COMPANY**

Subsidiary of Crucible Steel Company of America
GENERAL OFFICES: EAST TROY, WISCONSIN
MILLS: EAST TROY, WIS.; FULLERTON, CALIF.

take this unique
design...
PRESTO!
a much
faster mix!



Whatever the mixing job: a READCO mixer!

with Readco's unique split-level bowl:
complete dispersion, shorter cycle, lower cost

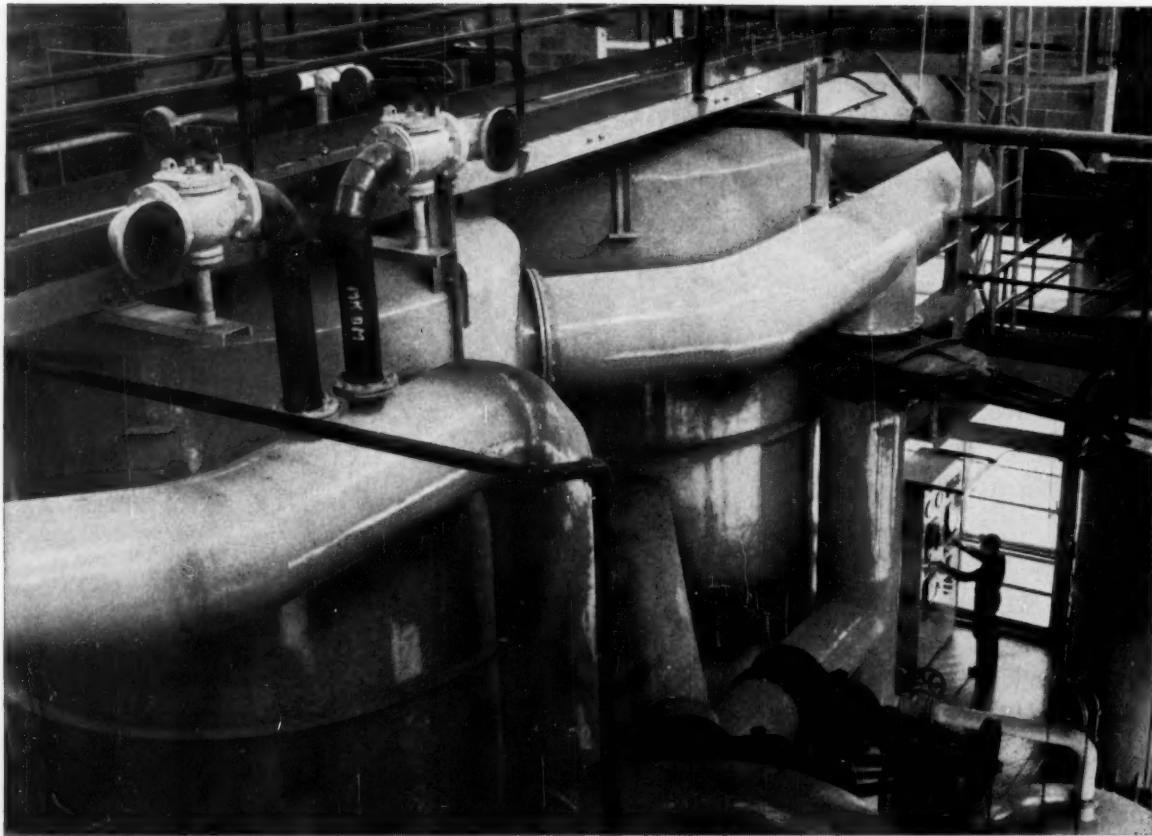
The special design of this Readco mixing bowl provides a 50% greater effective mixing area. Overlapping sigma arms operate at minimum clearance from the shell, prevent build-up of materials, speed dispersion. The design also permits maximum heat transfer from the jacket.

You'll get complete dispersion, consistent mixing, in substantially shorter cycles. Working capacities range from 150 to 900 gallons. Write for complete information.

READ STANDARD

York, Pennsylvania

A Division of
Capitol Products Corporation



Evaporator bodies and vapor piping at the new \$12 million chlorine-caustic soda plant of Hooker Chemicals Limited, No. Vancouver, B. C., are made of solid Nickel and

Lukens Nickel-clad steel to guard against caustic corrosion, to assure product purity. Much of the equipment was supplied by Puget Sound Fabricators Inc., Seattle, Wash.

"Bodyguards" . . . Nickel, Monel alloy . . . prevent corrosion, metallic pick-up at Hooker's new caustic soda plant

To prevent caustic corrosion . . .

To safeguard product purity . . .

These are the principal reasons why Inco Nickel and Monel* nickel-copper alloy are used in the new

chlorine-caustic soda plant of Hooker Chemicals Limited.

Equipment made of corrosion-resistant Inco Nickel and its alloys frequently gives more than a decade of

service in handling strong caustic. Equally important, Nickel equipment has enabled producers to make millions of tons of caustic a year with less than 100 ppm of metallic impurities.

It will pay you to specify equipment of Inco Nickel, Monel alloy or Nickel-clad steel. Inco Nickel Alloys can be obtained in most mill forms right from warehouse stocks. (Listed under "Nickel" in your classified directory.)

Get complete technical data and service records. Write for "The Resistance of Nickel and Its Alloys to Caustic Alkalies."

*Registered trademark

The INTERNATIONAL NICKEL COMPANY, Inc.
67 Wall Street  New York 5, N. Y.

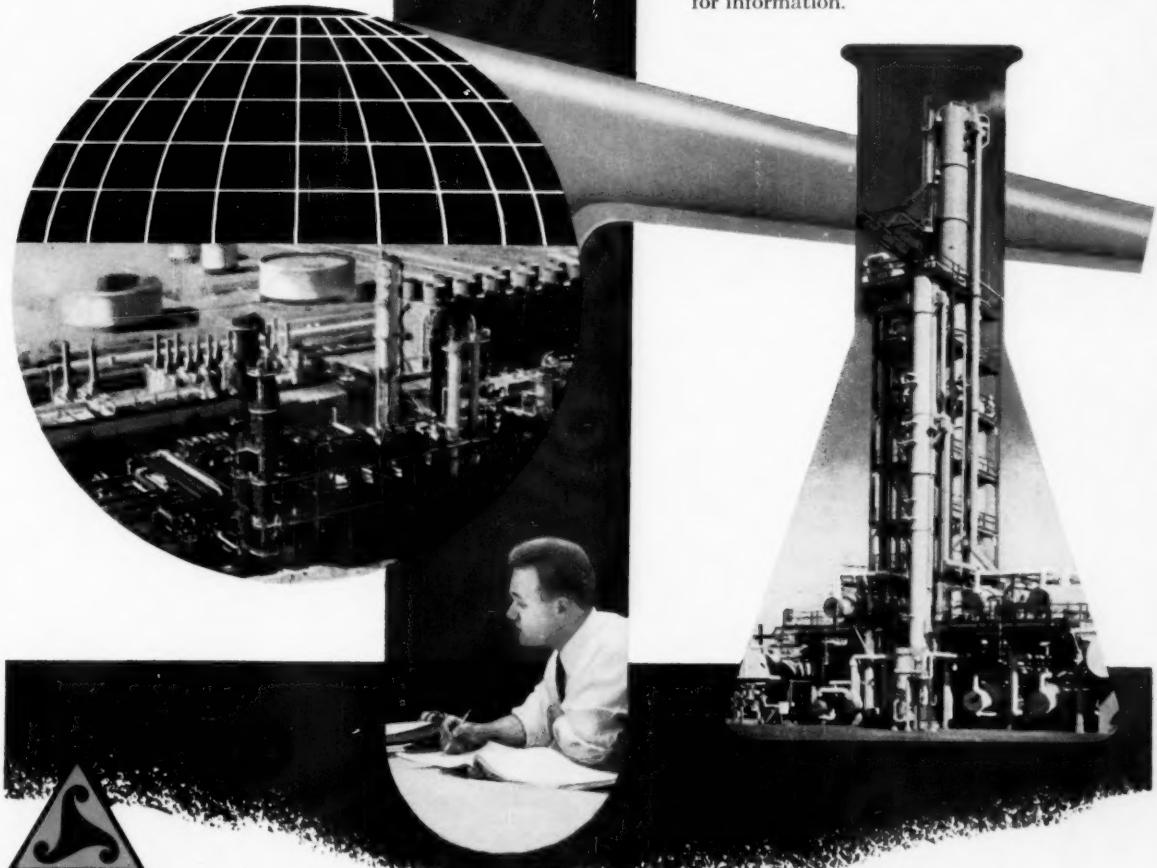
See how Nickel and Monel alloy are used in Hooker's new chlorine-caustic plant equipment

EQUIPMENT	MATERIAL	EQUIPMENT	MATERIAL
Caustic Tank	Nickel-clad steel	Salt receiver tanks	Nickel
Evaporator body	Nickel	Salt separator tanks	Nickel
Second effect vapor body	Nickel-clad steel	Barometric condenser	Monel alloy
Third effect vapor body	Nickel-clad steel	Cylinder coolers	Nickel-clad steel
		Cooling coils	Monel alloy tubing

INCO NICKEL ALLOYS

October 6, 1958—CHEMICAL ENGINEERING

The world is our workshop



Stone & Webster Engineering Corporation has provided Surveys, Reports, Appraisals, Process Engineering and Design, Procurement of Equipment and Materials, and Construction for process industries located in many countries in the world.

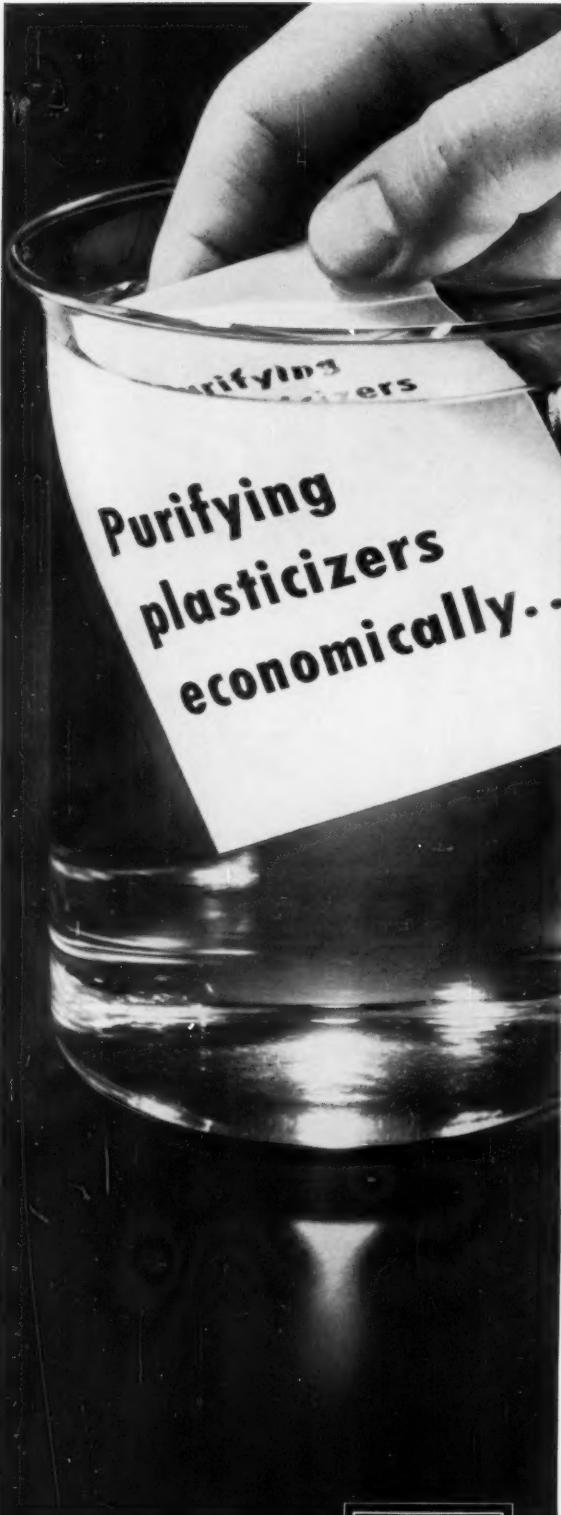
The services of this world-wide organization are available for any process problem from the engineering phases of a single unit to the design and construction of a complete project, including all related facilities such as steam, power, refrigeration, air conditioning, water supply, fire protection and waste disposal.

Stone & Webster's versatility and experience have helped both large and small companies reduce their construction and operating costs on many types of process plants. This integrated organization is ready to assist you with the planning of your project . . . economical design and construction . . . and completion on schedule. Write or call us for information.

STONE & WEBSTER ENGINEERING CORPORATION

AFFILIATED WITH STONE & WEBSTER ENGINEERING LIMITED (LONDON)

New York Boston Chicago Pittsburgh Houston San Francisco Los Angeles Seattle Toronto



Purifying
plasticizers
economically..

with **DARCO®**
Activated Carbon

Decolorizing a valuable chemical often poses the problem of keeping all the chemical while you get rid of all the color. That's when the low product retention of DARCO Activated Carbon pays dividends.

Take the case of organic plasticizers for use in clear coatings, cements, plastics and other transparent products. Producers found that they could cut plasticizer loss in the filter cake in half by using high density DARCO—a decisive saving where the non-water-soluble chemical is tough to recover from the filter cake. And DARCO's high adsorptive efficiency adds low cost to high yield, making it economically attractive for clean-up jobs on many chemicals.

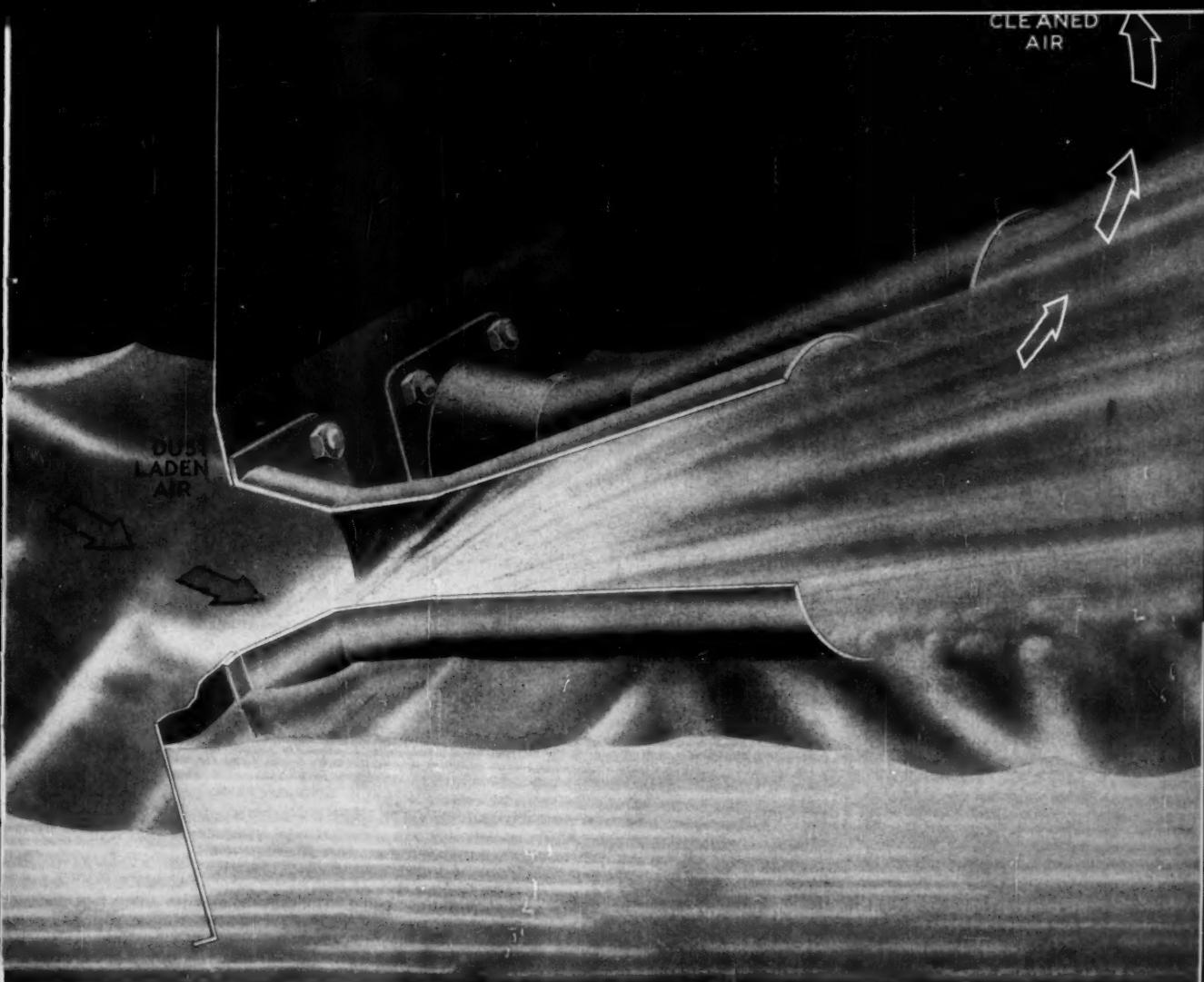
DARCO has been helping chemical manufacturers with purification for over 35 years. Chances are your problem is one it has already tackled—removing undesirable color bodies, odors, colloids, floc-precursors, or causes of haze or foam. On these . . . or on applications you may have just dreamed up . . . you can profit from our extensive know-how in adsorption. Call or write us today for data, samples or a consultation.



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ATLAS CHEMICALS DIVISION
ATLAS POWDER COMPANY
WILMINGTON 99, DELAWARE

In Canada: Atlas Powder Company, Canada, Ltd.
Brantford, Ontario, Canada



Puts the squeeze on difficult dusts

**Pangborn Ventrijet Wet Dust Collector uses
exclusive venturi tubes for peak efficiency**

Pangborn Ventrijet Wet Dust Collector on the job. This is just one of Pangborn's comprehensive line of wet and dry dust collectors.

That pinch-necked venturi tube is the secret behind Pangborn Ventrijet performance. As dust-laden air flows through these tubes, the constriction creates a low-pressure area which draws water into the air stream. The resulting turbulence breaks the water into particles which actually *wash* the dust from the air. The simplicity of Ventrijet design saves money in its ease of installation, its low cost of operation and maintenance.

Although the Ventrijet is particularly suited to collecting hot, moist, inflammable, corrosive and obnoxious dusts, the Pangborn engineering it typifies is important to any dust-producing

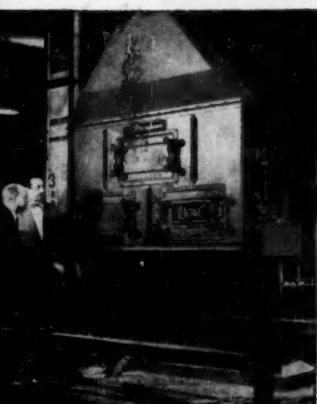
plant. It is not enough to put a dust collector within a plant. An efficient dust control system must be *scientifically* planned, designed and constructed to handle effectively a specific dust problem. This thinking is incorporated into every Pangborn proposal.

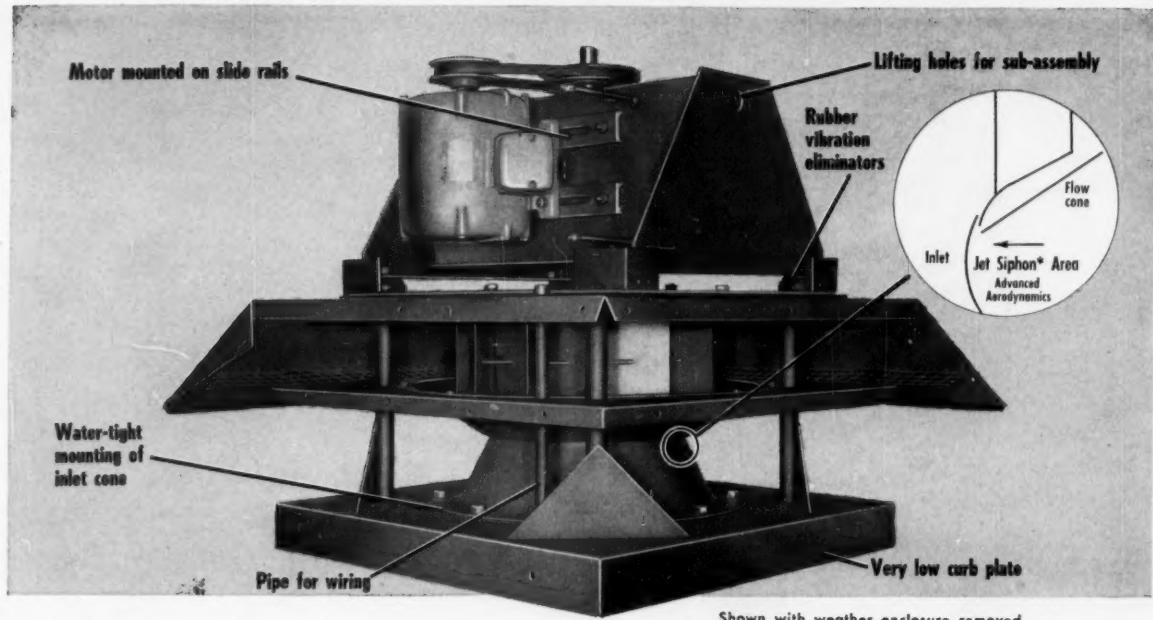
The Pangborn Engineer in your area will be glad to go to work for you. He is a dust expert and will discuss your individual problem at no obligation. And, for more information, write for Bulletin 922 to: Pangborn Corp., 2600 Pangborn Blvd., Hagerstown, Md. Manufacturers of Dust Control and Blast Cleaning Equipment.



Pangborn

CONTROLS DUST





PLUS VALUES... all yours in the Clarge Centrilator

POWER ROOF VENTILATOR — CENTRIFUGAL TYPE

Jet Siphon* feature for stable, high efficiency.

Static pressures to 2" — thus well suited to both light-duty installations without ductwork and applications where ductwork or hoods impose considerable resistance.

Adaptable to a wide range of motor sizes.

Variable pitch V-belt drive.

Wheel and inlet designed for streamlined air flow.

Built heavy-duty throughout to assure long-lasting, trouble-free service.

Every wheel statically and dynamically balanced on precision machines.

Inspection panel and complete accessibility.

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Venting of motor and drive area.

Engineered and constructed for extra quietness.

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Simple installation — only 4 bolts required.

Write today for Bulletin 550. Clarge Fan Co., Kalamazoo, Mich.

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*Patent applied for

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for low cost
purification and drying
of hydrogen and
other gases



The Deoxo Catalytic Purifier is combined with an extremely efficient automatically operated drying unit to provide oxygen-free hydrogen that is ideally pure and dry. The combined units are identified as the Deoxo Dual Puridryer. It supplies hydrogen with less than one part oxygen per million — dried to a dew point of -100°F . No inert gas purging is needed. The Deoxo Dual Puridryer can also be used with other gases such as: Nitrogen, Argon, Helium and saturated hydrocarbons, with equally fine performance. Write for descriptive literature.

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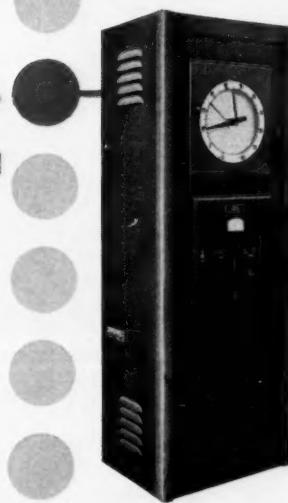
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traces of molecular
oxygen in gases



In metallurgical and chemical processes requiring an oxygen-free atmosphere, the Minoxa Indicator provides a means of insuring that failure of purification or ingress of atmospheric oxygen through an unsuspected leak does not cause costly spoilage. The ranges covered are 0-10 and 0-100 ppm. High sensitivity and rapid speed of response recommend its use for both laboratory investigation and production quality control in a wider range of applications.

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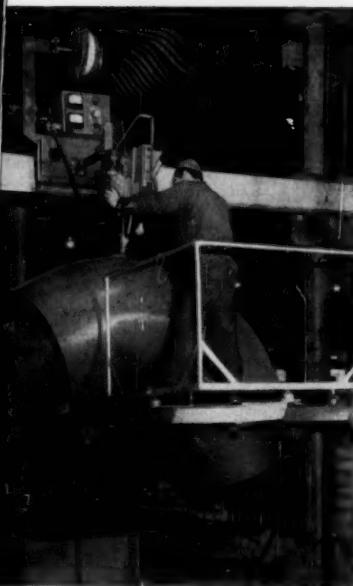
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Special gauges and instruments are used to make sure that we have complied with the extremely close tolerances often required on stainless fittings. Here wall thickness and concentricity were held within extremely close limits throughout the fittings.

The exclusive Midwest method of manufacture—much more versatile and flexible than any other—enables us to make almost any type of special welding fittings to the most rigid specifications. Midwest makes welding fittings from plate . . . usually much easier to get than pipe, particularly if the material is special. That expedites delivery. Closer tolerances are inherent in the Midwest process, and quality control is always beyond code requirements.

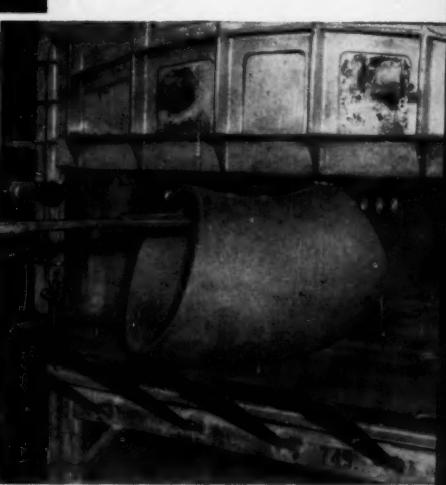
Even if you use only standard fittings, the exceptional quality of Midwest fittings can be important to you. Ask your Midwest distributor or write us for new Bulletin 5801.



36" O.D. 90° elbow with 16" tangent on one end being welded by an automatic submerged arc machine. Material is A-201 carbon steel.



Stainless-clad elbows undergoing ultrasonic inspection to check bonding of material and quality of weld. Since plate is often the only form in which clad material is available, the Midwest process is able to produce the most comprehensive range of clad fittings—and to do so promptly.



Special 24" x 21" 45° reducing elbow made of 1" thick 1 1/4% chrome 1/2% moly steel ready for heat treating furnace.

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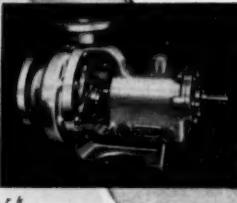
*Pump Buyers are saying this
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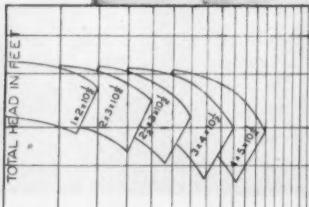
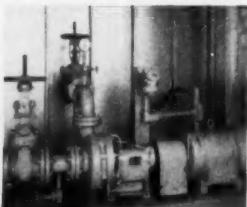
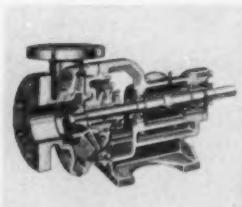
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THEY OFFER the type of quality construction that measures up to any standard. Continual checking at every stage of manufacture guarantees the buyer performance he can count on in the field. *The best!*

THEY PROVIDE the performance you expect and pay for, backed by actual operating records of Peerless pumps in installations like yours. Durability, dependability, efficiency—all proved in service.

THEY MEET exactly every pumping requirement, handle any job in your system that calls for a pump. The complete Peerless range offers all types of chemical process pumps, in all sizes and frames.

AN EXAMPLE of Peerless research is this recently released bulletin on the effects of radial loads in process pumps, "MECHANICAL CONSIDERATION IN PUMP DESIGN." Request Bulletin No. EM-79.



Largest New Cooling Tower Installation Is Fungus-Proof

The recent installation of 40 fan cells of Marley Double-Flow cooling towers at one location is outstanding in capacity and in pre-determined durability, too, because every foot of the 1,715,000 board feet of lumber used was MARLITH pressure protected after fabrication.

This huge installation highlights industry's growing concern over the greatest hazard to cooling tower service — FUNGAL DECAY. MARLITH treatment is a most positive and economical step to prevent the destructive action of fungi — a hazard the country and the world over. The efficacy of MARLITH treatment has been proved conclusively in hundreds of laboratory and field tests in many parts of the world.

There can be no question that the accumulated costs of maintenance and down time for an unprotected cooling tower will, over the years, far exceed those of a MARLITH-treated tower. Most important, MARLITH treatment assures for the future an adequate supply of cold water at an efficient operating temperature — a factor virtually as important as your basic materials supply.

If water conservation is in your development plans (it's good business for you, your neighbor, your country), you'll find it profitable to get full information from your Marley engineer on MARLITH — the "life insurance" for your cooling towers. Just ask him or write for Marliit Bulletin M-58.

MARLITH IS A REGISTERED TRADE NAME OF THE

The Marley Company Kansas City, Missouri



Pointer oscillation only a minor reason for dampening of industrial thermometers

It is generally assumed that industrial thermometers are silicone damped solely to prevent pointer oscillation when used on vibrating equipment. True, the prevention of pointer oscillation is necessary, but actually there are several far more important reasons for the use of silicone dampening fluids.

The primary reason for dampening bimetallic dial thermometers is to preserve accurate calibration, especially on the lower temperature ranges where a thinner bimetal element is used. An undamped bimetal element, when subjected to shock or severe vibration, would have a tendency to unwind slightly, throwing the instrument out of calibration. To prevent this, thermometers are damped by covering the bimetal element with silicone fluid. The silicone provides permanent protection for the critical bimetal element, holding the coil in place and preventing any unwinding or shifting action. This dampening, of course, also prevents pointer oscillation, eliminating difficult readings. But the primary reason for silicone dampening is to help maintain calibration accuracy, and it is therefore quite important to *all* industrial thermometer users.



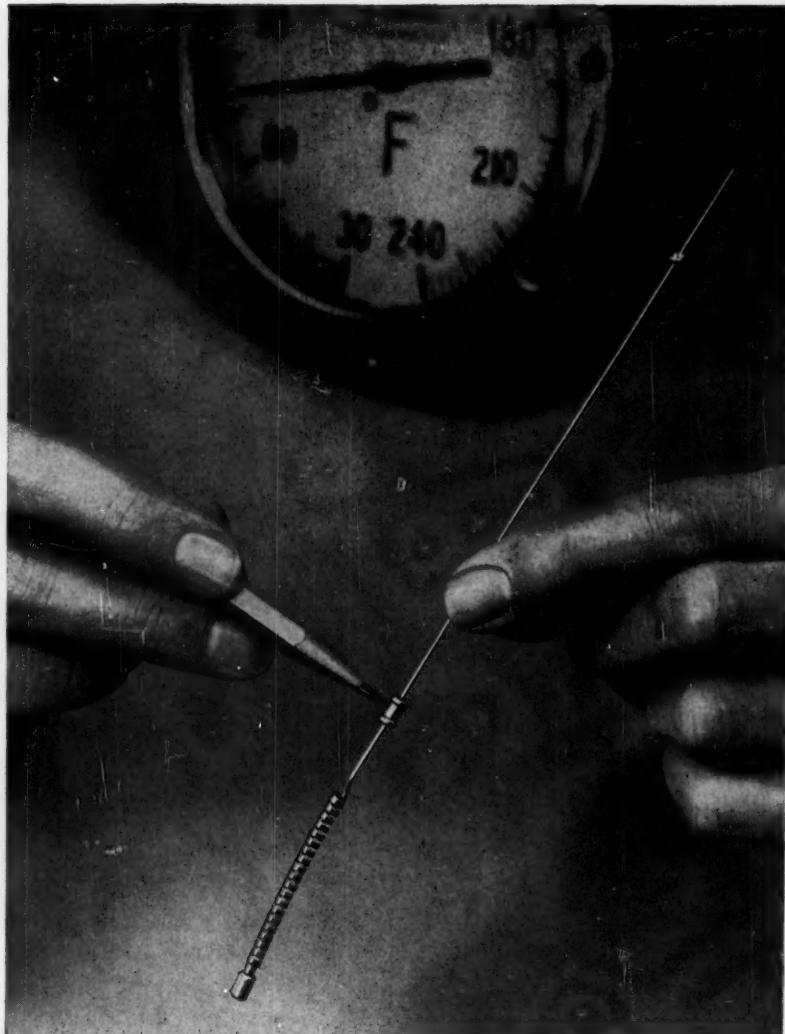
The RMC thermometer in this photograph is constantly subjected to extreme vibration. It is installed on a two-stage Synthesis Gas Compressor in Atlantic Refinery's Philadelphia Synthetic Ammonia Plant. Only a completely damped thermometer could maintain its accuracy under such conditions.

There is more, however, to the full dampening story. Rochester Manufacturing Company carries this dampening procedure one step further with a specially designed bearing which further dampens both the shaft and coil. It also serves as a better guide for the bimetal shaft to keep it perfectly aligned within the tube. RMC is the only manufacturer using this type of dampening bearing at the present time.

RMC offers compensated electrical remote-reading liquid level indicator

A double coil movement in the RMC electrical, remote-reading liquid level indicator compensates for voltage changes. Silicone damped and hermetically sealed.

Write, wire or phone—tell us your requirements for indicating instruments, and let RMC engineering skill go to work for you. ROCHESTER MFG. CO., 113 Rockwood St., Rochester 10, N.Y.

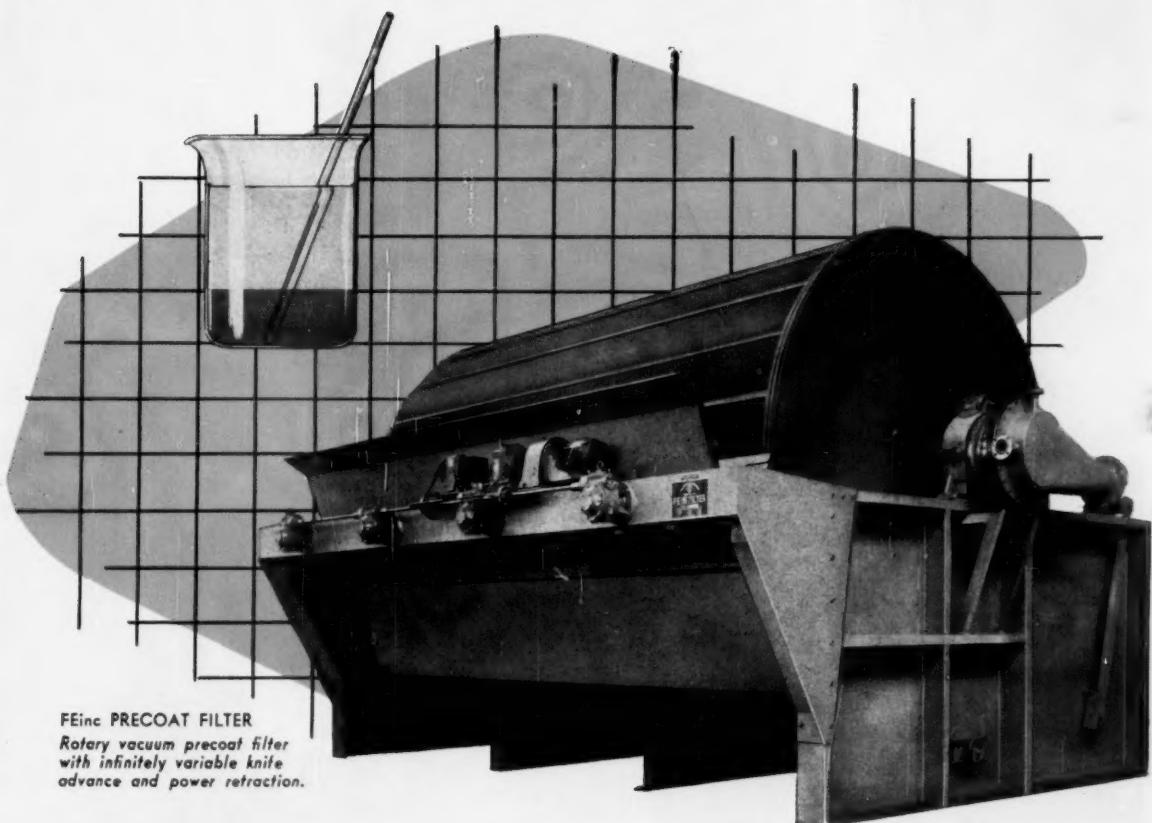


This special dampening bearing goes one step beyond silicone in the dampening of RMC thermometers. Only RMC uses this extra dampening device in addition to silicone and the usual stamped bearings. It is a precision machined part, serving several needed dampening functions.

Special bearing plus silicone double-dampens RMC thermometers

In RMC bimetal thermometers a specially designed dampening bearing is used just above the bimetal element. This bearing further dampens the shaft, helps to prevent coil unwinding and pointer oscillation, and also serves as a better guide for perfect shaft alignment within the tube. It's the combined use of this dampening bearing and silicone that makes RMC thermometers extra resistant to shock and vibration. You get this *only* in RMC industrial thermometers.





FEinc PRECOAT FILTER

Rotary vacuum precoat filter
with infinitely variable knife
advance and power retraction.

Custom Filter Design

BEGINS WITH YOUR FILTRATION PROBLEM

Your processing requirements are king at FEinc. They dictate the type of filter to be built, its size, the materials used, and the special refinements necessary to assure highest possible operating efficiency.

For example, a FEinc Precoat Filter designed to meet your particular needs pays off fast in

trouble-free operation, dryer cake discharge and high clarity of effluent.

If you require higher output in limited floor area and a long filtration cycle coupled with the above advantages, FEinc custom design can give it to you.

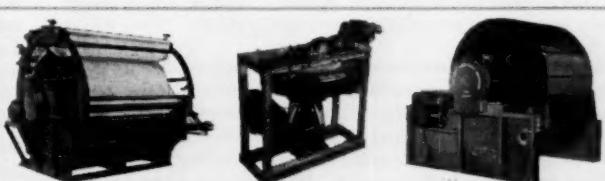
Send us your filtration problems. Specific recommendations provided without obligation.

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ROYAL PRECISION LGP-30**

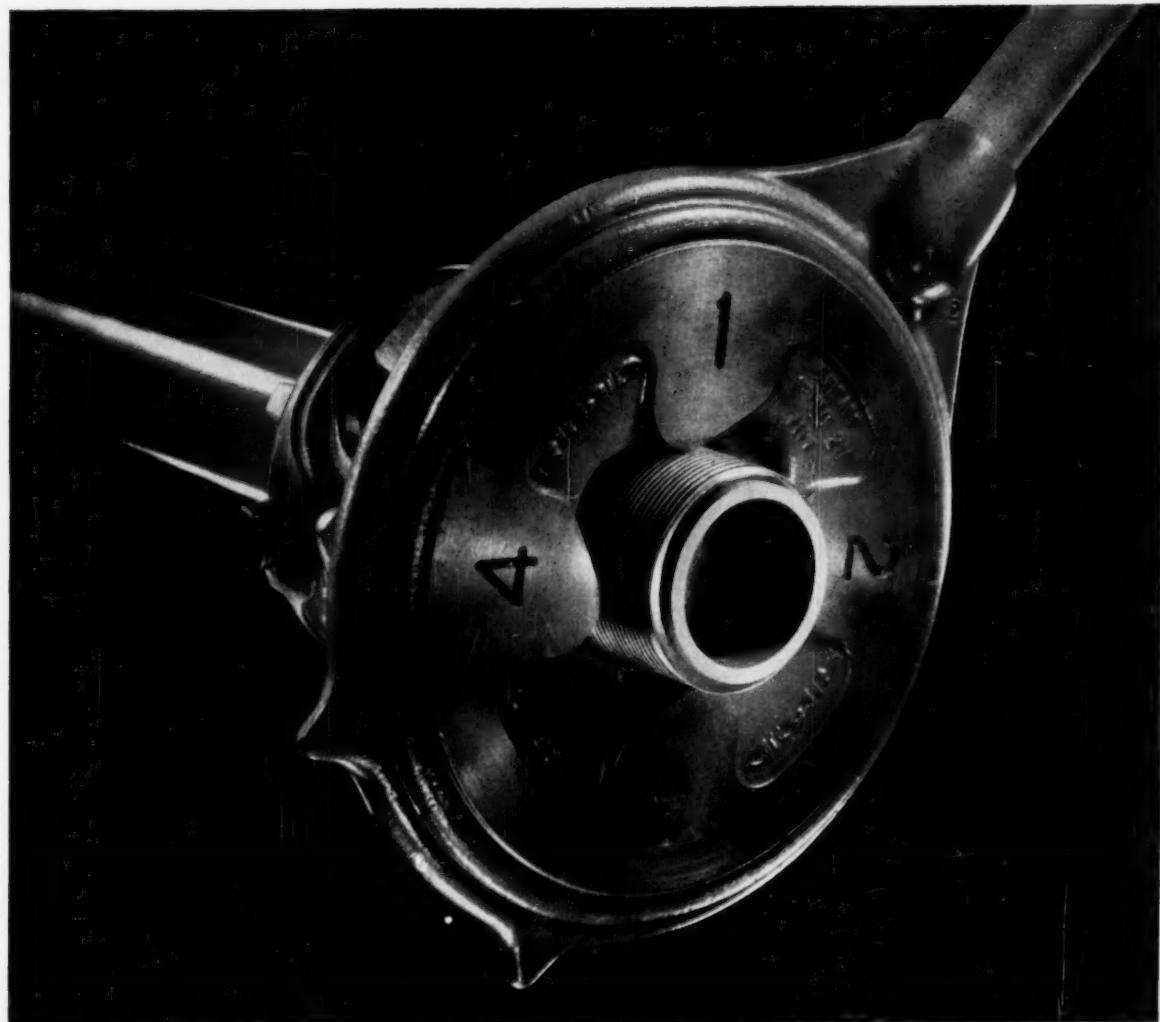
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Here's why saran lined pipe cuts installation costs

*It's easy to fabricate, easy to install at job site . . .
and it resists corrosion for years*

Here is a corrosion-resistant pipe that can be fabricated in the field. Saran lined pipe can be cut and threaded at the job site with conventional hand tools or power equipment. And, once installed, saran lined piping systems resist corrosion for years . . . offering proved long-range economy.

For piping acids, alkalis, solvents and other corrosive fluids specify saran lined pipe, fittings, valves, and pumps with the new gray lining. This new lining anchored under pressure within the steel casing, enables you to pipe fluids over a wider range of temperatures than ever before . . . with maxi-

mum protection from corrosion, plus the strength of steel.

Saran lined pipe, fittings, valves, and pumps are available for systems operating from vacuum to 300 psi, and from well below zero to 200°F.

If your operation can benefit from a *complete* corrosion resistant piping system, write today for more information about saran lined piping components. And be sure to ask about Saraloy® 898 tank lining, too! THE DOW CHEMICAL COMPANY, Midland, Michigan.

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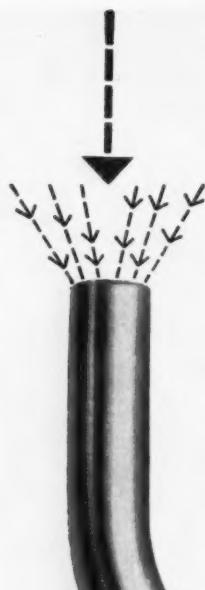
Please send me information on Saran lined pipe, fittings and valves. Saran lined centrifugal pumps. Saraloy 898 chemical resistant sheeting.

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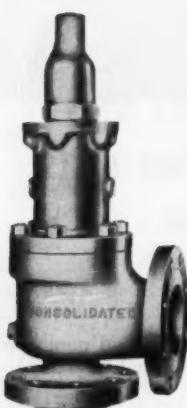
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Consolidated Safety Relief Valve, Type 1900 Series, Sizes: 1" x 2" to 8" x 10".

The Eductor Tube in Standard Consolidated Safety Relief Valves is a pressure evacuator. It efficiently removes pressure from the closed bonnet. If allowed to remain in the bonnet, the pressure would act on the top of the disc and tend to limit the lift and induce cycling. But with the pressure evacuated from the closed bonnet through the Eductor Tube, the spring alone controls valve action. Consequently, *reliable* valve action and guaranteed capacity ratings are attained. A new high in operational dependability is assured.

Reliable operation and performance of Consolidated Safety Relief Valves are your assurance of absolute protection for personnel and equipment. "2 in 1" design permits you to convert the Standard valve to the Bellows type in your own shop. But that is only part of the total economy of these modern valves. Get the complete inside story. Write for Catalog 1900.



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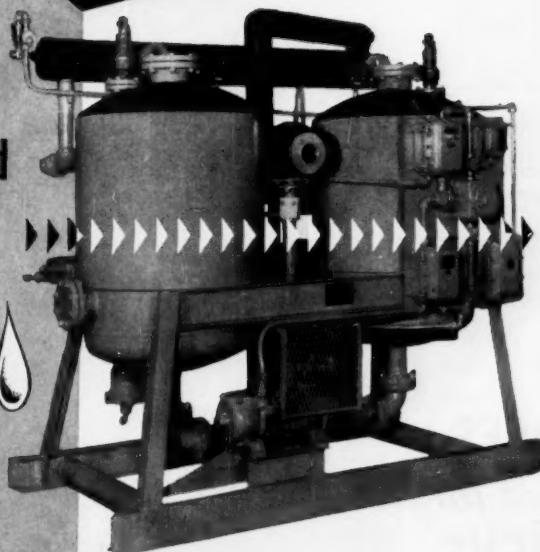
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keep processes
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Lectrodryer engineers have many years' experience in solving DRYing problems. The Lectrodryer equipment they recommend is generously designed and constructed for the moisture-removing load anticipated. No skimping on capacity or cutting corners on materials to meet a price.

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Send us Bulletin 223B.

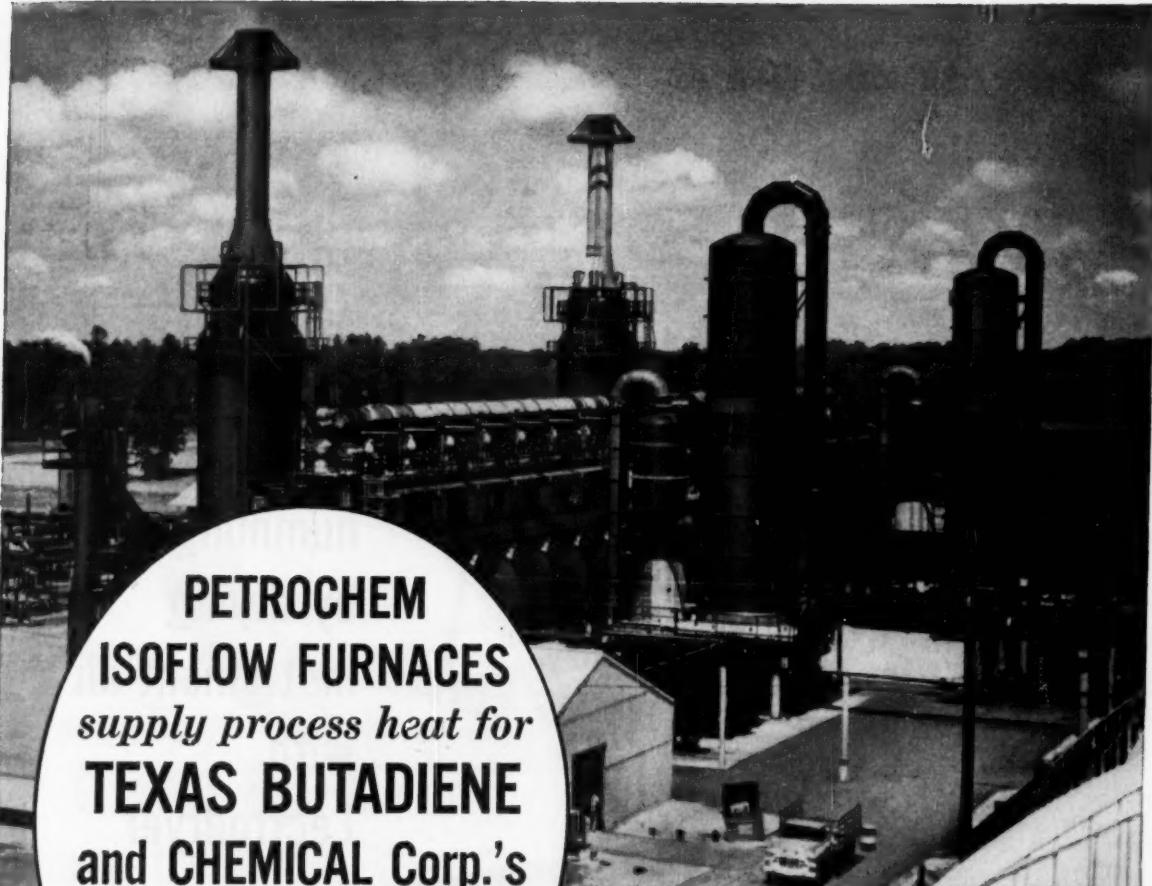
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Perhaps you've felt the need to meter your industrial liquids but have hesitated because you feared metering was costly or complicated. Actually, even a plant-wide installation of simple, direct reading Rockwell meters can be made very easily and for a nominal investment. They will pay their way many times over by providing realistic records for cost, inventory and utilization controls.

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If you blend, batch or package liquids, Rockwell meter accessories such as automatic shut-off controls, impulse counters and remote registration will cut your costs and increase production. Use the coupon for full details.



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Pipe Size _____ "

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Your Name _____

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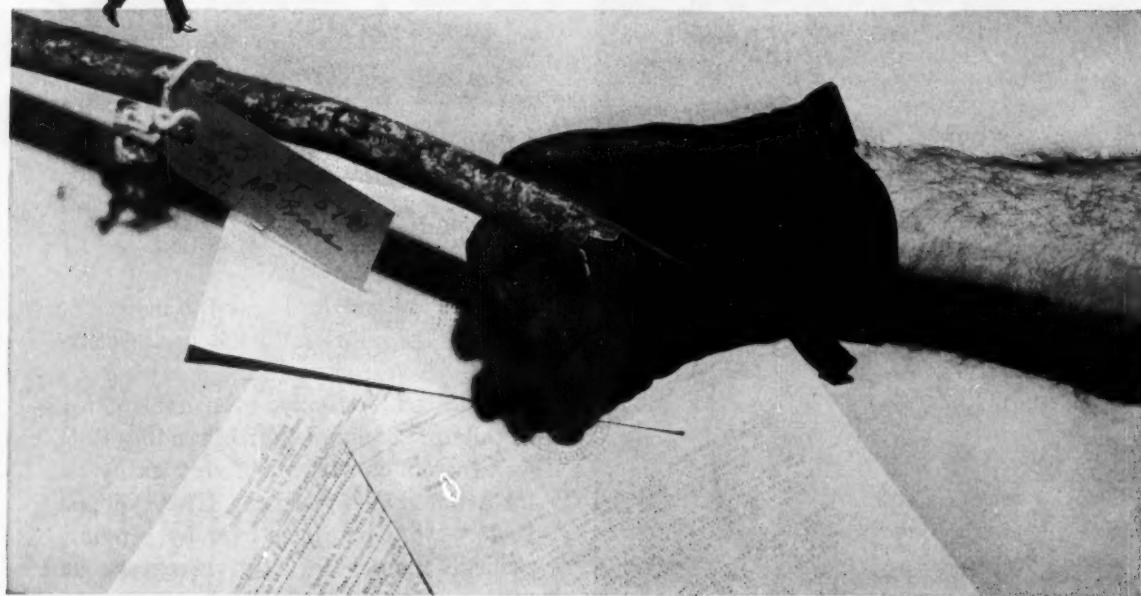
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BRIDGEPORT "T" MEN* IN ACTION

**Technical Service Men*



The Case of the Telltale Tube

When the tube came into the lab it was covered with the scars of a savage attack. An obvious case of malicious assault. Accompanying clues were a completed Bridgeport Corrosion Questionnaire and a letter of explanation. The customer—a rendering plant—wanted help fast. He asked for recommendations from the Bridgeport Technical Service Staff.

A sample of the tube was rushed to the Spectrograph, an instrument that analyzes 14 elements in less than 5 minutes. Areas of corrosive attack and cracks were examined on a Metallograph. The tube was found to be phosphorized aluminum brass, and tube failure due to stress corrosion from vibration and ammonia on the product side.

"T" Man telephoned customer's chief engineer and notified him of findings. They discussed plant's operation and the

products rendered. Neither ammonia nor vibration could be eliminated. From extensive experience in similar cases, "T" Man made several recommendations which would solve the problem. The customer installed Bridgeport 70/30 cupro nickel tube for greater resistance to ammonia and other organic products. Results? Unit operating with top efficiency and economy. No evidence of tube failure since. Case closed.

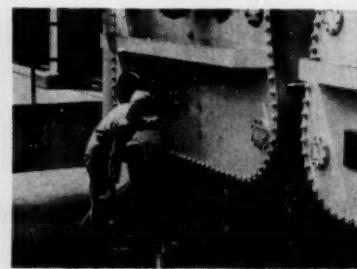
This is one of many cases from the files of Bridgeport's Technical Service Men. Practical field experience, modern laboratory equipment and expert corrosion engineers assure Bridgeport customers of maximum service and efficiency from their power and process equipment. Learn more about Bridgeport condenser and heat exchanger tubes and services. Call your nearest Bridgeport Sales Office today.



Spectrographic analysis determines tube composition. Can analyze 14 elements in less than 5 minutes.



Metallographic examination reveals type of tube failure from which cause can be determined.



Follow-through—Bridgeport "T" man visits plant to review effects of recommended solutions.

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When you buy Motor Starters --

YOU PAY FOR OVERLOAD PROTECTION

Only **ONE-PIECE** Overload Relays give 100% Protection. Only with **ONE-PIECE** construction can you know you've installed the heater correctly. Only with **ONE-PIECE** construction can you know the heater is exactly centered, or properly positioned, so that it performs according to its rating. Only with **ONE-PIECE** construction can you know your motors have full protection.

Only Square D has **ONE-PIECE** Construction. **ONE-PIECE** construction eliminates any possibility of heater misalignment. Square D melting alloy thermal overload relays can be installed only one way. They are tamper-proof. They are factory-assembled, are *individually* calibrated and tested. Repeated tripping will not affect accuracy.

Insist on

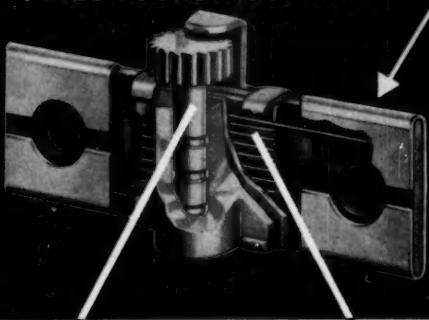
Square D melting alloy thermal overload relays

*Write for Bulletin SM-275 for the complete story on Square D starters with **ONE-PIECE** thermal overload relays. Address Square D Company, 4041 N. Richards St., Milwaukee 12, Wisconsin.*

**...BE
SURE
YOU
GET
IT!**

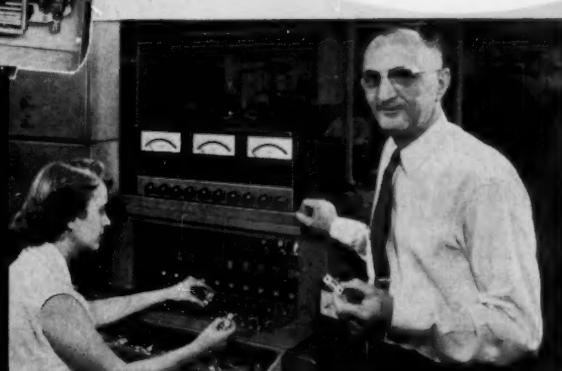


1-PIECE CONSTRUCTION



Heat-responsive element (solderpot) provides accurate response to overload, yet prevents nuisance tripping.

Heat-producing element is an integral part of overload unit. It's permanently joined to solder pot, can't become misaligned.

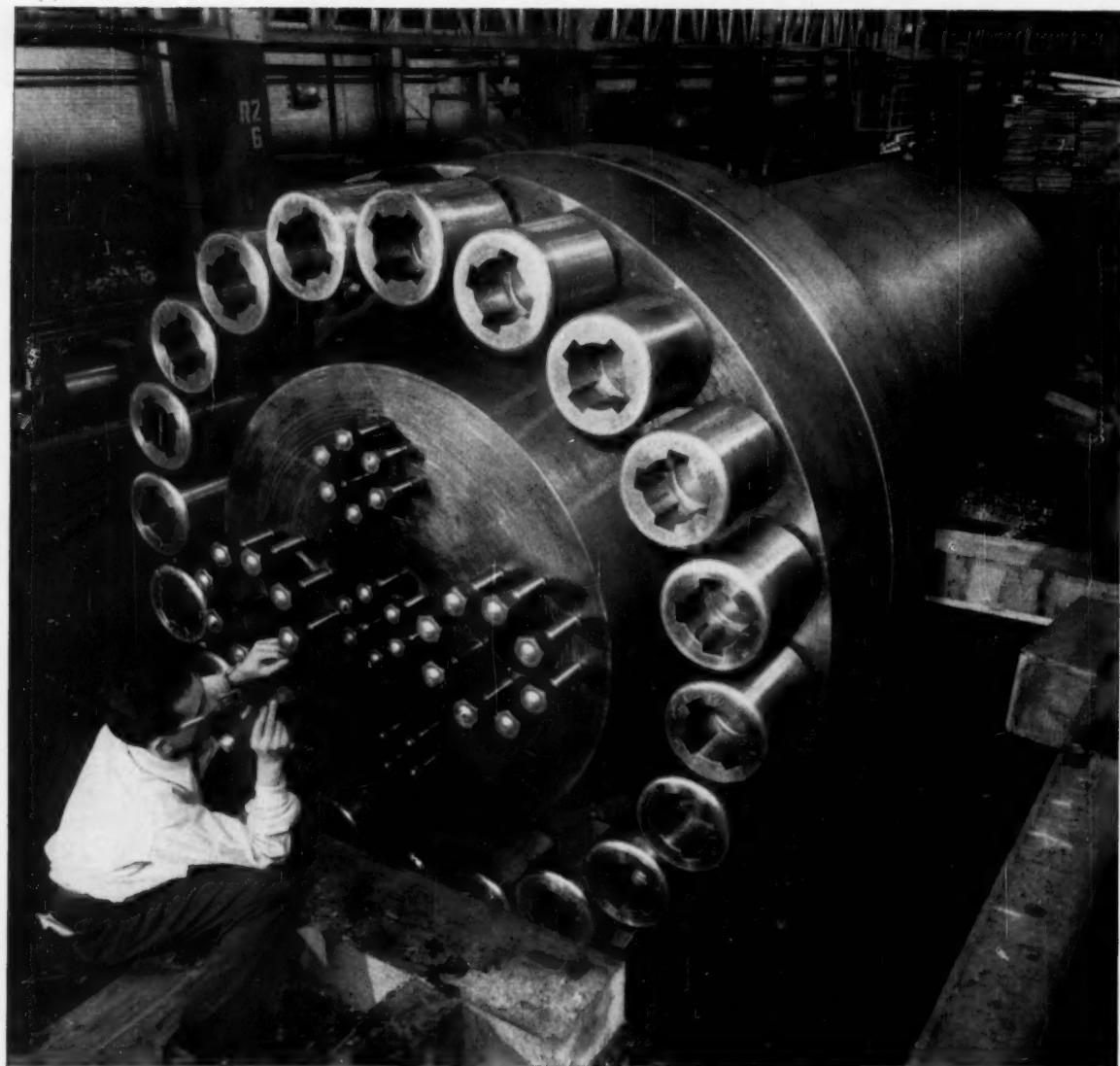


Individual factory inspection of every Square D melting alloy thermal overload relay means performance you can trust. Each unit is calibrated and thoroughly tested to make sure it will perform according to its rating.



EC&M HEAVY INDUSTRY ELECTRICAL EQUIPMENT...NOW A PART OF THE SQUARE D LINE

SQUARE D COMPANY



Big Separator Ready to Go

Here's a 43-ton forged-steel separator built recently in the Bethlehem shops. It's 14 ft long and has an ID of 48 in. Note the massive head and those tremendous closure nuts. Everything about this vessel has the ruggedness and strength needed to handle high pressures.

The unit is typical of the many seamless vessels that Bethlehem custom-builds for the chemical industry. We are equipped to forge, treat, machine, and assemble virtually any type of separator, filter, reactor, converter, autoclave, or accumulator—in weights ranging from a few hundred

pounds to 150 tons. No matter how small or how large, all Bethlehem vessels are made to exacting standards, with every specification met in full.

When you are planning new equipment of this nature, we suggest you discuss it with our engineers. They know all aspects of the technical problems involved, and you can rely upon them for complete cooperation.

BETHLEHEM STEEL COMPANY, BETHLEHEM, PA.

On the Pacific Coast Bethlehem products are sold by
Bethlehem Pacific Coast Steel Corporation
Export Distributor: Bethlehem Steel Export Corporation

BETHLEHEM STEEL



CARRIER CONVEYS

REALLY HOT MATERIALS

KILN DISCHARGE...SINTER...CLINKER
CASTINGS...DROSS...UP TO 1500° F!



- **Heavy Conveying Troughs** — $\frac{1}{2}$ " thick and heavier. Widths to 6', lengths to 500'. Easily vibrated in 1" stroke by rugged coil springs and single patented Carrier Natural-Frequency Drive.
- **Expandable Trough Sections** — Each 5' trough section attached by spring-loaded bolts through slotted holes. Sections expand independently of each other and of conveyor's structural members.
- **No Leakage** — A continuous one-piece dribble trough (not shown) mounted several inches below the conveying trough collects any fines which may leak through the conveying trough sections.
- **Replaceable Trough Sections** — New conveying trough sections easily installed. Little delay. Convenient replacement principle cuts costly down-time.
- **Heat-Resistant Materials** — Alloy and stainless steels resist warping and high-temperature scaling. Low abrasive wear due to gentle conveying action.
- **Quenching or Cooling** — Can be accomplished by direct or indirect water spray, plate-coil deck, or air.
- **Heat-Protected Drive** — Heat protection provided by heat shield, dribble trough, and flexibility of location.

CARRIER
~~NATURAL-FREQUENCY~~
CONVEYORS

Carrier Conveyor Corporation
254-A North Jackson Street
Louisville 3, Kentucky

Please rush full information on Carrier Natural-Frequency High-Temperature Conveyors.

Company _____

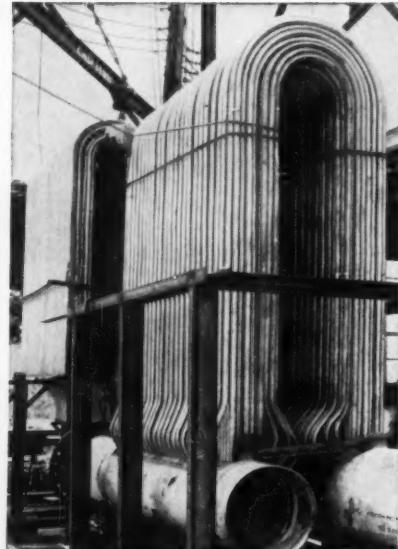
Name _____

Street _____

City _____ State _____

1600 Carpenter *bends*

harness 2,000,000 lb. of
corrosive hot air per hour



Conventional stainless steel tubing couldn't do the job. Six miles of tubing was needed, 1600 U-bends for a four-stage heat exchanger that raises 560 pounds of air from 350° to 700° F each second. The exchanger, one of the largest ever built, is being used in a gas-turbine aircraft engine test program.

The problems were carbide precipitation and loss of corrosion resistance due to the operating temperature. The problems were eliminated easily . . . with Carpenter Type 321 welded and cold drawn stainless tubing stabilized with titanium.

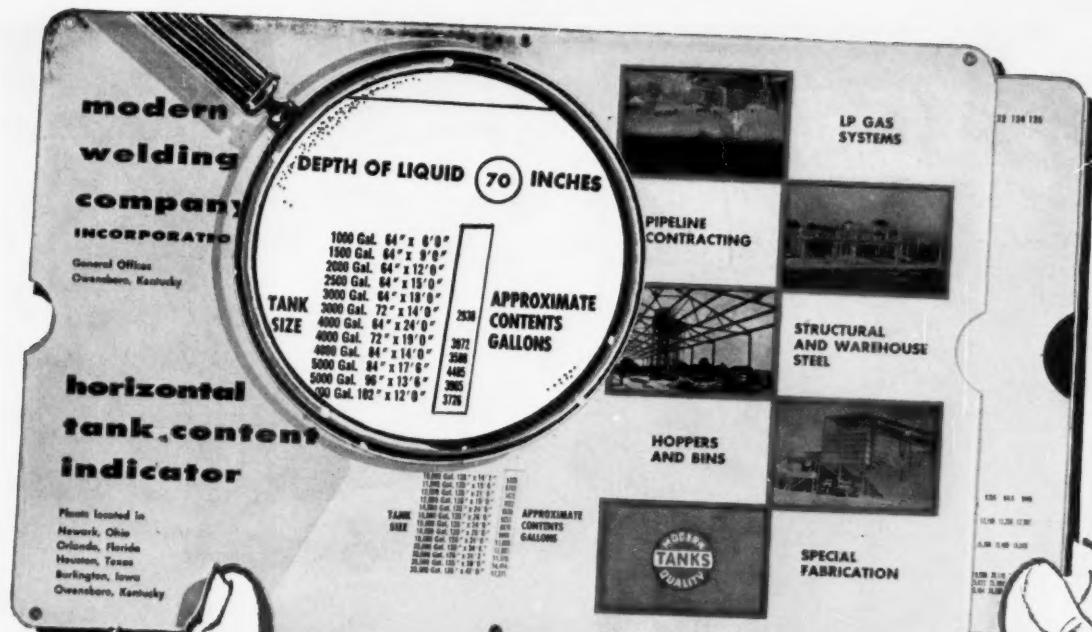
When something extra in uniformity, economy and low-cost service is needed, you'll benefit by contacting the Carpenter distributor or representative in your area. For complete data on the many analyses of Welded Stainless Tubing and Pipe available from distributor stocks or our mill, write for Bulletin T.D. 120 on your company letterhead. The Carpenter Steel Company, Alloy Tube Division, Union, N. J.—The House of Corrosion Control.

Export Dept.: The Carpenter Steel Co., Port Washington, N.Y.—"CARSTEELCO"

*your master key
to cost-saving
corrosion
control*



stainless tubing & pipe



Modern Welding Company, Inc.

1500 East 12th Street
Owensboro, Kentucky

Please mail, absolutely free, "The Modern Liquid Computer".
Have your representative call: _____ (Date)
NAME: _____
COMPANY NAME: _____
ADDRESS: STREET _____ CITY _____



YALE outperforms any loader—handles 25% more material every hour...Field tests prove it!

EXTRA WORK PER HOUR. No matter what bulk you handle, you'll get more productive work at less cost with the new Yale Industrial Tractor Shovel. *It carries more*—full 2500-lb. bucket capacity. *It moves faster*—accelerates to operating speed of 8 mph in 3.5 seconds—to 13 mph in 5.5 seconds. Exclusive Yale Torque Transmission (fully automatic) permits quicker, smoother starting, eliminates shifting, provides more power under load conditions—speeds cycle operations. Gasoline or LP-Gas.

EXTRA SAFETY. Yale's exclusive Safety-Curve Arms assure extra-safe elbow room—extra visibility when bucket is raised.

EXTRA MANEUVERABILITY. This is the first tractor shovel designed

especially for *industrial* use. It's *compact*—only 117" overall length—can maneuver in any aisle wide enough for a wheelbarrow.

EXTRA LOADING AND DUMPING FEATURES. Yale's exclusive 45° ground-level tipback insures the ultimate in loading action—and a grade-level carrying position to minimize spillage. Exclusive 6' dumping clearance is the highest on any model of similar wheelbase. Bucket is automatically self-locating—lowers from full dump-position to ground-level. Bucket automatically returns to digging position.

For a demonstration in your plant or for actual case histories, write to The Yale & Towne Manufacturing Co., Philadelphia, Pa., Dept. A-4410.

COMPARE!

For only 3¢ more per hour* the Yale Industrial Tractor Shovel offers these exclusive features

Exclusive Yale Torque Transmission (fully automatic)

Exclusive 45° ground-level bucket tipback

Exclusive Safety-Curve Arms

Exclusive accelerating speed of 8 mph in 3.5 sec.

Exclusive sealed brakes

Exclusive forward and rear operating lights

Exclusive 6' dumping clearance

*Based on comparative initial costs depreciated over 10,000 working hours.

YALE*

REG. U. S. PAT. OFF.

YALE & TOWNE

INDUSTRIAL LIFT TRUCKS & TRACTOR SHOVELS • HOISTS

GASOLINE, ELECTRIC, DIESEL & LP-GAS INDUSTRIAL LIFT TRUCKS • WORKSAVERS
WAREHOUSERS • HAND TRUCKS • INDUSTRIAL TRACTOR SHOVELS • HAND AND ELECTRIC HOISTS

YALE MATERIALS HANDLING DIVISION. THE YALE & TOWNE MANUFACTURING CO. MANUFACTURING PLANTS: PHILADELPHIA, PA.; SAN LEANDRO, CALIF.; FORREST CITY, ARK.



hydrofluoric acid—to 500° F,
in any concentration
can't corrode Fluoroflex®-T pipe

*liner of Teflon® in thermal
equilibrium with housing*

Lining is completely inert to all corrosives. It's made of Fluoroflex-T, a high density, *non-porous* compound* of virgin Teflon.

Liner and housing are in thermal equilibrium through an exclusive process developed by Resistoflex. It compensates for thermal expansion differential between the Teflon and the pipe housing, eliminating fatigue collapse, and cracking at the flange.

Reboilers constructed from Type S pipe are now in use handling boiling hydrofluoric acid with complete safety and *no* maintenance problems. Fluoroflex-T Type S piping systems can end maintenance problems for you, too. Bulletin TS-1A gives details. Write Dept. 143 RESISTOFLEX Corporation, Roseland, N. J. *Pat. No. 2,752,637

® Fluoroflex is a Resistoflex trademark, reg., U.S. pat. off.

® Teflon is DuPont's trademark for TFE fluorocarbon resins.

RESISTOFLEX

Complete systems for corrosive service

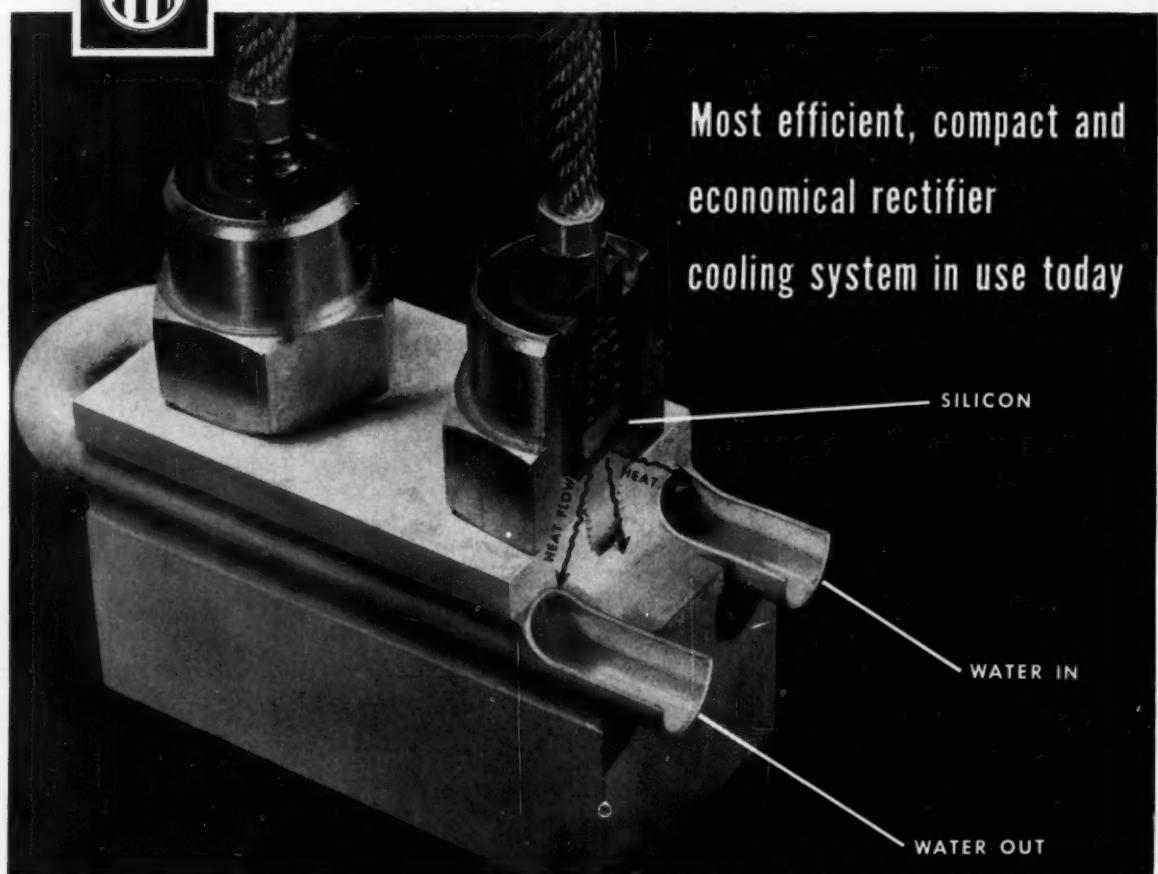


LINED STEEL PIPE • FLANGED FLEXIBLE HOSE • BELLows • ELBOWS • TEES • REDUCERS • DIP PIPES & SPARGERS • LAMINATED PIPE



UNITRON SEMI-CONDUCTOR RECTIFIER

Most efficient, compact and
economical rectifier
cooling system in use today



Section of bus bar... showing how cooling water flows close to cells for efficient cooling. Bus bar can be as long as necessary to hold the number of cells needed for the required current. Cells can be changed fast and easy without need to drain cooling system or shut down rectifier.

Just in the cooling system alone, the I-T-E UNITRON Semi-Conductor Rectifier saves you money. First, it costs so little to operate. Second, it takes little space. Third, it prolongs average cell life.

Uses ordinary tap water. No coolant is more efficient than water . . . none more economical than tap water. The I-T-E UNITRON takes ordinary tap water and continuously purifies it . . . deionizes it . . . to protect the system from corrosion and prevent electrical leakage. The resultant water is virtually a non-conductor of electricity.

The I-T-E UNITRON water cooling system eliminates the need for power-eating

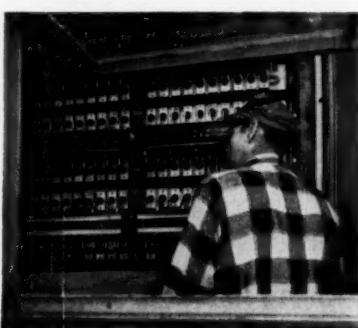
blowers and space-eating ducts. It saves the cost of special coolants and the danger of skin irritation to personnel.

Cooling water flows through the solid copper bus bar, close to the rectifying cells. Each cell is cooled to the same temperature. And since there are no hot cells, there are fewer cell failures.

This unique water cooling system is only one of the reasons the I-T-E UNITRON was chosen for the first 25 to 60 cycle reconversion by a large chemical plant in the Niagara area.

The I-T-E UNITRON can be built in any desired d-c voltage and current rating. For complete information, contact your local I-T-E representative. Or write

I-T-E Circuit Breaker Company,
Transformer & Rectifier Division, 19th
& Hamilton Sts., Philadelphia 30, Pa.



I-T-E CIRCUIT BREAKER COMPANY

New Protection For YOUR Equipment— At Temperatures Up To 3300°F

ALUNDUM castables
offer unusual
advantages to all
industries using
high temperature
installations*

The new Norton ALUNDUM Castables are made in two types: 33-I Insulating and 33-HD Heavy Duty. At temperatures up to 3300°F both types have been extremely successful in protecting high temperature processing — in many industries and many different installations.

ALUNDUM 33-I Insulating Castable is made up primarily of pure aluminum oxide bubbles, tiny and countless. Forming a network of air spaces, it assures excellent insulation, even at highest commercial temperatures.

ALUNDUM 33-HD Heavy Duty

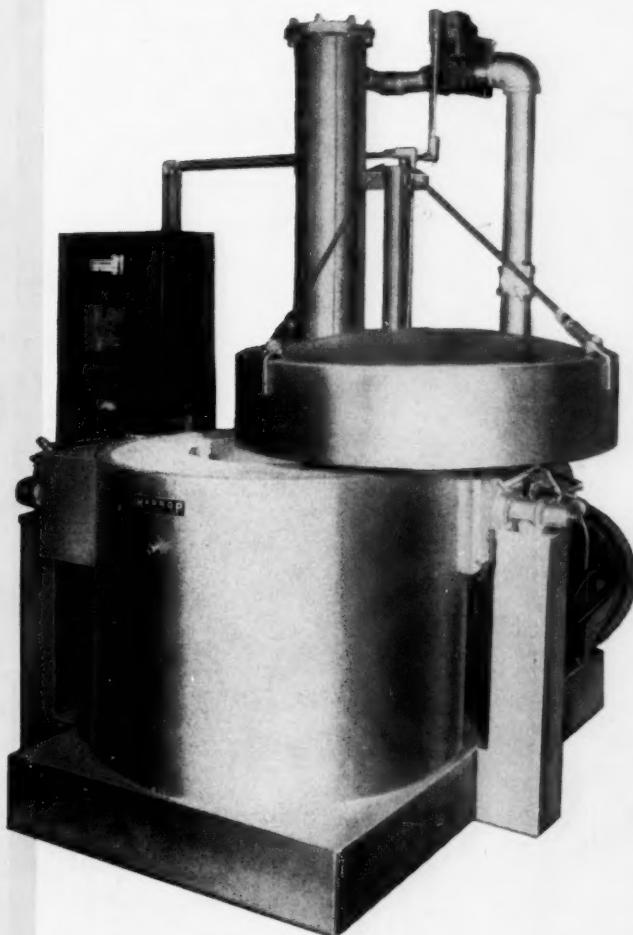
Castable is chiefly composed of dense grains of pure aluminum oxide. It is recommended for forming dense monolithic surfaces in many types of furnaces where high temperature conditions are particularly severe.

Both 33-I and 33-HD Castables are very easy to store, mix and use. With them you can cast simple or complex shapes quickly and economically, replace more expensive pre-fired shapes, and cut maintenance and replacement costs to very lowest. Ask your Norton Representative for details, and for the folder

Will fire continuously up to 3300°F. This Harrop gas-fired furnace, recently developed by the Electric Furnace Division of the Harrop Ceramic Service Company, Columbus, Ohio, is particularly applicable to the firing of ceramic oxide bodies. Norton ALUNDUM 33-I Insulating Castable selected for the inner lining of the furnace and its roof, provided completely satisfactory protection under repeated tests at highest operating temperatures.

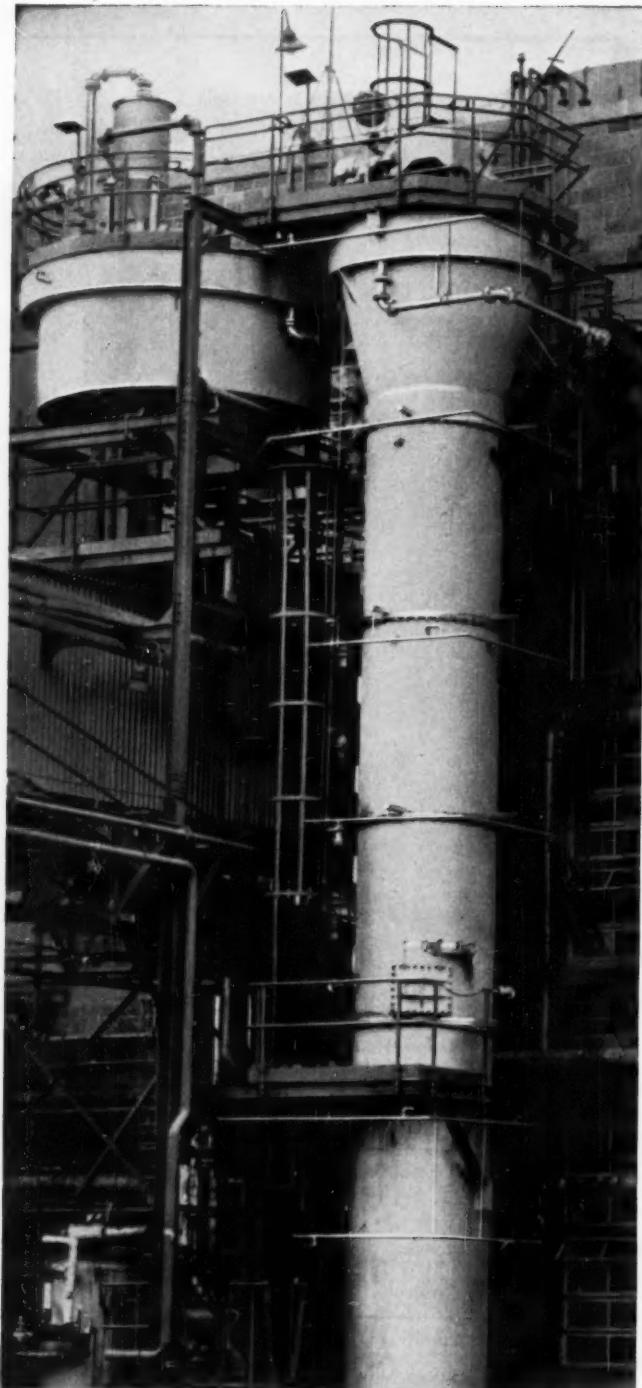
Two Norton Castables. Or write to NORTON COMPANY, Refractories Division, 510 New Bond Street, Worcester 6, Massachusetts.

*Trade-Mark Reg. U. S. Pat. Off. and Foreign Countries



NORTON
REFRACTORIES
Engineered... Rx... Prescribed

Making better products . . . to make your products better
NORTON PRODUCTS Abrasives • Grinding Wheels • Grinding Machines • Refractories • Electrochemicals — BEHR-MANNING DIVISION Coated Abrasives • Sharpening Stones • Pressure-Sensitive Tapes



Special Manhattan Rubber Lining to resist acidified solvent and abrasive cake is installed in this extraction tower for removal of anti-biotic from mycelia cake.

**PERMANENT
CORROSION,
CONTAMINATION
PROTECTION
WITH
MANHATTAN
RUBBER LININGS**

Manhattan Acid-Proof Rubber Linings are made from thick, multiple calendered sheets of natural or synthetic rubber for utmost protection and durability. These linings expand and contract with the metal under temperature changes . . . won't harden or crack. Resistance to most acids and alkalis is as fool-proof as 65 years experience and advanced technology can provide.

Every Manhattan Rubber Lining is bonded to metal so securely that they can't be separated . . . Every Manhattan Lined tank is tested under high voltage to assure flawless protection before being shipped to your plant. If the equipment *can't* be shipped to Manhattan, skilled crews will line the equipment in the field.

For permanent, positive protection for your processes *and* equipment, contact the R/M representative at the Manhattan Rubber Lining plant nearest you.

**RUBBER LINING PLANTS AT
PASSAIC, N. J. and NORTH CHARLESTON, S. C.**

R/M 806

BELTS • HOSE • ROLL COVERINGS • TANK LININGS • INDUSTRIAL RUBBER SPECIALTIES

MANHATTAN RUBBER DIVISION — PASSAIC, NEW JERSEY

RAYBESTOS-MANHATTAN, INC.

Other R/M products: Abrasive and Diamond Wheels • Brake Blocks and Linings • Clutch Facings • Asbestos Textiles • Mechanical Packings • Engineered Plastics • Sintered Metal Products • Industrial Adhesives • Laundry Pads and Covers • Bowling Balls



CHIKSAN



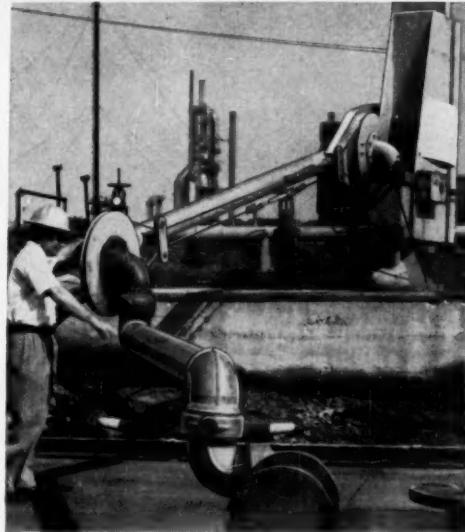
**PREVENTS LINE HANDLING INJURIES
SPEEDS BARGE LOADING
ELIMINATES HOSE BURSTS
SLASHES REPLACEMENT COSTS**

The Chiksan Barge Loading Arm ends hazardous manhandling of loading hoses, eliminates dangerous dock clutter. Mechanical operation makes hookup fast and simple.

Gear reduction enables one man to adjust the flange position anywhere in a 105° vertical range. Outboard arm is manually swung into position at any point in a 130° horizontal arc. The eight inch model rotates 360° to permit servicing barges on both sides of a narrow dock. Once hookup is made, the arm can be left unattended while free wheeling allows the unit to ride free during loading and unloading.

When not in use, the arm is raised up and out of dockside traffic.

6" x 25' and 8" x 28' sizes available. Handle petroleum products, both black and bright, and mild caustics in any temperature ranging between -60° F. to +225° F. Service all river and lake barges and lake tankers including those in 25,000 barrel class.



The Chiksan Barge Loading Arm is designed to reach approximately 20 feet from dock riser to barge flange. Total length of Arm is 25 feet.



CHIKSAN
A SUBSIDIARY OF
FOOD MACHINERY AND CHEMICAL CORPORATION



**CHIKSAN COMPANY - BREA, CALIFORNIA
CHICAGO 5, ILLINOIS • NEWARK 2, NEW JERSEY**

Well Equipment Mfg. Corp. (Division), Houston 1, Texas
Subsidiaries: Chiksan Export Company
Chiksan of Canada, Ltd.

58-36



CHIKSAN COMPANY
330 No. Pomona Ave., Brea, Calif.

Please send me your Barge Loading Arm Bulletin #456.

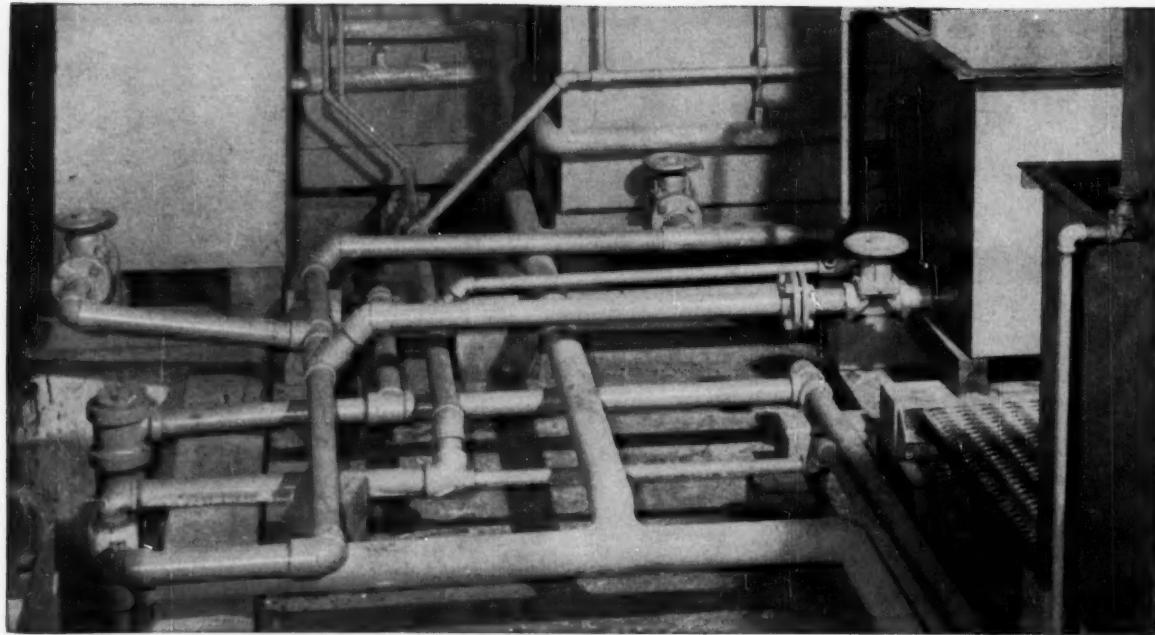
Name _____

Title _____

Company _____

Address _____

City _____ Zone _____ State _____



Muriatic acid lines of National PVC Pipe used at National Lock Fastener Plant

The National Lock Co. Fastener Division, Rockford, Illinois, is using 3,000 feet of USS* NATIONAL Polyvinyl Chloride Pipe in sizes from 1" to 4" O. D. to convey muriatic acid, deionized water and acid wastes for their plating process. Their choice was dictated by USS NATIONAL* PVC Pipe's immunity to acids and corrosion, and its excellent economy.

Two types of USS NATIONAL PVC Pipe are available:
Normal Impact—for installations requiring the highest chemical resistance attainable, together with high strength and excellent creep resistance.

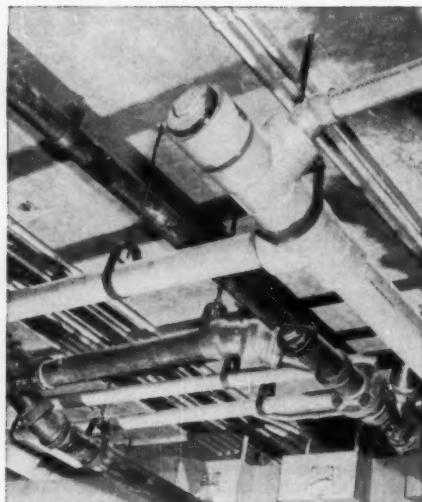
High Impact—for installations requiring excellent chemical resistance and a high degree of toughness, even at low temperatures.

USS National PVC Pipe comes in sizes from $\frac{1}{2}$ inch to 14 inches in diameter, and in Schedules A, 40, 80 and 120.

National Polyvinyl Chloride Pipe has a variety of uses in the chemical industry because it is resistant to many chemicals, including acids, alkalies, salt solutions and alcohol.

If you'd like more information, write to National Tube Division, United States Steel Corporation, 525 William Penn Place, Pittsburgh 30, Pa. Ask for Bulletin No. 24.

*"The world's largest and most experienced manufacturer of tubular products—
NATIONAL TUBE"*



This seal of the National Sanitation Foundation means
Tested . . Approved . . Sanitary!



*TRADEMARK

**National Tube
Division of
United States Steel**

Columbia-Geneva Steel Division, San Francisco, Pacific Coast Distributors • United States Steel Export Company, New York

October 6, 1958—CHEMICAL ENGINEERING

MAGIC GENIE OF THE REACTOR HARSHAW CATALYSTS

WILL DO A GIANT'S WORK FOR YOU

Harshaw Catalysts do a giant's work and Harshaw produces catalysts in giant quantities—carloads every week. A letter or phone call will put our 20 years' experience and acres of production and research facilities to work for you.

CATALYTIC CHEMICALS SUPPLIED BY HARSHAW

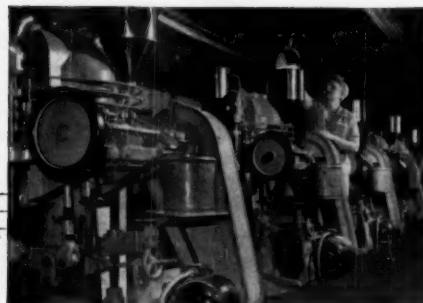
Aluminum Nitrate	Cobalt Nitrate	
Copper Nitrate	Manganese Nitrate Solution	
Metallic Soaps (Cobalt, Manganese)		
Nickel Carbonate	Nickel Formate	Nickel Nitrate
Nickel Sulfate	Sodium Methoxide	Zinc Nitrate

Our experienced technical staff will assist you in developing the best and most economical catalyst. If you have a catalytic process in the development or production stage, a discussion with us may prove beneficial.

PREFORMED CATALYSTS

to fit special process requirements

Hydroforming	Dehydrogenation	Alkylation
Cyclization	Dehydration	Hydrogenation
Oxidation	Desulphurization	Hydro treating
	Chlorination	

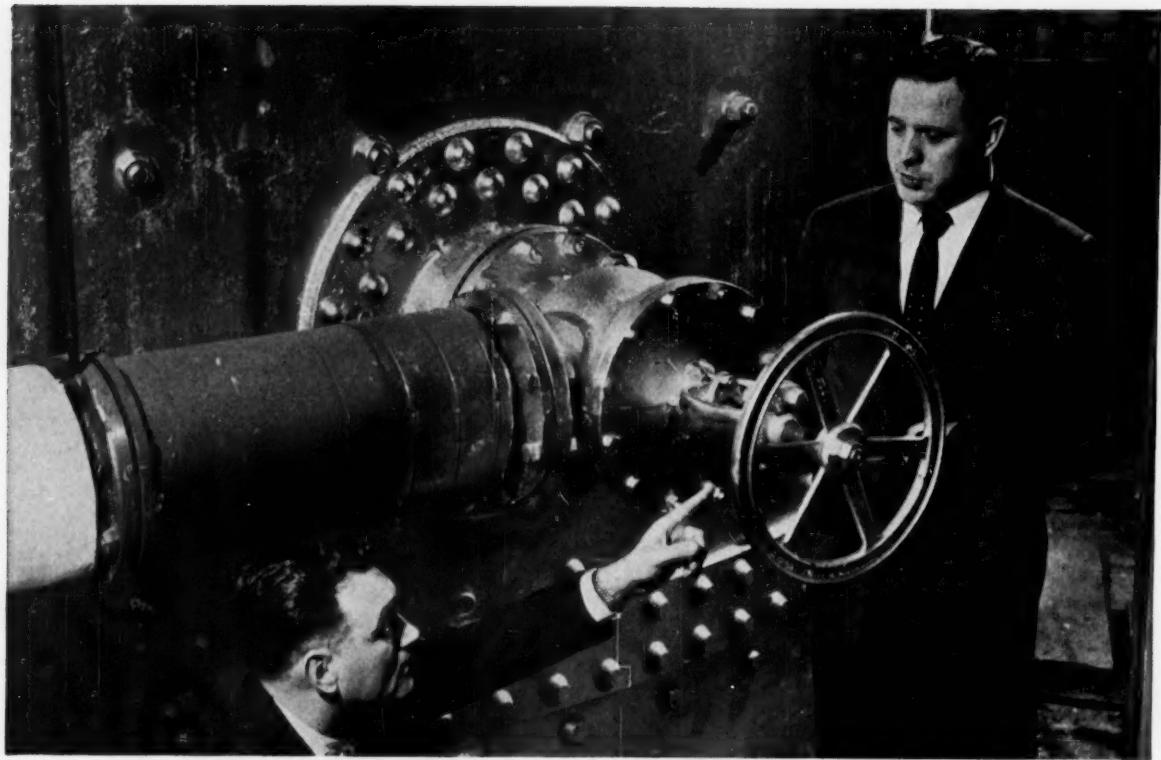


THE HARSHAW CHEMICAL CO.

Chicago • Cincinnati • Cleveland • Detroit • Hastings-On-Hudson
Houston • Los Angeles • Philadelphia • Pittsburgh



Write
for FREE Book



Harold Blakney (right), Maintenance Manager, Brown Company, Berlin, N. H. Left, Frank Hiltz, Vice President Brown Wales Co., Cooper Alloy distributors, Auburn, Me. Center, Cooper Alloy 8" angle circulating valve on digest tank.

BLAKNEY of BROWN COMPANY tells why Cooper Alloy Valves suit him

Q. Mr. Blakney, why does Brown Co., a leading manufacturer of pulp, paper, and other forest products, use stainless valves and fittings in its mills?

A. Because stainless steel is one of the few materials that can take the tough corrosion punishment of pulp mill digester fluids.

Q. Why Cooper Alloy valves?

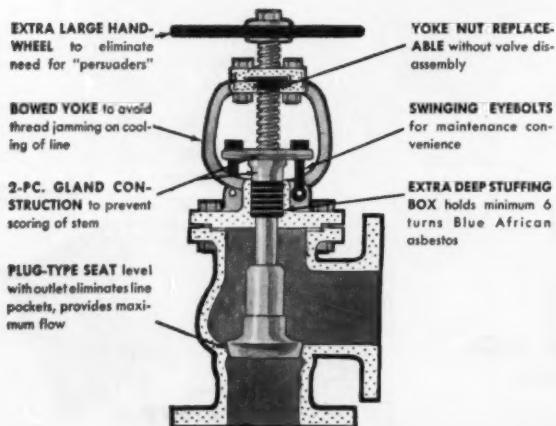
A. For long life and low maintenance. Over the years Cooper Alloy valves have proven themselves to be extremely well designed for the tough service we give them.

Q. How, specifically?

A. Well, these 8" angle valves, for example, have that extra-deep stuffing box to give a tighter stem seal. The seat, level with the outlet, eliminates line pockets and provides maximum flow. These plus extra large handwheel all give me less maintenance problems.

Q. Anything else you like about Cooper Alloy valves?

A. Yes, I like the engineering service available from Cooper Alloy we have had occasion to use, and the fine fast delivery and service we obtain from Brown Wales' nearby warehouse.



A VALVE DESIGNED FOR STAINLESS! The Cooper Alloy valve is not an adaptation of earlier brass and iron patterns. Cooper Alloy, with over 35 years of experience in handling stainless steel, created a valve *designed to be cast in stainless!* Check the Special Design Features shown at left.

As the little CA man below is saying: "You can tell a Cooper Alloy Valve as far as you can see it!" Write today for your copy of our folder "Valves and Fittings in the Pulp and Paper Industry." The Cooper Alloy distributor near you will be glad to show you the complete line of Cooper Alloy valves and fittings, and their advantages. He can serve you promptly from local stocks.

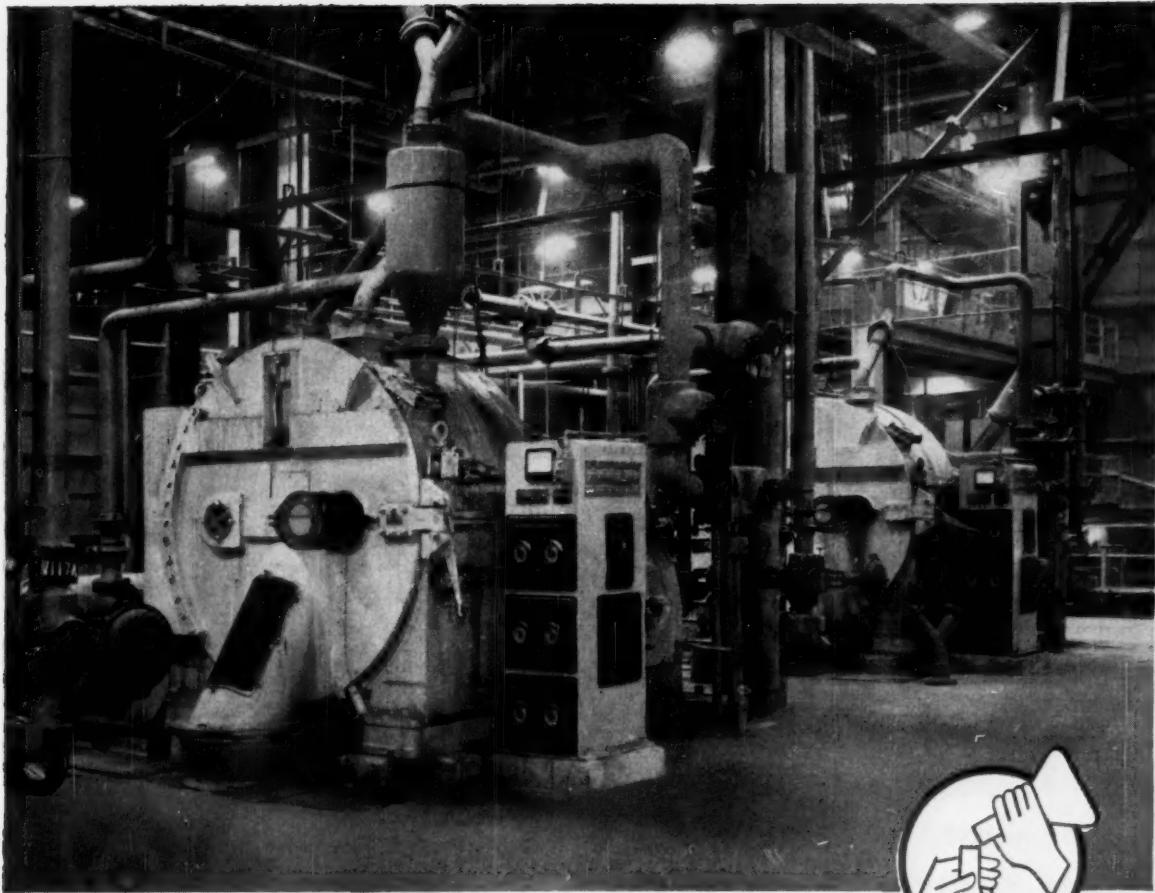
COOPER ALLOY

Corporation • Hillside, New Jersey

FOUNDRY PRODUCTS DIVISION

THIRTY-FIVE YEARS OF STAINLESS STEEL PIONEERING

October 6, 1958—CHEMICAL ENGINEERING

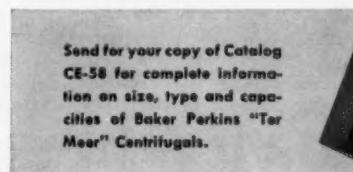


B-P CENTRIFUGALS used by ELECTRO METALLURGICAL COMPANY in Titanium Production

Although a metal, titanium is produced by a chemical process. Metal in the form of ore is converted to titanium tetrachloride, which is purified and then reduced to metallic sponge by sodium. In order to separate the brine from the titanium sponge, Electro Metallurgical Company, Division of Union Carbide Corporation, New York, utilizes Baker Perkins 66" diameter type HS Universal Centrifugals. It's a tough application, but the B-P Type HS has proven itself efficient and dependable. These same machines are adaptable to a wide range of filterable fine solid-liquid slurries. Baker Perkins also manufactures type S Continuous Centrifugals which are used extensively for the separation of filterable coarse solid-liquid slurries.

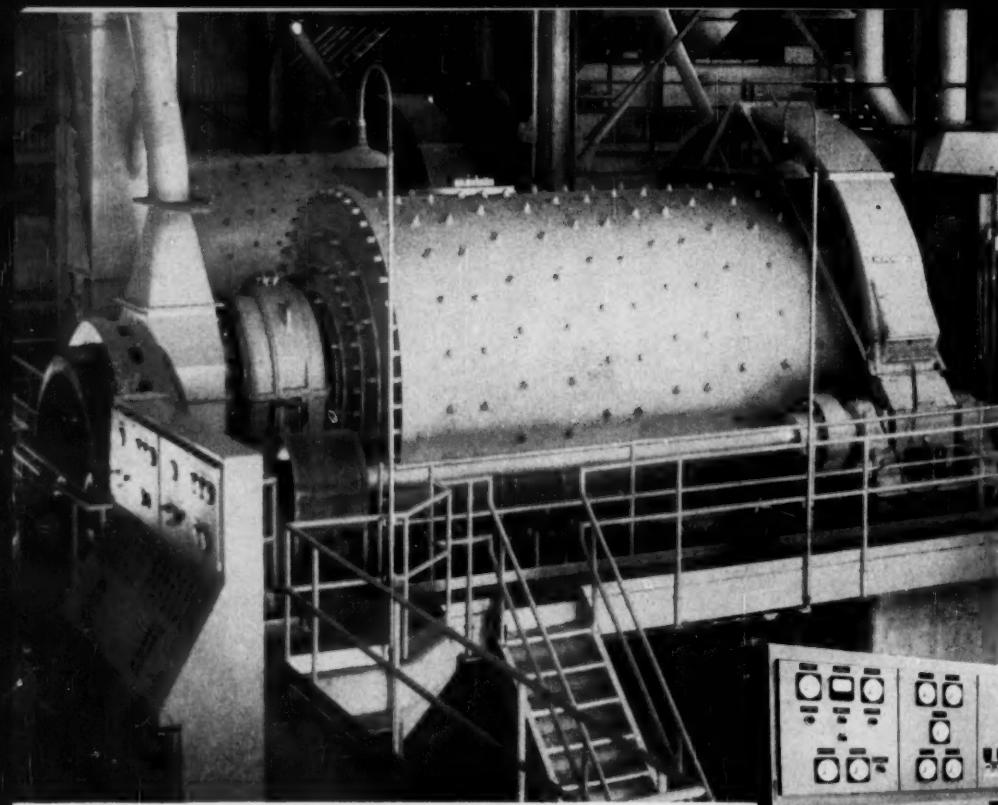
Since centrifugation is such an important process in the

chemical industry, and, since there are so many types of slurries that must be separated, Baker Perkins engineers give special design consideration to each specific problem. No matter what factors are involved in each application, our engineers can make recommendations on the proper centrifugal machinery.



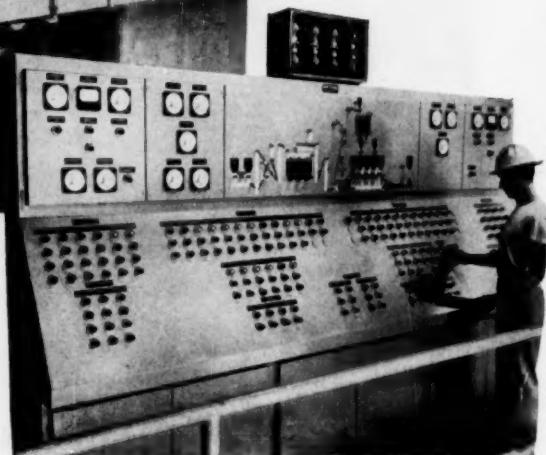
BAKER PERKINS INC.

CHEMICAL MACHINERY DIVISION
SAGINAW, MICHIGAN



Left: Two of five 11' x 17' Nordberg Grinding Mills installed for dry process service at a new cement plant.

Below: Close-up view showing modern, functional Nordberg grinding mill control console, with interlocking relays for sequence starting of all equipment. Note flow diagram with indicator lights at center of top panel.



3 reasons why it pays to specify **NORDBERG** GRINDING MILLS

1 Advanced Engineering Nordberg mill design reflects significant technological improvements that may measurably affect your installation and operating costs. Sealed trunnion bearings; positive bearing lubrication; optimum life of wearing parts are among the features that will benefit you.

2 Quality Manufacture Nordberg Mills are (1) precision built to rigid specifications in shops renowned for (2) skilled manufacturing personnel, and (3) modern machine tools and equipment to assure quality workmanship. Good reason why the name NORDBERG has always signified the *ultimate* in mining, quarrying and process machinery.

3 Dependable Operation A team of experienced application engineers with a sound understanding of your milling operations qualifies Nordberg to serve you. More important, it assures you of the right machinery for the job . . . machinery that must be dependable and will continually produce to your specifications.

Nordberg Grinding Mills are built to meet specified conditions for wet or dry grinding—in the manufacture of cement; the fine reduction of metallic and non-metallic minerals; and in numerous other processes where friable material must be comminuted to fine sizes at low cost per ton. They are available with grate, overflow or peripheral discharge . . . and are built in sizes from 6 feet to 13 feet in diameter and up to 50 feet in length.

Write for a copy of Bulletin 232, which describes the complete line of Nordberg Grinding Mills.



©1958, N. M. Co.

NORDBERG MFG. CO., Milwaukee 1, Wisconsin

NORDBERG



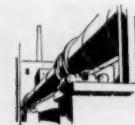
ATLANTA • CLEVELAND • DALLAS • DULUTH • HOUSTON • KANSAS CITY
MINNEAPOLIS • NEW ORLEANS • NEW YORK • ST. LOUIS • SAN FRANCISCO
TAMPA • WASHINGTON • TORONTO • VANCOUVER • GENEVA
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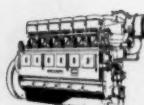
SYMONS®
CONE CRUSHERS



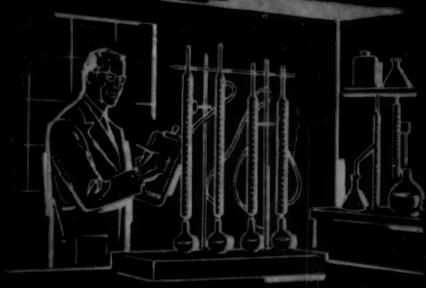
VIBRATING GRIZZLIES
and SCREENS



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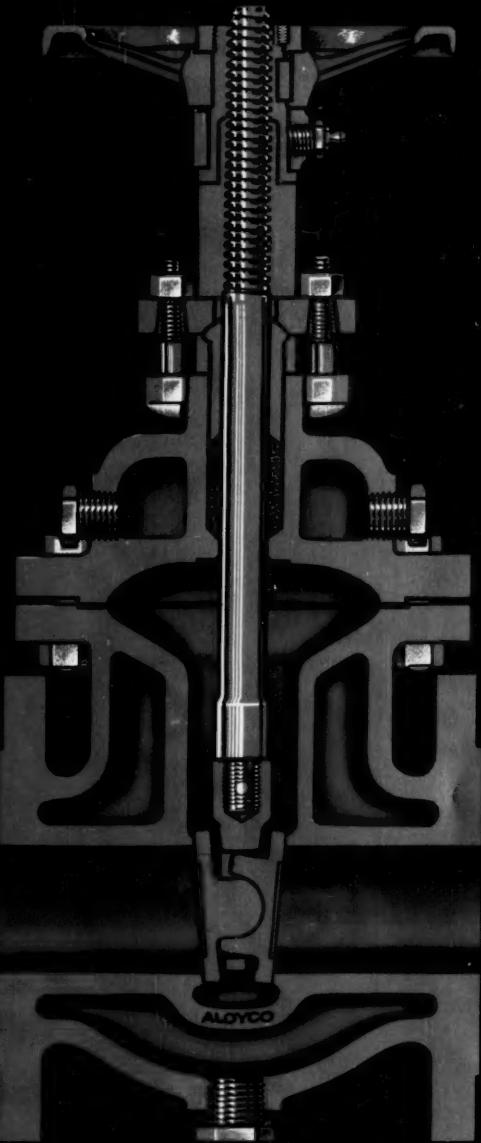
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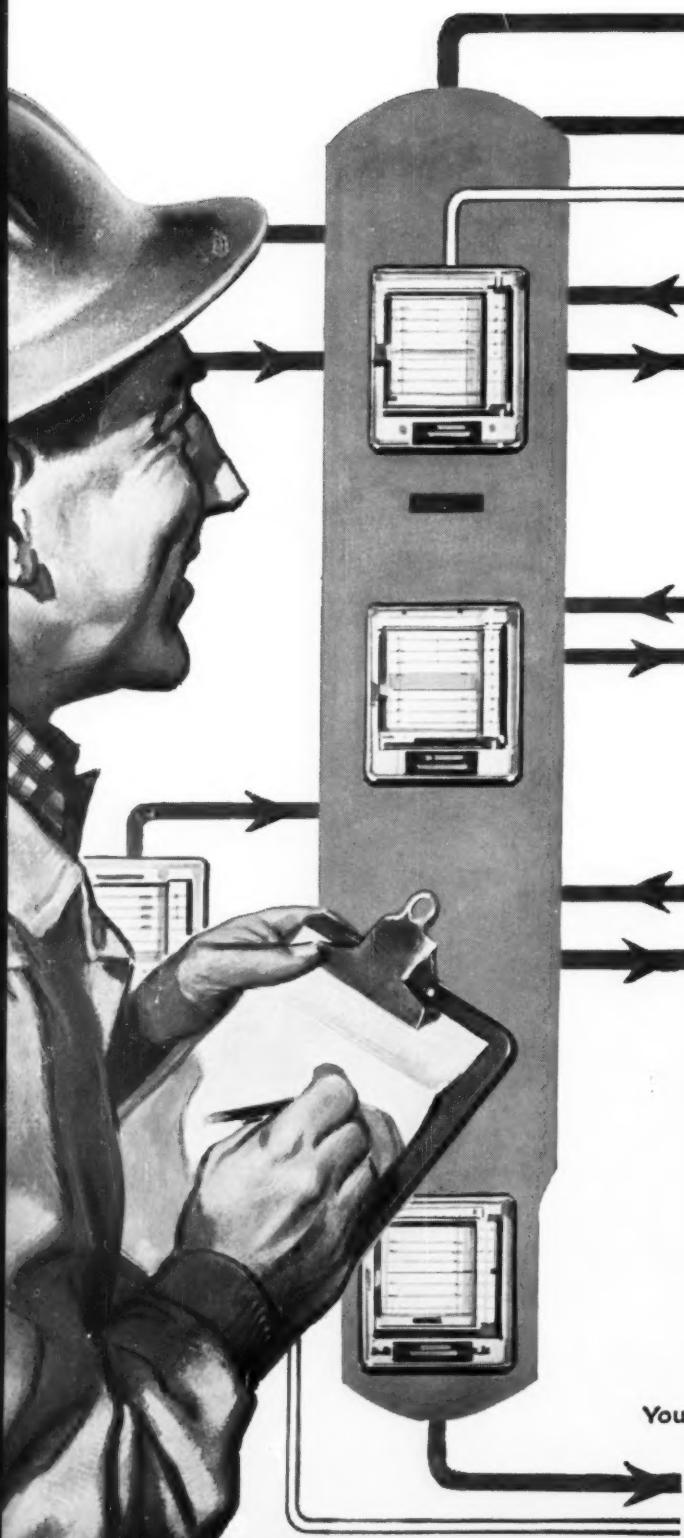
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makes certain of the

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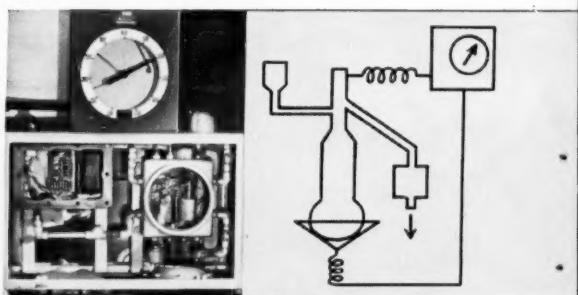
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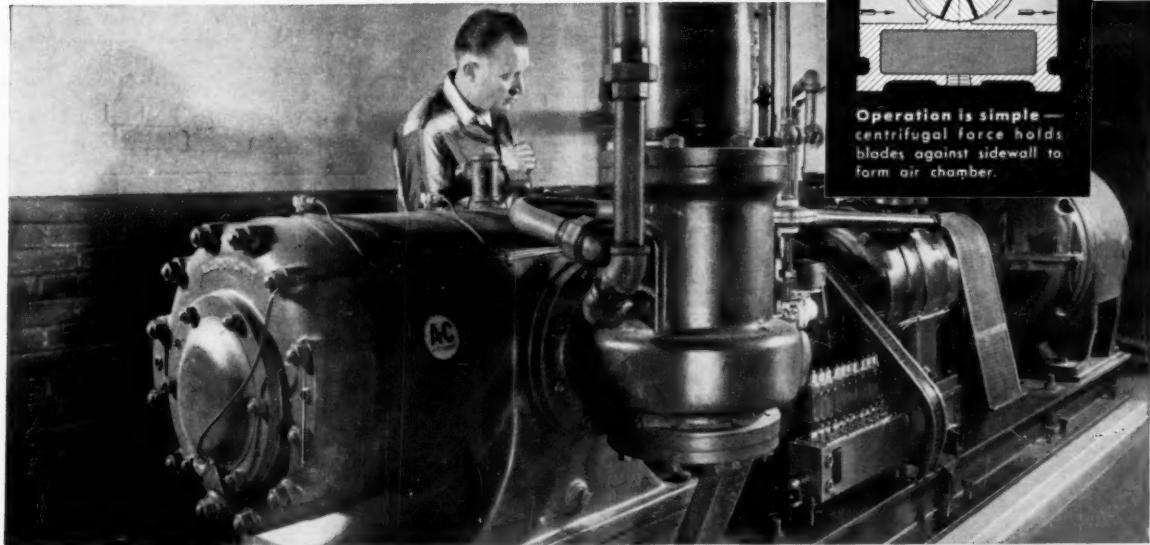


Automatic end-point tester works this way. A small sample is placed in an electrically heated flask. The temperature is measured and recorded during a heating cycle when distillation is accomplished. Distillate is condensed and drained, the flask temperature is lowered by introduction of the next sample, and the apparatus is ready for another test.

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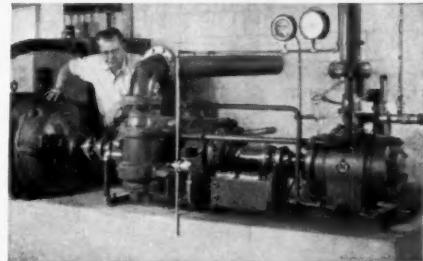
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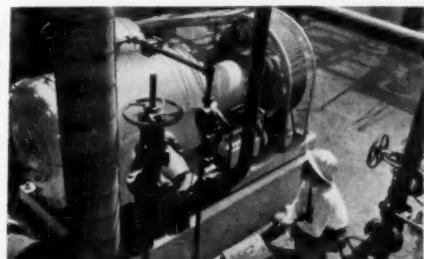
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Two-stage rotary compressor used for plant air service in a midwestern plant.



Ro-Flo hydrogen compressor in a southwestern plant, used here in conjunction with acrylic monomer process.



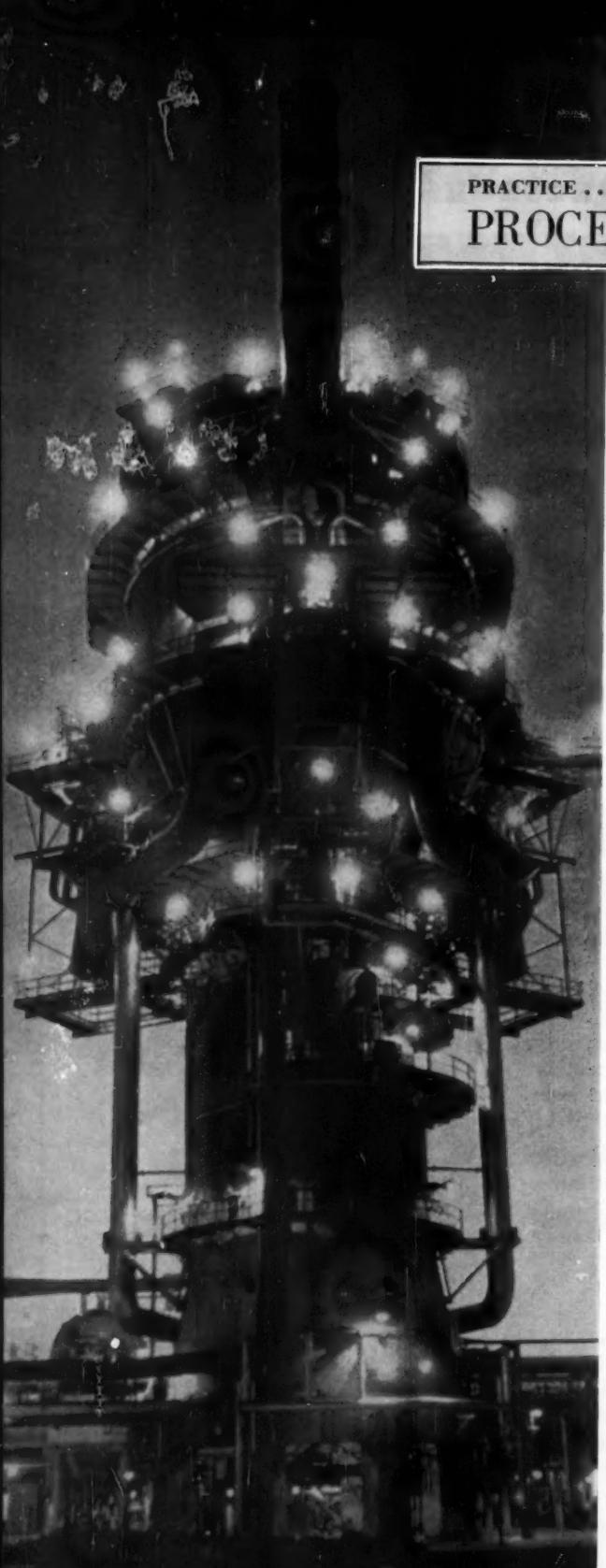
For complete information on Allis-Chalmers rotary compressors, ask for two-stage Bulletin 16B8244 or single-stage Bulletin 16B8126. Call your nearby A-C office or write Allis-Chalmers, Industrial Equipment Division, Milwaukee 1, Wis.

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PRACTICE . . .

PROCESS FLOWSHEET C. H. CHILTON

In: Gas-solids contacting
Piping design
Fluidizing techniques
Materials of construction . . .

Cat Cracker Sets Challenges

Crowning the trend toward bigger, higher-capacity refinery equipment, Tidewater Oil's giant Orthoflow fluid catalytic cracking unit* at its Delaware refinery, south of Wilmington, stands as the largest such unit in the world (design capacity: 102,000 bbl./day) and as an impressive (height: 250 ft.) monument to king-size engineering effort (maximum operating catalyst inventory: 1,300-1,400 tons).

Tidewater's cracker has now completed nearly two years of successful operation (15 months since the last turnaround), proving that, in many technical respects, bigness pays off.

Operating in conjunction with a fractionating tower, cracker's prime purpose is to convert gas oils to high-octane gasoline (29,000 bbl./day). Other large-scale product streams from the fractionator are 18,000 bbl./day of light gas oil and 184,000 lb./hr. of butanes and lighter.

► **Size Is the Spur**—A description of the unit's immense size points up the most formidable engineering problems.

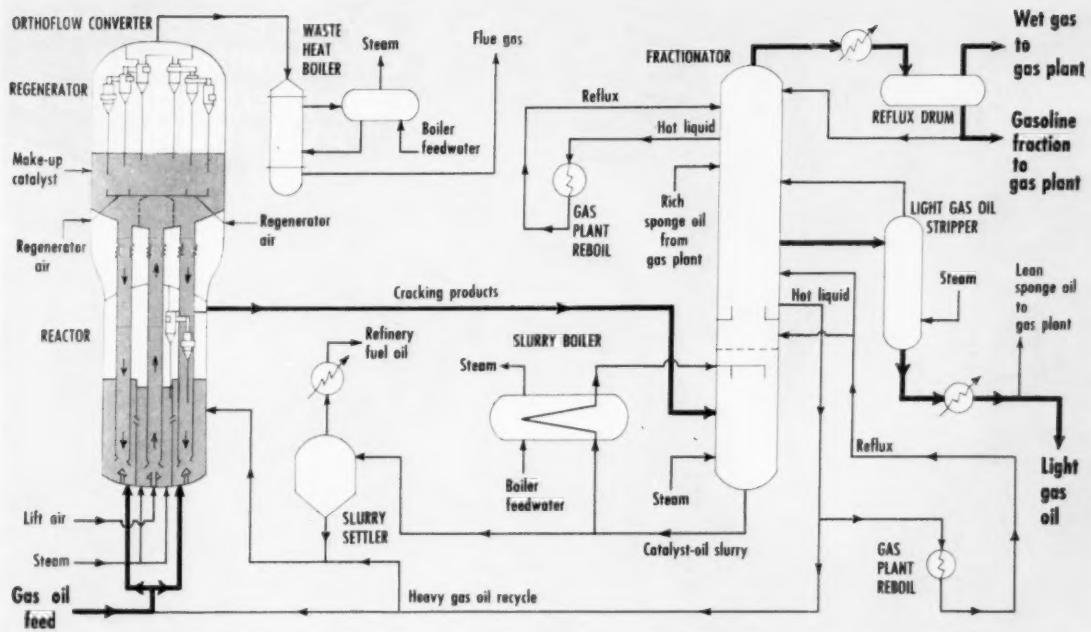
Cracker consists of a single 200-ft.-high converter vessel which houses reactor and catalyst regenerator, contains facilities for cracking and for catalyst stripping, regeneration and circulation. The 60-ft.-dia. regenerator is mounted on top of the reactor vessel which contains the catalyst stripper in its center section. Maximum total weight is 9,500 tons.

Regenerated alumina-silica gel catalyst flows from regenerator down through straight, 28-in.-dia. refractory-lined standpipes into the reactor bed.

Spent catalyst flows into the stripping zone through slots in the cylindrical plate that separates this section from the reaction zone, and then is air-conveyed

*Designed by M. W. Kellogg Co., built by C. F. Braun Co.

Unfold Flowsheet



up through two 42-in.-dia., refractory-lined risers into the regenerator.

These risers handle catalyst at a whopping rate of 85 tons/min., with linear velocities of 20-30 ft./sec. ▶ **A Lot of Air**—It's quickly apparent that to circulate and regenerate this amount of catalyst, Tidewater needs air on a mammoth scale. And it has just that.

Regenerator air blower is an Ingersoll-Rand centrifugal blower with a capacity of 137,200 scfm., driven by an 11,250-hp. turbine using steam at 575 psig. and 750 F. Blower takes suction at 14.4 psia. and discharges at 30 psia.

Lift air blower which supplies air to circulate catalyst is an Ingersoll-Rand centrifugal with 29,800 scfm. capacity, takes suction at 14.4 psia. and discharges at 36.1 psia.

▶ **Making Contact**—Handling such vast amounts of catalyst and air presents a number of problems in pipe design and gas-solids contacting.

Kellogg's design approach involves using two risers and four standpipes—twice the number conventionally used in Orthoflow units—to help catalyst distribution. Multiple pipes, together with a large number of oil inlets to the reactor (28, including those for recycle), assure good contacting throughout large areas of reactor and regenerator.

Distributing regeneration air is aided by a system of four large half-rings set in the regenerator bed. Perforated tubes, over 2 ft. in dia., are shaped into half-rings about 50 ft. in dia. fed by two air inlets. Having thousands of holes to emit air, distributor does effective job of contacting air with catalyst—more effective, claims Kellogg, than conventional flat grid.

Two- and three-stage cyclones (16 in the reactor, 60 in the regenerator) separate entrained catalyst—about 40 tons/min. in the regenerator alone—and return it to catalyst beds.

▶ **Construction materials**—Straight risers and standpipes, of course, help reduce pipe wear, but they're

refractory-lined, too, to keep erosion to a minimum. Sound thinking led Kellogg to line reactor, regenerator and cyclones with insulating and refractory concrete.

Risers and standpipes are fitted with expansion joints between reactor and regenerator to allow for metal expansion under different operating conditions.

Tidewater avoided costly materials of construction as much as possible. Converter shell is carbon steel, as are reactor cyclones and most of the internals. And, even at the bottom head of the reactor, steel thickness is never over 1½ in.

Lower part of the fractionating column, from above the recycle draw-off pan, is protected from corrosion by an 11-13%-chrome-clad plate.

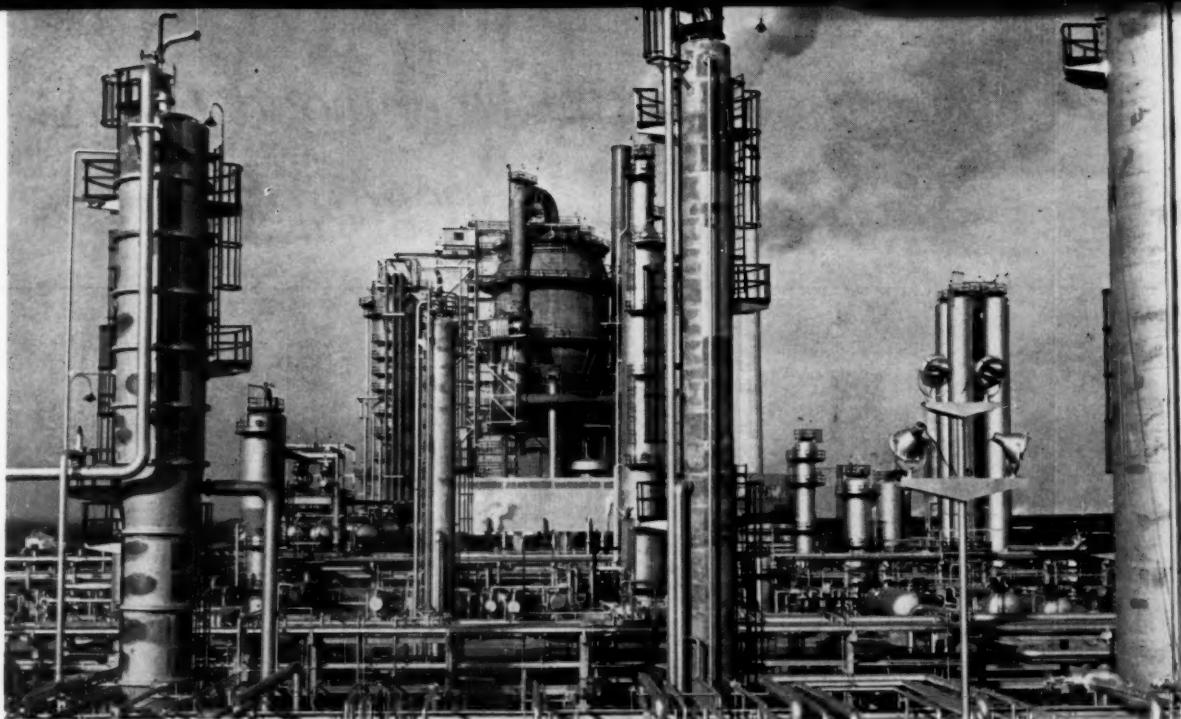
▶ **Flow Route**—Here's how the fluid cracker works at Tidewater. Gas oil feed, a mixture of virgin and fluid coker gas oils, is fed in the bottom of the reactor, where it passes up through catalyst bed at about 900 F. and is cracked. Cracked vapors pass through reactor cyclones where entrained catalyst is separated and then pass to 25-ft.-dia. bubble-cap fractionating column.

Two waste-heat boilers, hung on either side of the regenerator shell, recover heat from flue gases by generating 175-psi. steam.

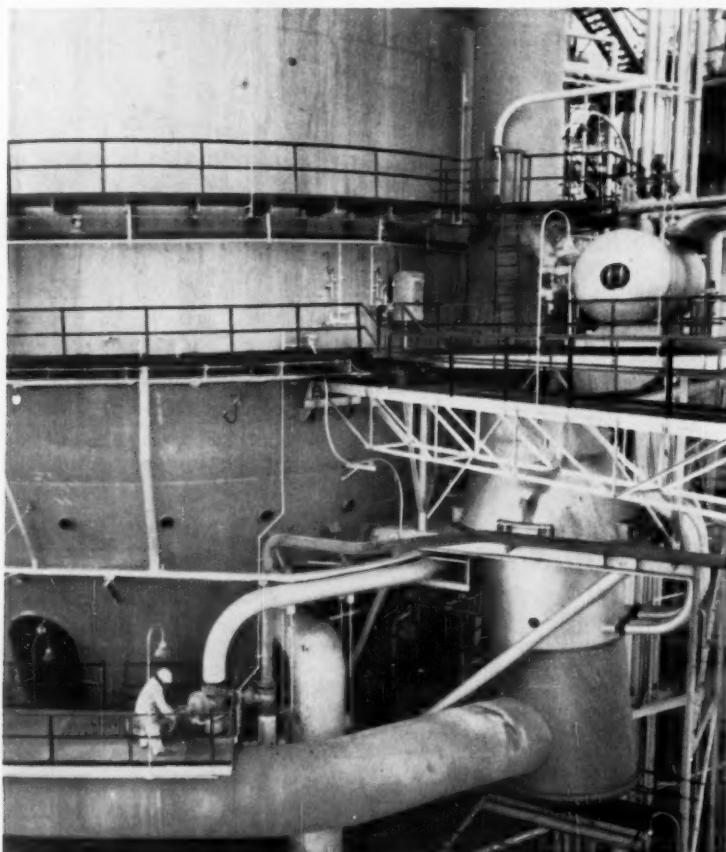
In fractionator, cracking products are split into 430-F.-end-point overhead stream, light gas oil, heavy gas oils and a bottoms stream of catalyst-in-oil slurry, of which part is taken off as fuel oil after catalyst is separated out. Sponge oil cut from the column is pumped to the gas plant to absorb propane and propylenes, then returns to column for stripping.

Two side cuts are taken from fractionator to supply reboil heat for the gas plant to get the needed temperature gradients in the tower for optimum separation.

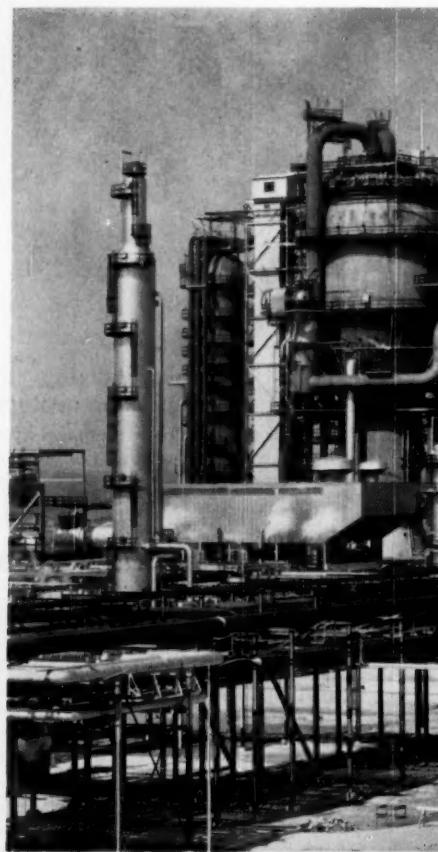
Nearby catalyst storage bins can hold as much as 500 tons of fresh catalyst and 1,800 tons of used catalyst.



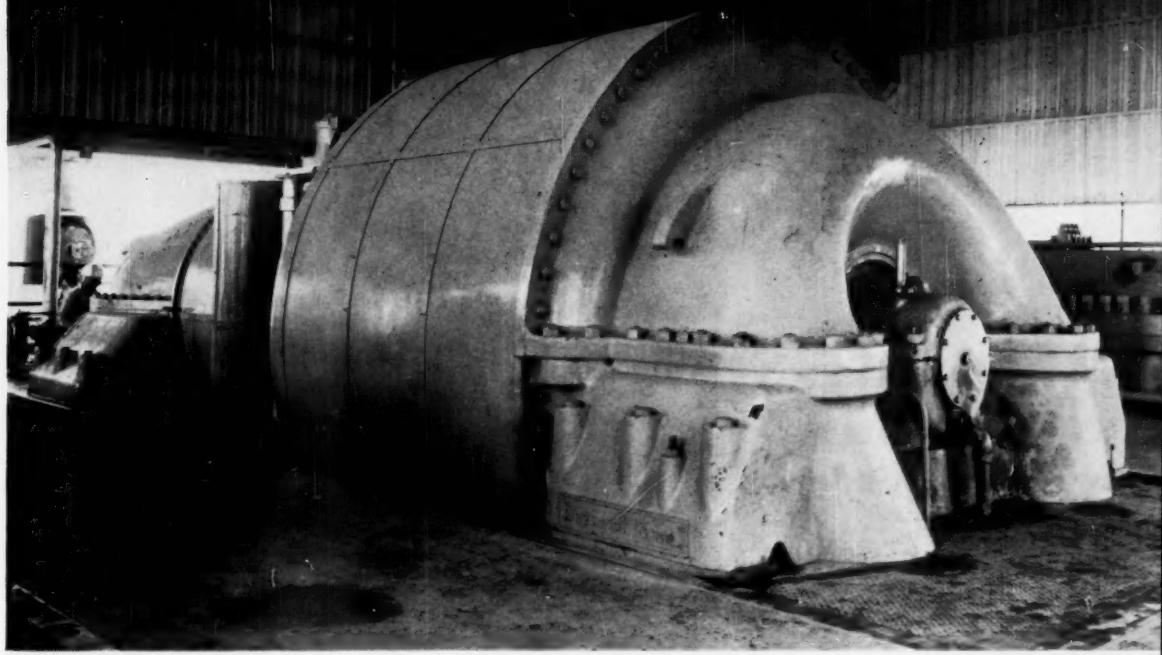
WIDE VIEW OF REFINERY shows how Orthoflow fluid cracking unit dominates maze of piping and towers. In background can be seen cracking-products splitting tower (at left of cracker) and fuel-gas surge tanks (right).



WASTE-HEAT BOILER, at right, one of two similar units, recovers heat from flue gases by generating 175-lb. steam, sends gases to stack.

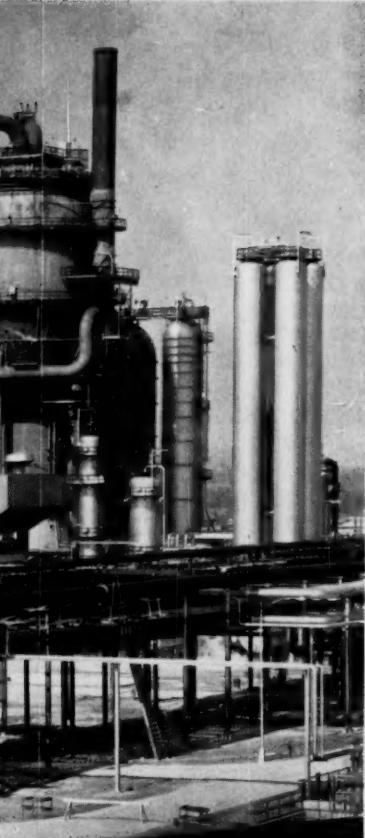


CRACKER is flanked by splitting tower and fuel-gas surge tanks (far left and far right). Far left and far right: absorber-deethanizer.

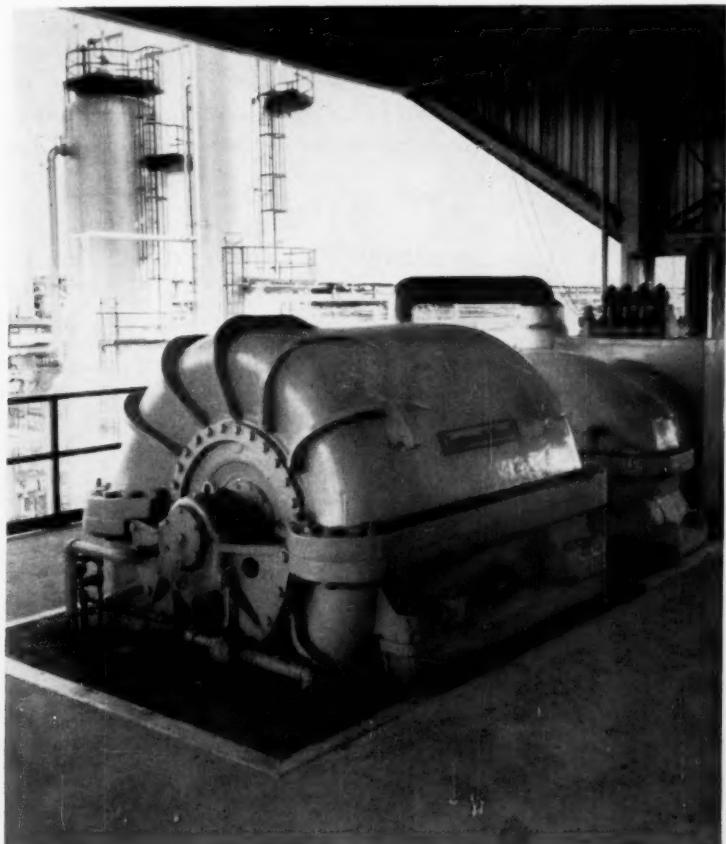


REGENERATOR-AIR BLOWER delivers 137,200 scfm., takes suction at 14.4 psia., discharges at 30.0 psia. It supplies combustion air and is driven by an 11,250-hp. turbine using steam at 575 psig. and 750 F.

ound

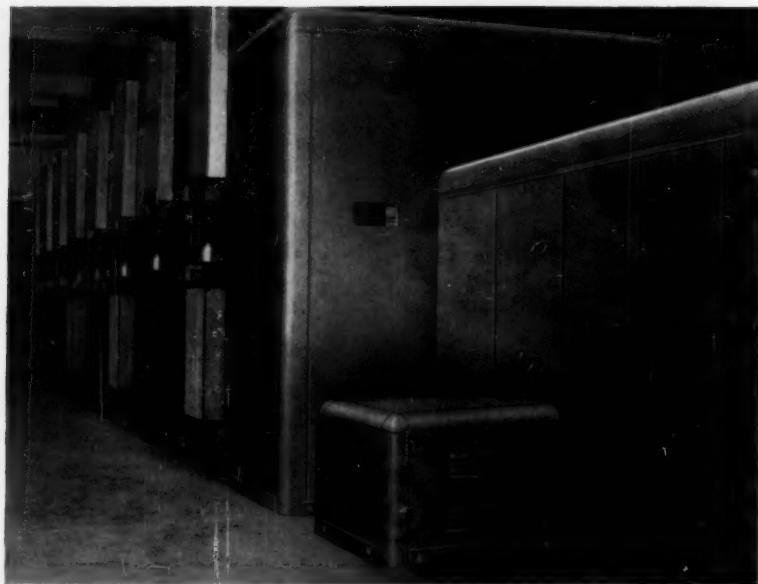


over and catalyst storage bins (left and
ber-deethanizer, fuel gas surge.



LIFT-AIR BLOWER is rated at 29,800 scfm., takes suction at 14.4 psia., discharges at 36.1 psia. Air circulates almost 90 tons/min. of catalyst.

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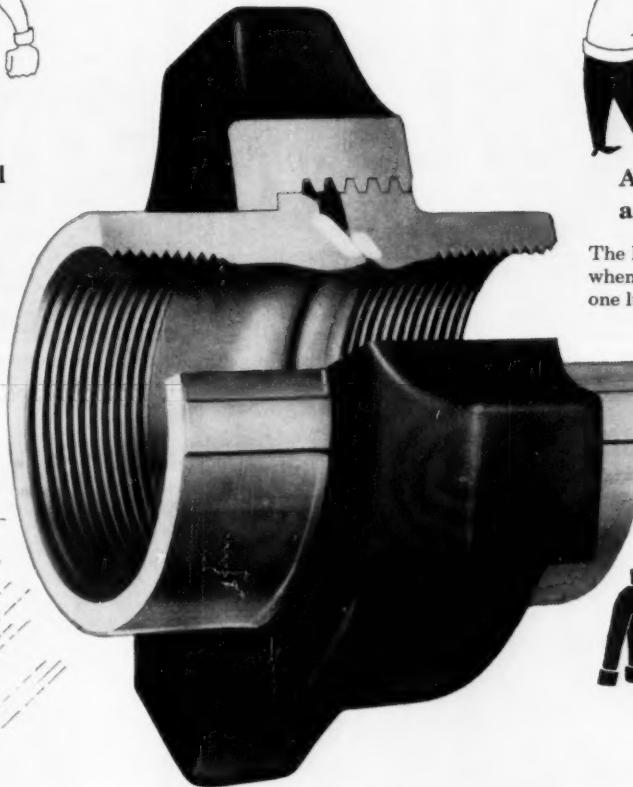
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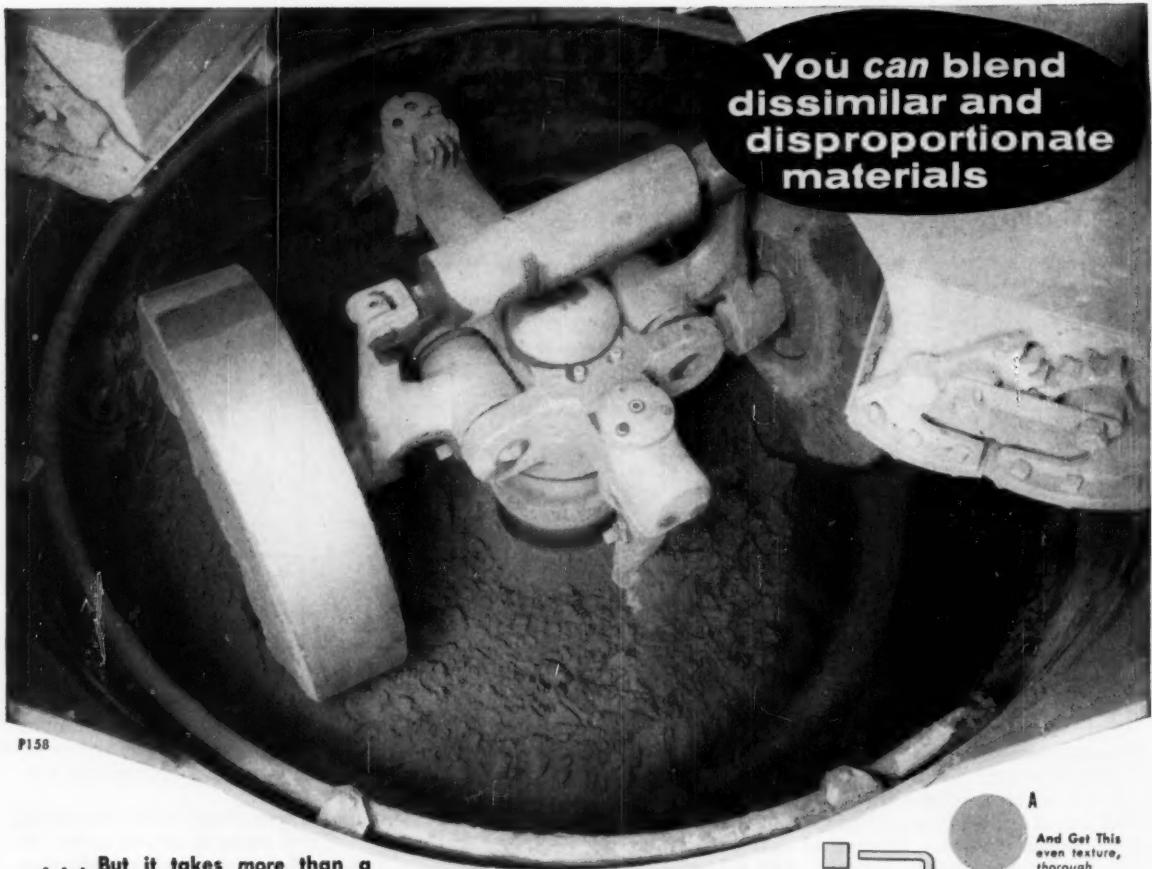
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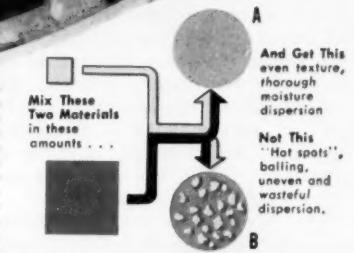
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Chemical Engineering

Practice

King-size "cat" has corresponding appetite 120

Processing at a total rate of 3,000 gpm., the Orthoflow fluid catalytic cracking unit of Tidewater Oil—the world's biggest unit—represents a lot of engineering effort.

Technique for making mountains from mole hills 129

Here's some expert advice on getting from pilot operations to full-scale plants. Both data and equipment scale-up are covered in this 12-page Feature Report.

Get the latest costs of heat exchangers 141

We present the first of a series of heat exchanger cost charts based on Provisional Data Sheets of the American Association of Cost Engineers.

One chart solves extraction design problems 142

Effectiveness of multi-stage countercurrent operations is determined by many variables. Now, one chart gives you their optimum values without tedious calculation.

How to correlate mass transfer coefficients 146

These methods explain the limitations and the use of mass transfer rate coefficients, when and how to supplement these data with experimental measurements.

You can save time in heat exchanger design 149

For streamline flow through the tubes of heat exchangers, these charts enable you to calculate rapidly tubeside heat transfer coefficients and pressure drops.

The story of an \$18,000/year strike 156

No matter what your opinion on unionization of engineers, this bipartisan report about engineers on strike is must-reading for every well-informed member of the profession.

OCT. 6, 1958

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ANOTHER

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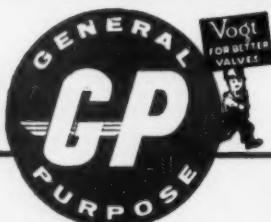
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FEATURE REPORT

Chemical Engineering

OCTOBER 6, 1958

How
to

SCALE UP

pilot
plant
data and
equipment

E. L. CLARK, Consultant, Pittsburgh, Pa.

THE ACID test of any pilot-plant program comes in the conversion of pilot-plant data into design parameters and operating conditions for the industrial plant. The results do not "just happen" to come out in a proper form, but are preformed by careful attention to detail during the entire experimental program. The realization that the end-use of the data is to be an extrapolation to industrial-size equipment is basic to our definition of a pilot plant. Thus each experimental-plant item must be designed with this end in view, and the experimental program must be arranged to provide data suitable for this extrapolation.

Our ability to extrapolate information from a small experimental unit to a larger industrial unit is a direct function of our ability to understand the effects of the variables involved. If we could write a set of simple relationships covering all the factors, the scale-up process could be reduced to a routine arithmetical procedure.

SCALE UP . . .

Unfortunately, such a situation is not always apparent or possible. There are many interacting variables which are difficult to reduce to simple relationships.

In addition to the chemical reactions involved, we are often confronted with problems of heat transfer, mass transfer and distribution. The rates of these processes in many cases affect the rates of the chemical reactions, and we encounter situations wherein changes in process variables may affect several competing or opposing processes in a different manner. Furthermore the size and geometry of the equipment can also affect these processes.

A logical approach to this problem is: be certain you know the characteristics of the chemical or physical changes taking place and that these changes are being observed in an experimental environment which approximates or is some function of the environment to which extrapolation will be made.

The first part of this report considers the problem of converting data obtained in the experimental

program to some logical and usable set of relationships. The effect of changing the size and geometry of equipment in which these data are obtained will be considered in the second portion as a direct exposition of extrapolation problems.

Organization of Data

The most obvious experimental data observed are the effects of temperature, pressure, time and concentrations of reactants on the production of some desired material. This information is required in selecting an economical production level and a proper return on invested capital. It's also necessary for understanding the effect of changes in process variables.

Very often these effects can be conveniently expressed as functional relationships. This is desirable for calculating various design possibilities. Furthermore such functional relationships are particularly useful in programming computers which can then optimize many-variable systems.

To obtain meaningful and reliable data, one must plan at the start of the experimental program. Considerable information is available on the proper design of experiments, but the discussion of this subject is beyond the scope of this report. It's important that we emphasize though that preliminary planning must be done.

In correlating results considerable help can be obtained by fundamental information on kinetics of simple reactions. This procedure often permits the treatment of complex reactions by incorporation of simplifying assumptions. Another approach for complex reactions is to evaluate the component reactions separately and to combine the various steps into some over-all relationship which fits the experimental result. By such a technique it may be found that one of the intermediate or component reactions is the rate-controlling step and the entire complex may be treated as a function of this one reaction.

A less time-consuming procedure is to find some algebraic expression which fits the experimental data adequately. In many cases we aren't interested in the entire range of process variables but in a relatively limited area which appears economically attractive. By using

these limits judiciously, simple relationships can sometimes be obtained which suit the particular area under investigation.

Kinetics of Simple Reactions

The simplest reaction involves a single molecule which reacts and evolves a product or products in a homogeneous system. The reaction rate depends on the concentration of the reacting material. This is a first-order reaction where the logarithm of reactant concentration is a linear function of the time at reaction conditions:

$$\ln \left(\frac{100}{100 - x} \right) = kt$$

where k = reaction rate constant, in reciprocal time units.

x = percentage of material which disappears during time, t .

t = time in convenient units.

The rate constant may be related to temperature by the Arrhenius equation:

$$\ln k = \frac{-E}{RT} + \text{constant}$$

where k = reaction rate constant.

R = gas law constant.

T = absolute temperature.

E = energy of activation.

This is a straight-line relationship between the logarithm of k and the expression $-E/RT$.

If we can show by a moderate amount of experimentation that the particular reaction under study acts like a first-order reaction, we can represent our data by two very simple relationships. Since both these relationships give straight lines on semi-logarithmic paper, the extrapolation or extension of our data becomes a simple matter.

Hydrocarbon Thermal Cracking

A surprising number of reactions are pseudo first-order reactions. The thermal cracking of petroleum hydrocarbons, provided that the amount of decomposition is limited to below 20-25%, can be expressed as a first-order reaction. Nelson¹ presents a series of curves showing the reaction rate constants for various petroleum fractions and hydrocarbons. Some of these are shown in Fig. 1.

Many hydrogenation reactions are pseudo first-order, even though the reaction depends on two molecules and should not fit a first-order



E. L. CLARK is a consulting engineer for the chemical, coal and nuclear industries. Headquartered in Pittsburgh, he's Russian-born, Boston-educated and has worked as an engineer in Israel and in the North, East and South United States.

Clark is a graduate chemical engineer from Northeastern University. His experience includes service with the Commonwealth of Massachusetts, Stone & Webster, Cities Service Refining Corp., the U. S. Bureau of Mines, and Israel Mining & Industries. Also he's taught and lectured in chemical engineering at the University of Pittsburgh and Catholic University.

plot. However, hydrogen is usually present in large excess and only the concentration of the molecule being hydrogenated is significant in determining the rate. Many polymerization and isomerization reactions follow a first-order reaction scheme as one might expect since these are often unimolecular reactions. Some behave differently when catalysts are employed.

The use of this correlating technique gives us additional information as to the type of resistance we must overcome in order to increase reaction rates. In Fig. 1, the slope of the lines give an activation energy in the 50 to 60 kilocalorie range. This indicates that at the conditions used for obtaining these reaction rate constants, there was little diffusional resistance.

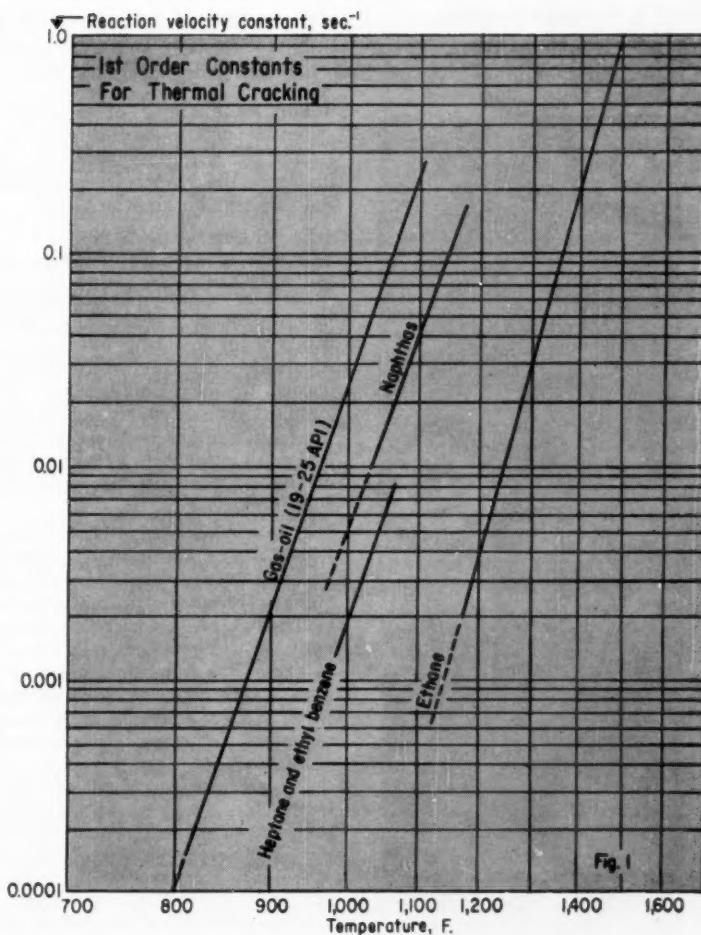
Another interesting point is that the reaction of thermal cracking is not limited to the gas-oil fed to the system. All products produced by gas-oil cracking themselves undergo decomposition or cracking. We can imagine a process of consecutive first-order reactions, each reaction having its own reaction velocity constant. By combining these, we can calculate the concentration of any intermediate product—such as gasoline—in a thermal cracking process.

If we permit the gasoline to remain at cracking temperature for a long enough time, we would appreciably reduce the yield of this desirable product. From Fig. 1, we can see that the rate of gasoline (naphtha) decomposition is much slower than that of gas-oil at any chosen temperature—as indicated by a lower reaction rate constant. In industrial units gasoline destruction is prevented by distilling it from the reaction system as soon as it is formed and by controlling reaction time and temperature.

Kinetics of Coal Hydrogenation

Another interesting use of this technique is given by Weller and co-workers² in organizing data for the hydrogenation of coal in batch autoclaves. It's postulated that the conversion of coal to a hexane-soluble oil proceeds through two consecutive first-order reactions.

The reaction rate constant for the first step—the conversion of coal to asphalt—was obtained by plotting the logarithm of the percent of organic matter in the coal



remaining against time as shown in Fig. 2. A quantity of this asphalt was isolated and the reaction rate constant for its hydrogenation similarly obtained from Fig. 3.

Both figures indicate the straight-line relationship between the logarithm of concentration and time. The slopes of the lines indicate the reaction rate constant since:

$$\ln(100 - x) = kt + \text{constant}$$

Knowing the two rate constants Weller uses the expression

$$A = \alpha C_o \frac{k_1}{k_1 - k_2} [e^{-k_2 t} - e^{-k_1 t}]$$

where A = asphalt present at time t .
 α = fraction reacted coal converted to asphalt.

C_o = coal at initial time.

k_1 = rate constant for coal conversion.

k_2 = rate constant for asphalt conversion.

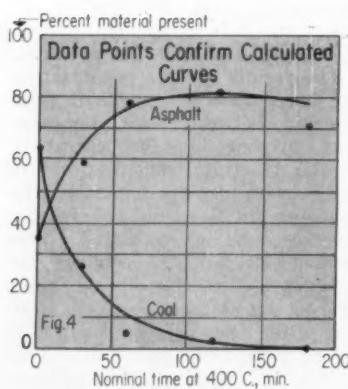
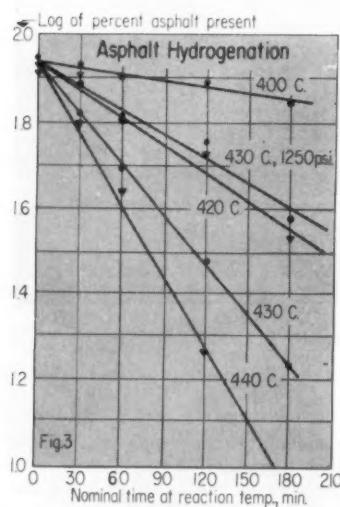
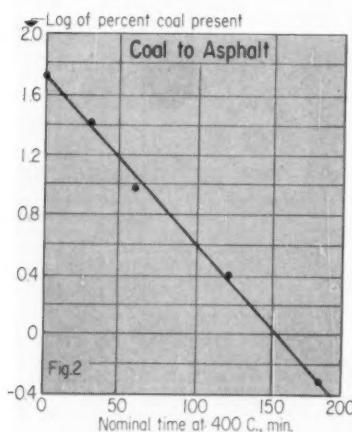
to calculate the concentration of asphalt present at any time.

In Fig. 4 the calculated concentrations are plotted against time and compared with the experimental values. The agreement is reasonably good. Pelipetz et al.³ extend this data to include the effect of catalysts and hydrogen pressure.

The results of data organization are to provide a convenient relationship between time, temperature, pressure and concentration. If the fraction reacted, pressure and temperature are stipulated, the time—or its function, the reactor volume—can be calculated. This type of calculation is seemingly independent of reactor size or shape. One tacitly assumes complete similarity of reaction conditions between large and small units. This similarity includes all conditions

SCALE UP . . .

Here's A Complex Reaction Correlated As First-Order



such as type of contact, extent of mixing, heat effects, reactant concentration, temperature, and pressure.

For an example of a complex situation where several rate constants for different reactions are involved, the reader is referred to Smith's text on kinetics.⁶

Techniques for Complex Reactions

In many cases—particularly for heterogeneous reactions where catalytic or reacting surfaces are involved—an empirical approach is needed to organize the data. The simplest type of expression of some generality might be the rate of reaction as a function of some power of the reactant, product or diluent concentration:

$$\text{Rate} = k(P_A)^n(P_B)^m(P_C)^o \dots$$

where A and B might be reactants and C a product or diluent; P represents the partial pressure or concentration of a particular component in the reaction mixture; m , n , and o are numerical exponents; k is a rate constant for the reaction. Weller⁵ suggests such an expression for many heterogeneous reactions.

In catalytic reactions, the exponents for very weakly absorbed products or diluents are often zero, simplifying the empirical rate expression. The exponents indicate the apparent order of the reaction with respect to the individual components and permit conventional experimental techniques for their determination (e.g., by varying concentration or partial pressure of one component at a time).

In many reactions it is found that the exponents do not change appreciably with temperature over the range being studied. Thus only the temperature dependence of the rate constant must be considered. The experimental work may be done on a very small section of a catalyst bed—a so-called differential reactor—and the rate expression integrated over a large reactor in which both concentration and temperature may vary.

A more elegant and time-consuming approach is to postulate probable mechanisms for a catalytic reaction, set up rate equations for the steps involved in each probable mechanism, and determine which of these equations best fits the experimental data. This procedure assumes that one step in the series is

rate-controlling and its rate equation fits the over-all reaction.

Weller⁵ discusses this approach and its basis and compares the accuracy of these rate equations with empirical equations of the form given above. For detailed description and examples of this type of data evaluation, the reader may consult Hougen and Watson's text.⁶

In general the simplified approach suggested by Weller, though empirical, is preferred for pilot-plant work. The primary purpose of data organization for a chemical reaction is to provide some functional relationship between time and amount reacted at various levels of temperature, pressure and concentration. This relationship can then be used to determine the size of reactor needed to evolve the desired amount of product in an industrial plant.

The type of data needed to determine the kinetic relationships discussed above can be obtained in laboratory or bench scale equipment. If we can set up these relationships which theoretically permit us to calculate reactor size for a desired throughput and yield, it's obvious that in some cases we can dispense with pilot-plant experimentation and can design a commercial reactor directly. However the primary problem in such an extrapolation is the lack of assurance that identical conditions will still exist as reactor size is increased. While minor variations as a function of size may not affect an extrapolation of one order of magnitude, these variations can grow to serious proportions in the jump of several orders of magnitude from laboratory to commercial units.

Data for Physical Processes

Similar techniques are applied to processes which do not involve chemical reaction. Here a diffusional resistance is usually encountered and the functional relationships are often empirical. Data are obtained on the time required for drying, mixing, absorption, solution or flotation under different conditions of temperature, pressure and concentration.

As in a chemical-reaction process, we attempt to evolve a functional relationship between time and a certain desired effect. The time may be expressed as heat transfer area, height of packed column, vol-

ume of flotation cell or size of drying chamber needed for a certain volume or weight of material to be processed per unit time. Still it's a time-rate relationship dependent on the same variables as those which affect rates of chemical reactions.

Time in Experimental Units

In the preceding discussion time has been repeatedly pointed out as a critical and important factor. Our chemical process industry has thrived through the use of highly productive, large, efficient units. The time required for a reaction or process operation measures the potential productivity of a capital investment and the fixed operating costs per unit of product. Hourly or daily throughput is merely the reciprocal of reaction or process time. A variation of 10-20% in productivity for a given industrial plant can create very large differences in its profitability. It is obviously important that we understand the inherent errors in the experimental determination of this variable.

The simplest type of reaction experiment uses a batch autoclave in which reactants are placed and kept at a given temperature and pressure for a certain period of time. The autoclave is then opened, and the extent of reaction is determined by analysis. It sounds simple. But the periods during which the autoclave is heated to reaction temperature and—after the reaction time—cooled so that it may be opened involve reactions at conditions other than those selected for investigation. If we know the effect of temperature on reaction rate we can convert the time spent at the lower temperatures during heating and cooling to an equivalent time at the desired reaction temperature. A similar adjustment may be necessary if pressure varies during the reaction period.

Usually these adjustments are minor since reaction rates are slower at the lower temperatures encountered during heating-up and cooling-down periods, but there are other possibilities. For exothermic reaction portions of the reaction mass may be heated to temperatures considerably higher than desired because of poor heat transfer. Then the corrections become quite significant. In addition, formation

of undesirable products may result. Thus, there are problems of determining reaction time even in a simple non-flow system.

In a flow system, we have the same problem of adjusting for variations in temperature and pressure. Kandiner et al.⁷ in determining time and temperature values for a coal hydrogenation pilot plant have presented a convenient method for tabulating and calculating these adjustments.

Another problem in a continuous system is the effect of expansion or contraction of reacting mixture volume during the reaction. A contraction of volume increases the time spent in the reactor, while an expansion decreases this time. Brinkley⁸ discusses a mathematical approach for correcting reaction time for such variations.

The usual technique is to disregard these factors and to use space velocity instead of reaction time. For ideal conditions this value is the reciprocal of reaction time and is expressed as volumes of feed per volume of reactor or catalyst bed per unit time. In cases where the feed to the system is a partly vaporized liquid, weight or volume of the liquid per unit time per volume of reactor (or per weight or volume of catalyst) is a time measure.

Another time measure is that of "space-time-yield"—expressed as product (volume or weight) per volume of reactor per unit time. This value is a more complex one, involving possible reaction and destruction of the desired product as well as its formation. Therefore it often shows a maximum, which is the preferred operating point for an industrial plant since it represents maximum product yield per unit of investment in reactor and catalyst.

Another important problem in reaction-time measurement is the conversion of data from batch to continuous operation. Most engineers realize that in a turbulent continuous system some portions of the reactants spend more time within the reactor than others; there's always a certain amount of by-passing. Ham and Coe⁹ and McMullin and Weber¹⁰ evaluate this problem and calculate the effect of using one or a multiplicity of completely stirred reactors on the reaction results for different order reactions. Both these results are for series of vessels of equal size. Kandiner¹¹ ex-

tends these equations to include series of vessels of unequal sizes and evaluates purging times and sampling lags.

Obviously if one assumes piston-type flow, the time spent in a reactor can be easily calculated by dividing the reactor volume by the volumetric throughput. If we have four 1000-gallon tanks in series, and a flow rate of 100 gal./min., it will require $4000/100 = 40$ minutes to displace the content of the four tanks assuming plug-like flow and no mixing within the tanks.

If we assume complete mixing in each of the four tanks and the same flow rate, it would require 66 minutes to achieve 90% displacement of the original content of the four tanks. If we use one stirred tank of 4000 gallons and the same flow rate, the time required for 90% displacement becomes 96 minutes, while for plug-flow only 40 minutes again is required. These results are calculated from curves presented by Kandiner¹¹ and give some indication of the effect of using stirred reactors.

Scale-Up Techniques

Most chemical engineers have become accustomed to making extrapolations of data from small laboratory-scale experiments to large-scale industrial applications. The entire fund of information compiled by the study of unit operations consists of such extrapolations. Each time an engineer uses a Reynolds number to calculate a pressure drop he is, in effect, extrapolating data from the laboratory results of Reynolds, Stanton and Powell, Nikuradse and a host of other experimenters who have developed the correlations currently in use. This type of extrapolation has become so well-accepted that it is not even considered to be an extrapolation process.

We are all familiar with less-understood unit operations for which our correlations are not as accurate. This is another way of saying that we find them more difficult to extrapolate. When chemical reactions are combined with a unit operation, our difficulties are increased—the extrapolation is more involved.

As previously stated, the first problem is to understand the effects of all process variables.

A. Cylindrical Tube Scaled-Up With . . .

Geometrical similarity—linear dimensions of large tube r times those of small.
Dynamic similarity—Reynolds numbers equal in both tubes.

Parameter	Small System	Large System	Derivations
Internal diameter	d	$D = rd$	For equal Reynolds numbers and the same fluid in both the tubes, the Reynolds numbers reduce to:
Length	l	$L = rl$	$du = DU = rdU$ or $U = u/r$
Velocity	u	$U = u/r$	
Volumetric throughput	$q = \frac{\pi}{4} d^2 u$	$Q = rq$	
Reactor volume	$v = \frac{\pi}{4} d^2 l$	$V = r^3 v$	
Contact time	$t = v/q = l/u$	$T = V/Q = r^2 t$	
Surface area	$s = \pi dl$	$S = r^2 s$	
Surface area/volumetric throughput	$s/q = 4l/du$	$S/Q = r(s/q)$	

The second problem is to realize the changes caused by increasing the scale of our operation to the industrial unit. We'll consider here several typical examples which may assist in solving other problems.

Criteria for Scaling Up

In order to properly scale up a chemical system we must set up some basis for maintaining a relationship between the results in a small system and those to be predicted for the larger system. We have previously presented techniques for evaluating yields of desired product as a function of throughput and process variables.

It's been mentioned that some reaction velocities depend more on physical or diffusional conditions than chemical reaction rates. In many endothermic reactions the reaction rate may depend on the rate of heat transfer. For others the rate may depend on diffusion of products or reactants through a gaseous or liquid film. For still others the important factor is only the rate of the chemical reaction itself.

The effect of temperature on the over-all reaction rate is one guide to determining the critical or rate-controlling step. Similarly, the effect of added turbulence determines the extent of diffusional or other film-type resistance.

Considerable information has been published on setting some basis of similarity for the transference of results from small to large equipment. Damkohler¹³ suggests five dimensionless groups which can be used as a means of equating conditions in large and small reactors. These would be used to denote reaction similarity as we utilize Reynolds numbers to denote equivalence of turbulence in various systems.

Johnstone¹⁴ discusses the work of Damkohler and suggests that the number of dimensionless groups can be reduced by including the Arrhenius relationship which relates reaction rate and temperature. He suggests the following groups for homogeneous and heterogeneous chemical reactions.

Homogeneous reactions — For first order reactions the dimensionless groups are: $(x_1 t)$ and (E/RT) where x_1 = a constant having the dimensions of the velocity constant for a first-order reaction, T^{-1} .

t = reaction time, T .
 E = energy of activation, $ML^2 T^{-2}$.
 R = gas constant, $ML^2 T^{-2} \theta^{-1}$.
 T = absolute temperature, θ .

The dimensions are the familiar M , L , T , θ representing mass, length, time and temperature.

For reactions of higher order the groups become: $(X_n a_1 \dots a_n t)$ and (E/RT) , where n denotes the order of the reaction and $a_1 \dots a_n$ denote concentrations of reactants.

The dimensions of X vary with the reaction order as do the dimensions of the velocity constant.

Heterogeneous reactions — Here a term is introduced to represent the quantity of surface available to the reaction and the dimensionless groups become:

$(X_n a_1 a_2 \dots a_n \sigma t)$ and (E/RT) where X_n = constant with varying dimensions depending on apparent order.

E = apparent energy of activation, $ML^2 T^{-2}$.

R = gas constant, $ML^2 T^{-2} \theta^{-1}$.

T = absolute temperature, θ .

a_1, a_2 = concentrations of substances $A_1, A_2 \dots$, ML^{-3} .

t = reaction time, T .

σ = interfacial surface area per unit volume of system, L^{-1} .

If the dimensionless groups for a large and small system are equal, then chemical similarity is considered to exist. This is achieved in a homogeneous system when the initial concentrations, time and temperature are equal. For a heterogeneous system the product σt , initial concentrations, and temperature shall be equal at all points.

Damkohler achieves similar results in considering this problem. His requirements for chemical similarity are: time of reaction should be equal; temperatures should be equal; the surface heat losses from large and small systems should be the same proportion of the total heat input. Actually the last requirement refers to those

scale-up cases where heat transfer rates affect the control of temperature.

Thus far we have not considered at all the problems of those reactions in which diffusion—or "dynamical resistance" as Johnstone¹³ suggests—is a controlling factor. Laupichler¹⁴ considers the rate of the water-gas reaction, a heterogeneous second-order reaction, to be governed by a term equivalent to $A \sigma t$. The value $1/A$ is the total resistance to the reaction and consists of two terms:

$$\frac{1}{A} = \frac{1}{kC_m} + \frac{\delta}{D}$$

where k = velocity or rate constant of the reaction.

C_m = mean concentration of water vapor.

δ = thickness of streamline film on catalyst surface.

D = diffusion coefficient of carbon monoxide through the gas film.

Thus $1/kC_m$ is the "chemical resistance" which will vary only with temperature and reactant concentration, while δ/D is the dynamical resistance which will be affected by the degree of turbulence or by changes in Reynolds number. If the reaction depends on a heat transfer rate, the dynamical resistance may be expressed as δ/K , where K is the thermal conductivity of the fluid film.

The relative effect of each resistance is an important scale-up consideration. In effect this statement reverts to our previous discussion of the "rate-controlling" step, but more definitely and exactly.

If the chemical reaction rate is low, the resistance due to dynamic considerations may be disregarded. Then the scale-up problem may only require that we maintain similar temperatures and contact times in the small and large plant with dimensional and dynamic considerations being disregarded.

At high temperatures or with rapid reactions, the problems of dynamic similarity in both large and small plants are the critical ones. The most difficult situation occurs when both resistances are appreciable. Then the design of the pilot-plant reactor usually must be a compromise between competing similarities, and therefore extrapolation becomes more difficult.

Effects of Changes in Size

All engineers have at some time or another considered the effect of

enlarging an experimental unit to increase its permissible production. Often the effects are predictable and understandable; occasionally an "exception" is encountered. Usually the so-called exception is merely a case where all effects of the enlargement were not considered nor completely understood. To illustrate this possibility, we have calculated several examples of the effects of size changes.

Example A—The first example shown in the table considers two cylindrical tubes, the larger of which is r times the smaller. We have postulated geometric similarity, which requires that the ratio of any corresponding dimensions in the two systems be equal to the size ratio r . If we further postulate dynamic similarity (equal Reynolds numbers), we completely fix all characteristics of the system.

The velocity in the large tube is $1/r$ times the velocity in the small tube. Also the contact time in the large tube is r^2 times that in the small tube, for these conditions.

Let us consider what this means in regard to scale up of a pilot-plant reactor which is a 1-inch diameter tube 5 ft. long. For a 10-fold increase in size ($r = 10$), we would have a 10-inch diameter reactor 50 ft. long with a volumetric throughput 10 times the smaller unit. This would give us equal Reynolds numbers in both small and large units, but a contact time in the large unit 100 times that in the smaller.

If we want to get equal contact or reaction times in the large and small reactors, the length of the larger tube must be reduced by a factor of 100 to 0.5 ft. However a reactor with these dimensions (10-in. diameter by 0.5 ft. long) is not too satisfactory. We can see at once that if we desire to maintain constancy of reaction time and Reynolds number in a scale-up, the small tubular unit must be longer than the larger unit.

In the example we have a reaction or physical change in which dynamical resistances are of importance. If we're concerned with heat transfer through the wall of the small reactor, another problem arises in the case of the larger unit. For example, the wall surface area in the larger reactor for equal contact times expressed as surface area per volumetric throughput of reactants is $\frac{1}{10}$ that of the small system. Thus we must insert additional

heating or cooling surface area into the larger reactor to obtain equivalent results.

Example B—For this example we've chosen a system described by Johnstone and Thring¹⁵ in their text on scale-up methods. Here we have a system in which reactants are fed into a tube where a homogeneous reaction is taking place. The effect of turbulence is considered to be negligible. For chemical similarity, though, the temperature and contact time must be identical in both large and small units. In order to have equal contact times, the initial and final pressures should be the same in both large and small units.

In Example B we've shown the relationships between feed rates, diameter and coil length that must exist for the assumed conditions. It's evident that no geometrical or dynamic similarity exists. The ratio of large and small diameters is considerably greater than the ratio of lengths of the large and small coils. Though the Reynolds numbers are different, it's assumed that turbulent flow exists in both coils.

If we examine Example B a bit more critically, we can appreciate that even for chemical similarity there's chance of scale-up problems. If we assume a volumetric throughput ratio (Q/q) of 100 (i.e., large system to handle 100 times the throughput of the small unit), the diameter ratio (D/d) of the tubes would be $(100)^{0.41} = 6.75$. The length ratio (L/l) would be $(6.75)^{0.41} = 2.18$.

The (surface area per unit volumetric throughput) ratio— $(S/Q)/(s/q)$ —calculates as $1/6.75 = 0.148$. And the Reynolds number ratio (N_{re}/n_{re}) = $(6.75)^{1.41} = 14.8$.

The heat transfer coefficient would be greater in the larger system, but not sufficiently greater to compensate for the smaller area available per unit of throughput. This can be calculated by assuming that the Nusselt number will vary as the 0.8 power of the Reynolds number.

If (HD/hd) is the ratio of Nusselt numbers for the two tubes:

$$(HD/hd) = (14.8)^{0.8} = 8.65$$

$$\text{Since } (D/d) = 6.75,$$

$$(H/h) = \frac{8.65}{6.75} = 1.28$$

$$\text{Then } \frac{(HS/Q)}{(hs/q)} = (1.28)(0.148) = 0.19$$

If the reaction under considera-

B. Circular Cracking Coil Scaled-Up With . . .

Turbulent flow in both coils.

Equal pressure drops, temperatures, and contact times in each coil.

Parameter	Small System	Large System	Derivations
Internal diameter	d	$D = d(Q/q)^{0.41}$	For equal contact times: $L = l(U/u)$ (1)
Length	l	$L = l(D/d)^{0.41}$	For turbulent flow, the friction factor can be expressed as a function of the Reynolds number: $f = 0.04(n_{Re})^{-0.16}$ and $F = 0.04(N_{Re})^{-0.16}$ (2)
Velocity	u	$U = u(D/d)^{0.41}$	For turbulent flow and equal pressure drops, Darcy's equation gives: $flu^2/d = FLU^2/D$ (3)
Volumetric throughput	$q = \frac{\pi}{4} d^2 u$	$Q = q(D/d)^{2.41}$	Combining equations (1), (2) and (3) gives: $U = u(D/d)^{0.41}$ and $L = l(D/d)^{0.41}$ (4), (5)
Reactor volume	$v = \frac{\pi}{4} d^2 l$	$V = v(D/d)^{2.41}$	From equations (4) and (5), other parameters for Example B are derived.
Contact time	$t = v/q = l/u$	$T = L/U = t$	
Surface area	$s = \pi dl$	$S = s(D/d)^{1.41}$	
Surface area/volumetric throughput	$s/q = 4l/du$	$S/Q = (s/q)/(D/d)^{1.41}$	
Reynolds number	$n_{Re} = q(4\rho/\pi d\mu)$	$N_{Re} = n_{Re}(D/d)^{1.41}$	

tion is one which requires addition of heat—such as thermal cracking of petroleum fractions—the larger area available for heat transfer per unit quantity of reactants in the pilot plant would permit a lower temperature differential across the tube wall than that needed for the larger unit. This condition would exist in spite of the slightly higher film heat transfer coefficient in the larger unit.

The higher wall temperatures needed in the larger unit may cause coking at the tube wall and other undesirable effects not observable in the pilot-plant unit. To avoid such a possibility, additional test work should be included in the pilot-plant program to investigate this effect of higher tube-wall temperatures on operability and product distribution.

Heterogeneous-System Examples

While conditions for chemical similarity have been discussed for heterogeneous reactions, it should be appreciated that quantitative relationships for reaction velocity in such systems are not well-established. It's often difficult to obtain equations governing the adsorption of products and reactants at catalyst surfaces. Often dynamical resistance is the primary rate-con-

trolling factor. Another problem in heterogeneous reactions is that the interfacial area may be mobile and variable, as in a liquid-gas system. In such reactions it's difficult to ensure that a relationship is maintained between the pilot plant and the industrial system.

Example C-1—Here we are considering a heterogeneous system in which there's a fluid reacting on a solid catalyst. In this case it's possible to calculate the solid surface interface which has been designated as σ . As indicated in Example C-1, geometrical similarity has been assumed extending even to the diameter of the catalyst granules.

If it's desired to maintain chemical similarity—equality of the dimensionless group $(X_a a_1, a_2, \dots, a_s, \sigma, t)$ —the contact time in the smaller system is shorter than that in the larger by the linear dimensional ratio of the two systems. This is compensated by the greater catalyst interfacial surface area in the smaller system. The velocity in the two systems is identical.

There are some obvious difficulties in making the above analysis. The assumption that the geometric surface of the catalyst is the important criterion governing the extent of reaction is open to question. In many cases the surface area is more a function of catalyst weight

or actual volume than of geometric surface.

Manufacture of two sizes of catalyst granules often introduces particle density differences for the two sizes with major differences in activity. For this reason it's wiser to utilize commercial catalyst particles in a pilot-plant program. This does not allow complete geometric similarity, but it eliminates a source of difference that's often difficult to analyze. It's assumed that the ratio of catalyst-bed pressure drop to inlet pressure is small enough to have an insignificant effect on contact time.

Example C-2—It's important and worthwhile now to consider the heat transfer and fluid film conditions of the system in Example C-1, as shown in Example C-2. Here the industrial unit is an uncooled reactor where the only heat removal is through natural convection from the external wall. The major resistance to heat removal is probably represented by the coefficient of natural convection.

Thus, as developed in Example C-2 in the table, for uninsulated reactors with geometrical and chemical similarity the heat loss per unit of throughput is the same in the large and small units. This is an important factor in simplifying scale-up of such a unit. Of course

C. Heterogeneous Reaction System

1. Cylindrical reactor with . . .

Geometrical similarity, including diameter of solid catalyst granules—linear dimensions of larger system r times those of smaller system.

Chemical similarity—equal dimensionless groups ($X_n a_1, a_2 \dots a_n \sigma t$).

Any type of reactor cooling—e.g., natural convection from reactor outer shell, water jacket surrounding reactor, or tubes or coils inside reactor.

Parameter	Small System	Large System	Derivations
Internal diameter	d	$D = rd$	For chemical similarity, and equal temperatures and reactant concentrations ($X_n a_1, a_2 \dots a_n$ is constant), then the value of the dimensionless group σt must be equal in both systems.
Length	l	$L = rl$	Contact time in small system = $t = v/q$
Reactor volume	$v = \frac{\pi}{4} d^2 l$	$V = r^3 v$	Contact time in large system = $T = V/Q = r^3 v/Q$
Catalyst granule diameter	d_e	$D_e = rd_e$	Also, $\sigma_e t = \sigma_e T$; or $\sigma_e v/q = \sigma_e/r(r^3 v/Q)$
Catalyst surface area per unit reactor volume	σ_s	$\sigma_l = \sigma_s/r$	Thus, $Q = r^2 q$, and $T = rt$
Volumetric throughput	$q = \frac{\pi}{4} d^2 u$	$Q = r^3 q$	
Velocity	$u = 4q/\pi d^2$	$U = u$	
Contact time	$t = v/q$	$T = rt$	

2. Same system as in C-1 with . . .

Reactor cooled only by natural convection from external wall.

Parameter	Small System	Large System	Derivations
External surface area	s	$r^2 s$	Major heat removal resistance is represented by a natural convection coefficient. The only internal condition affecting this is temperature, which is equal in both systems. Therefore, we can assume equal heat loss coefficients.
Surface heat loss coefficient/external area	h	h	
Surface heat loss	hs	$r^2 hs$	
Heat loss/volumetric throughput	hs/q	$r^2 hs/Q = hs/q$	

3. Same system as in C-1 with . . .

Reactor cooled externally by surrounding water jacket.

Parameter	Small System	Large System	Derivations
Modified Reynolds number	$n_{Re} = \left(\frac{d_e q}{d^2} \right) \left(\frac{4 \rho}{\pi \mu} \right)$	$N_{Re} = rn_{Re}$	Gas film is major heat transfer resistance—its coefficient as function of modified Reynolds number:
Heat transfer coefficient (b = a constant)	$h = (b/d)(n_{Re})^{0.7}$	$H = r^{-0.3} h$	For small system: $h = (b/d)(n_{Re})^{0.7}$; b = constant and, $n_{Re} = (d_e u \rho / \mu) = (d_e q / d^2)(4 \rho / \pi \mu)$
Heat transferred per unit volumetric throughput	hs/q	$HS/Q = r^{-0.3}(hs/q)$	For large system: $H = (b/D)(N_{Re})^{0.7}$; b = constant and, $N_{Re} = (D_e Q / D^2)(4 \rho / \pi \mu) = rn_{Re}$

Then: $(H/h) = (d/D)(N_{Re}/n_{Re})^{0.7}$ and, $H = r^{-0.3}h$

D. Heterogeneous Reaction System Scaled-Up With . . .

Chemical similarity.

Catalyst particles of equal size in large and small systems.

Volume of larger system r times volume of smaller system.

Parameter	Small System	Large System	Derivations
Reactor volume	v	$V = r^3 v$	For chemical similarity σ_l terms must be equal (see Example C).
Catalyst diameter	d_c	$D_c = d_c$	Contact time in small system $= t = v/q$
Catalyst surface area per unit reactor volume	σ_s	$\sigma_l = \sigma_s$	Contact time in large system $= T = V/Q = r^3 v/Q$
Volumetric throughput	q	$Q = r^3 q$	And, $\sigma_s t = \sigma_l T = \sigma_s T$
Contact time	$t = v/q$	$T = V/Q = t$	Then, $v/q = V/Q = r^3 v/Q$
Velocity			Thus, $Q = r^3 q$ and $T = t$
Geometrical similarity	$u = 4q/\pi d^2$	$U = ru$	
Equal velocities	$u = 4q/\pi d^2$	$U = u$	
Internal diameter			
Geometrical similarity	d	$D = rd$	
Equal velocities	d	$D = r^{1.5} d$	
Length			
Geometrical similarity	l	$L = rl$	
Equal velocities	l	$L = l$	

this example assumes that catalyst activity is proportional to catalyst geometric surface, and that our dimension group really signifies chemical similarity.

Example C-3—A different result is obtained if the catalytic reactor requires cooling through the use of water jackets or water-tubes within the catalyst bed, as in Example C-3.

Under such conditions the major resistance is represented by the gas film coefficient, which is a function of a modified Reynolds number within the catalyst bed. Leva et al.¹⁰ have correlated the gas film coefficient for cooling in packed tubes by an approximate relationship:

$$h = 0.4 \frac{k}{d} \left(\frac{d_c G}{\mu} \right)^{0.7}$$

where h is the film coefficient based on tube surface; d is the tube diameter (reactor in this case); d_c is the particle diameter (catalyst granule here). Thus $\left(\frac{d_c G}{\mu} \right)$ is a modified Reynolds number.

From the relationships derived for this example, in a large unit 10 times the linear dimension of a pilot-plant system, the heat transferred through water cooling of the

external shell per unit volumetric throughput of reactants would be $10^{-0.5}$ or about $\frac{1}{2}$ that obtained in the small unit.

Example D—Here we've eliminated the assumption that catalyst activity and geometric surface area are identical by using similar catalyst particles in both small and large units. We have retained the volume ratio between units of r^3 used in Examples A through C.

For equal contact times the volumetric flow rate in the large unit is r^3 times the flow rate in the small. For geometrical similarity (equal length to diameter ratio for both reactors), a higher velocity is obtained in the larger unit. This would result in higher Reynolds numbers and different heat transfer rates and pressure drops for the larger unit. However, if the diameter ratio of the two units were $r^{0.5}$ and the units were equal in length, then velocities would be equal as would the Reynolds numbers.

For two tubes of geometric similarity, charged with identical catalyst particles, the heat transfer conditions are not similar. The surface heat loss by natural convection per unit of throughput in the

smaller unit would be r times the amount in the larger unit.

The heat transfer coefficient for the gas phase in the larger unit would be $r^{-0.5}$ times the smaller unit. The heat transferred per unit volumetric throughput in the smaller unit (for gas-phase resistance controlling) would be $r^{1.5}$ times that in the larger unit. This calculation is made as shown in Example C, and assumes that the tube wall is used as the cooling surface.

Use of industrial catalyst particles in a small reactor requires some care in avoiding excessive "wall effects." The diameter of the catalyst tube should be at least six to eight times the diameter of the particles. Since industrial catalyst pellets are usually at least $\frac{1}{4}$ inch to $\frac{1}{2}$ inch in diameter, the experimental unit must therefore not be smaller than 2 to $2\frac{1}{2}$ inches in internal diameter. This requirement is similar to that suggested for pilot-plant fractionator or absorber column packing.

Example D can also be considered from the point of view of a fluidized catalytic reactor. The importance of the fluidized technique has been amply demonstrated in many processes. Usually the catalyst particles

are identical in both industrial and pilot-plant units.

If we consider the situation for identical catalyst in geometrically similar tubes as shown in Example D, we realize at once that the difference in velocity is a very important factor. Tests made in a small reactor cannot always be scaled up.

For a diameter ratio of 20-30 between small and large units, the velocity in the large unit will be 20-30 times that in the smaller unit. This would be beyond the fluidization range for the catalyst particles, and they would be carried out of the larger unit. A decrease in velocity would result in a different contact time for the large unit.

This situation has been resolved in two ways. Some experimental units have been operated with mechanical stirring of the fluidized bed to permit using low velocities. Another alternative is to have the experimental unit sufficiently long to avoid excessive velocity variations between large and small systems.

Unit Operations Scale-Up

While the discussion on scale-up techniques has been oriented towards systems involving chemical reactions and equipment for such processes, the same general approach is applicable to scale-up of unit operations and other processes involving physical changes. The difficulties encountered in scaling up heat transfer and other diffusional and transport processes has been mentioned in the discussion. We can use Examples A through D to evaluate the scale-up effects on heat transfer or other diffusional processes where the film thickness at a surface is the controlling factor. The Reynolds number can be considered as a measure of this thickness.

A similar approach to the problems of scaling up mixing equipment has been presented by Jordan.¹² In his illustration the Nusselt group with the film coefficient of heat transfer is found to be a function of the modified Reynolds number. He points out that the ratios of impeller speeds in two geometrically different systems depends on the functional relationships between the desired result (Nusselt group here) and the Reynolds number. He thus indicates that the common approach to scale-

up of mixing equipment—constancy of power input per unit volume—may not always hold.

Only if the desired result varies as the 0.75 power of the Reynolds number will the power input per unit volume be identical for both large and small units. Often such a relationship does hold—e.g., most heat transfer rates in mixing equipment do vary as the 0.6-0.8 power of the Reynolds number.

Unit operations involving equilibrium stages or plates such as fractionation, absorption or extraction can usually be projected to the industrial scale without pilot-plant study as we've mentioned before.¹³

The use of simple models is a "scale-down" technique which is applicable to many physical processes. Again the unit operations for which these methods can be used have been discussed.¹⁴ In all cases we should be certain that our model is a truly representative one. For example the use of a unit filtration area is a quite common method for evaluating the performance of an industrial filter. The particles and the fluid-solid mixture fed to our pilot-plant system must be identical to those processed on the industrial scale. The geometry of the filtration unit and the turbulence in the slurry chamber are important.

Extrapolating Corrosion Effects

Another important area for pilot-plant investigation is the determination of economical materials of construction. In many cases, the pilot plant is built with this factor as its primary purpose. The step from the glass equipment of the laboratory to the use of standard construction materials is important.

There is a tendency to oversimplify the corrosion problem in the pilot plant by considering that the effects of corrosion and erosion in the pilot plant are exactly indicative of the industrial-scale effects. The problems of the chemical reactions causing deterioration of materials of construction must be considered in the same manner as the reactions which form the products. Scale-up of various items of equipment may change the velocities and concentrations of materials in such a direction as to seriously increase the rates of corrosive reactions. Variations in heat transfer conditions on scale-up may result in higher metal temperatures at some points.

For example, consider a simple boiler tube in a power plant. The type of water passing through this tube, its velocity of flow and the temperature can easily be simulated to evaluate the corrosion rate under operating conditions. It is much more difficult to simulate the heat transfer rate through the wall of the tube and the surface properties of the tube which exist under normal boiler operation. Yet these conditions probably affect corrosion rates of tubes in commercial boilers.

Design Pilot for Scale-Up

Size variation effects between experimental and industrial units indicate the importance of considering scale-up problems in pilot-plant design. One can simplify these problems by evaluating the situation in advance. The scope of this discussion is not sufficient to include all factors for every process. We'll tell some of the difficulties which may be encountered trying to satisfy all conditions dictated by the various similarities. One must realize that similarities are not exact values, particularly for heterogeneous reactions.

Bosworth¹⁵ discusses the problem of the difficulty of satisfying all the dimensionless terms suggested by Damkohler. He concludes that it's only possible to obtain complete similarity between experimental model and industrial prototype by varying catalyst activity or by using geometrically dissimilar units. The same result has been demonstrated in our discussion. The design of the model and its relation to the industrial unit will vary with the dominant factor which regulates the process.

In each of our examples we've considered a different situation and evaluated the parameters and their effects. In the first system the design criterion was geometric and dynamic similarity. It was shown that the experimental system—a tubular unit—should be considerably longer than the industrial unit to permit equal contact times. If heat loss from the tube surface is a critical factor, adiabatic windings will be needed to control this loss in the smaller unit due to its larger surface area per unit volume.

A similar situation in the length of the pilot-plant unit was noted in the second system, where equal

pressure drops across the reactor were maintained in both systems. Again in the last example we noted considerable advantage in a pilot-plant reactor of greater length. The only exception was Example C.

Most pilot-plant reactors are too short to obtain simplified scale-up relationships. A long, thin experimental reactor does introduce operating problems of temperature control and difficult clean-up and maintenance, but the ease of scale-up is considered much more important in the over-all picture. Actually there's considerable advantage in the use of a pilot-plant reactor of length equal to the projected industrial unit. This is equivalent to using an element of the industrial unit as our model or test system.

Many industrial processes have been developed by such techniques. The first Houdry cracking reactors were essentially a bundle of small tubes containing catalyst, heated by a fused salt bath. The German Fischer-Tropsch reactors were similarly designed as was the Downs converter for phthalic anhydride production. In all these cases the experimental unit consisted of a single tube while the industrial reactor had many tubes, each identical to or larger than the original experimental unit. Both reaction time and heat or material transfer were important factors. These cases are similar to our Example D, where we find that both velocity and contact time can be kept identical by tubes of similar length and suitable diameter-throughput-volume ratios.

Tips for Using Elements

Industrial unit elements as test systems are often used for many unit operations. The common tubular heat-exchanger is made of a number of tubes—each easily capable of being an experimental system for finding the appropriate film coefficient. Screens and filters are designed based on the action of a section or unit area in an experimental system.

Care must be taken that the flow distribution and surface or wall effects are similar. It is simple to evaluate one tube of a tubular reactor or heat exchanger. Consider-

ably more thought must be given to the experiment where the pilot unit is a section of a much larger diameter reactor. Though the wall of the experimental unit may be a heat transfer surface, it must be remembered that a different situation can exist in the larger unit if heat transfer surfaces of different shape and spacing are required.

Where highly exothermic reactions are being investigated, a good value to determine is the maximum distance which can be allowed between a catalyst particle and the nearest heat exchange surface. This value will eliminate much uncertainty about the safe design of the industrial unit. For an adiabatic reactor, the small unit must be designed so that the rate of heat loss can be controlled to simulate that of the larger unit with its lower surface per unit throughput.

Where heat must be supplied to the reactor, the problem is a bit more difficult. In an elemental model, the maximum allowable distance from a heating surface can be determined. For furnace design, one of the parallel furnace tubes can be used as a pilot unit. In the second article²⁰ in this series, such a case was described (the development of an acetic-anhydride-from-acetone-process). Here the same size furnace tube was used in the pilot plant and the large multi-tube production furnace.

In experimental work with dense-phase fluidized beds, velocity limitations imposed by such a system are an added factor. If in scaling up the experimental unit the length is increased, there's an excellent possibility that the velocity increase will cause excessive carryover. A further complication is decrepitation of catalyst particles. Again it's very important that the experimental-unit length approach that of the production unit.

Point-Conditions Important, Too

The same problems in the scale-up of chemical reactions must be solved also for physical changes. Where separation or transport processes must be evaluated on a pilot-plant scale, the techniques discussed for chemical reactions can be utilized.

In many cases, though, a more serious difficulty arises. Changes in size and geometry may affect the *average* conditions in a uniform and predictable manner. But the effect on conditions at some specific *points* may have unpleasant results.

An example of such a situation might be a corrosive reaction on the wall of the vessel or conduit. If conditions exist at some point in the system which increase the rate of such a reaction, serious failures in the industrial system can result. Another example is carbon formation in a high-temperature system. A point-condition may exist which can plug the system just as effectively as a major oversight in the over-all scale-up.

System scale-up is far from an exact science, although one certainly can use scientific techniques in its accomplishment. Possibly the need for some "guessing" and the satisfaction at occasionally guessing right are the spicy ingredients that attract so many of us to the problems of the pilot plant.

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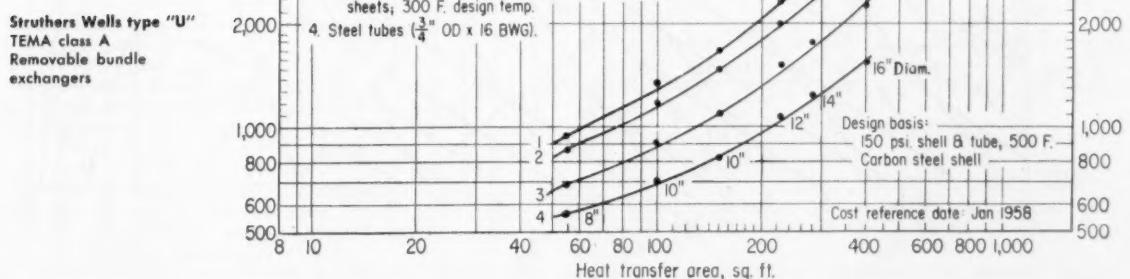
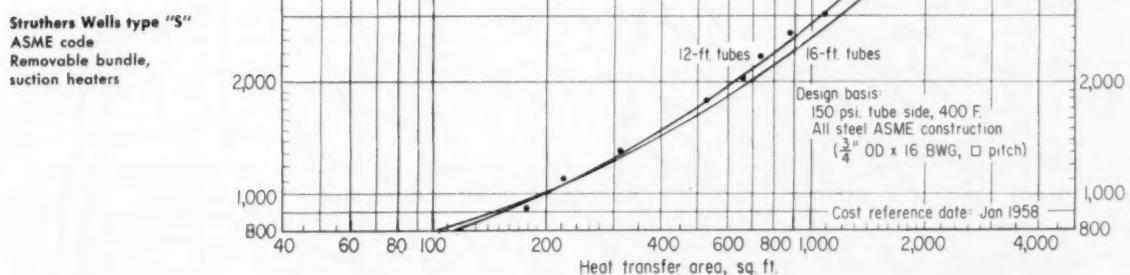
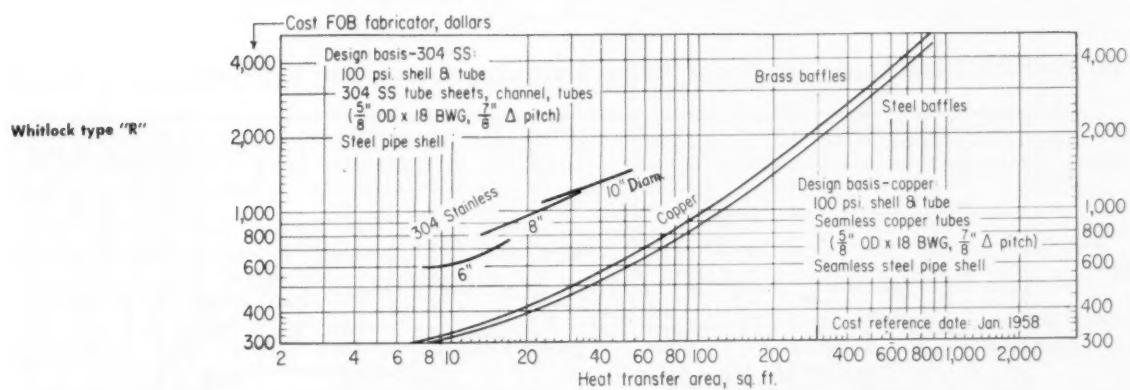
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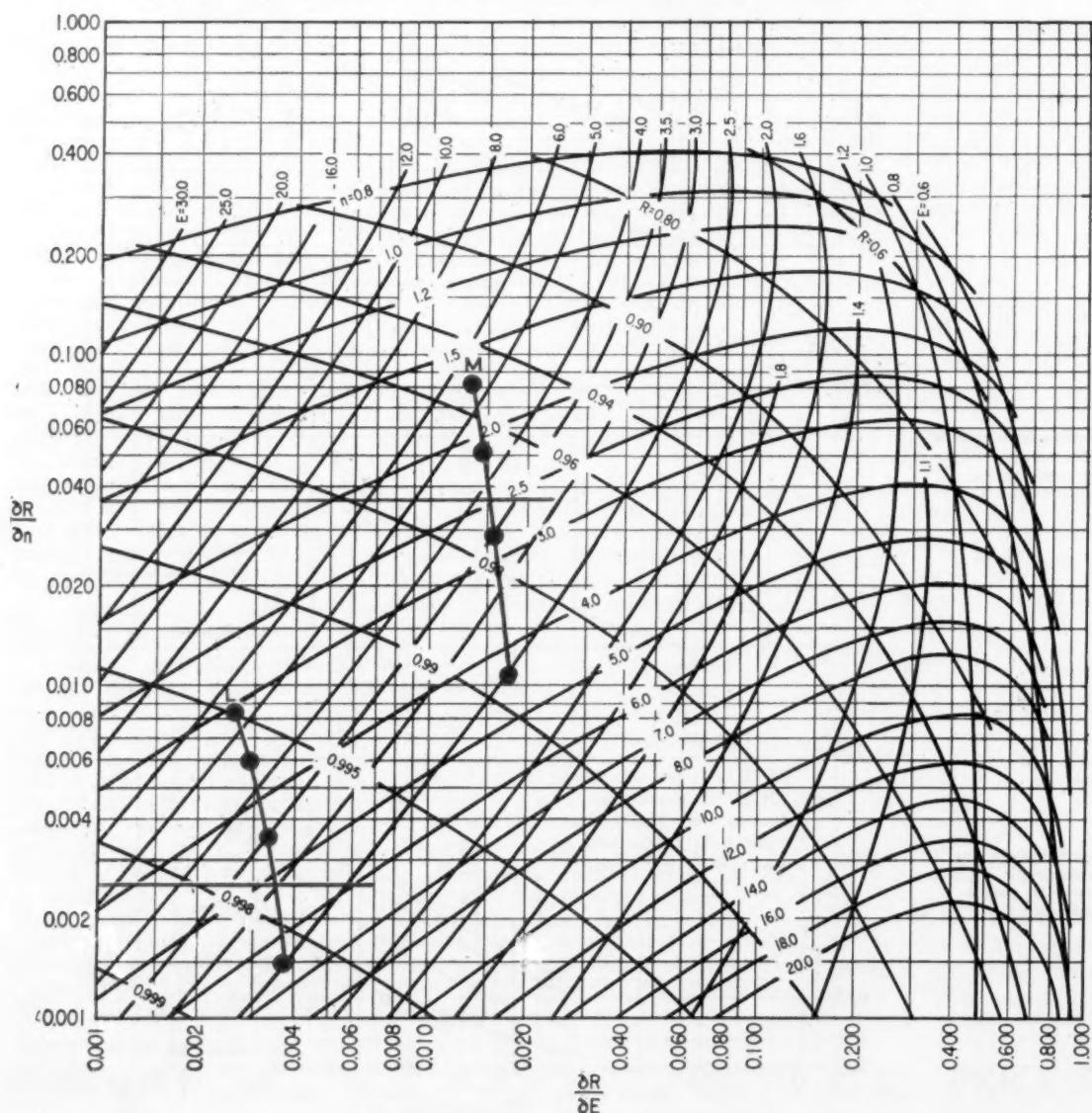
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Use Graph to Design for

Intersection Gives Optimum No. of Stages, Extraction Factor and Recovery



Optimum Economic Extraction

Now you can determine optimum economic values for variables in countercurrent, multiple-stage operations. One graph solves the equations.

ROBERT S. OLSON, Project Leader, Research Dept., Dow Chem. Co., Pittsburg, Calif.

SOLVENT extraction, decantation and absorption are often set up as countercurrent, multiple-stage operations. Effectiveness of these operations is fixed by the feed ratio, distribution coefficient and number of theoretical stages.

You can determine optimum operating conditions for any of these systems by calculating the efficiency at several values of the operating variables. This is a long, tedious and time consuming procedure.

In many systems, you'll find the distribution is linear or nearly so; i.e., $y = mx$. This means you can find the optimum design point mathematically.

There's an equation¹ to calculate the optimum number of stages. Unfortunately, it's very complex and requires repetitive calculation.

Graphs are also available² for determining the optimum feed ratio and number of stages for extraction columns at a given recovery. These graphs are limited because of the assumptions made and because you must pick a figure for the recovery.

On top of this, neither the equation nor the graphs gives a design based on incremental investment.

Chart Solves Equations

When the distribution is linear, recovery R is related to the extraction factor E and the number of stages n by the Kremser relationship:^{3, 4}

$$R = \left(\frac{E^{n+1} - E}{E^{n+1} - 1} \right) \quad (1)$$

Nomenclature

A	Feed rate of phase <i>X</i> , gpm.
B	Feed rate of phase <i>Y</i> , gpm.
E	Extraction factor, mB/A .
F	Feed.
I	Capital investment, \$.
m	Distribution coefficient, y/x .
N	Terminal stage.
n	Number of theoretical stages.
R	Recovery, $(x_F - x_S)/(x_F - y_F/m)$.
r	Value of recovered material, \$/day.
s	Cost of stages, \$/day/ Δn .
t	Cost of extraction factor, \$/day/ ΔE .
X	Phase solute is removed from.
x	Concentration of solute in phase <i>X</i> , lb./gal.
Y	Phase solute is transferred to.
y	Concentration of solute in phase <i>Y</i> , lb./gal.

Here, the extraction factor $E = (mB/A)$ and recovery $R = (x_F - x_S)/(x_F - y_F/m)$. Taking the partial derivatives of Eq. (1) gives the optimum design points.

Optimum design with respect to the number of stages n :

$$\frac{\partial R}{\partial n} = \left[\frac{(E^{n+1})(E - 1) \ln E}{(E^{n+1} - 1)^2} \right] \quad (2)$$

Optimum design with respect to the extraction factor E :

$$\frac{\partial R}{\partial E} = \left[\frac{(nE^{n+1}) - (n+1)(E^n) + 1}{(E^{n+1} - 1)^2} \right] \quad (3)$$

In Eq. (2), we have the optimum recovery with respect to the number of stages. Increasing the number of stages increases the recovery. Any increased cost due to increasing the number of stages must equal the greater value of the increased recovery:

$$ds = dr \quad (4)$$

Multiplying Eq. (4) by (dR/dn) and rearranging, gives:

$$dR/dn = \frac{(ds/dr)}{(dr/dR)} \quad (5)$$

At optimum conditions:

$$\left(\frac{\partial R}{\partial n} \right)_E = \lim_{\Delta n \rightarrow 0} \frac{(\Delta s/\Delta n)}{(\Delta r/\Delta R)} \quad (6)$$

$= \frac{\text{increase in cost with addition of } n}{\text{increase in value with increase in } R}$

In the same way, the optimum with respect to E :

$$\left(\frac{\partial R}{\partial E} \right)_n = \lim_{\Delta E \rightarrow 0} \frac{(\Delta t/\Delta E)}{(\Delta r/\Delta R)} \quad (7)$$

$= \frac{\text{increase in cost with increase in } E}{\text{increase in value with increase in } R}$

You can calculate the optimum values of n and E from Eq. (2) and (3) after determining optimum $(\partial R/\partial n)$ and $(\partial R/\partial E)$ from Eq. (6) and (7) given above.

However, it's more convenient to use the chart given in this article. Here, n and E are shown as a function of $(\partial R/\partial n)$ and $(\partial R/\partial E)$. Number of stages, extraction factor and recovery are read directly from this chart at the intersection of optimum $(\partial R/\partial n)$ and $(\partial R/\partial E)$.

This procedure is an incremental investment-return

Data for Example 1: Countercurrent Decantation

E	$I, \$$	$\Delta I, \$$	Invest., \$/Day, $(\Delta I \times 0.4)$ 365	Entrain., \$/Day	Total Cost, \$/Day, $(\Delta t/\Delta E)$	$(\partial R/\partial E)$, $(\Delta I/\Delta E)$ $(\Delta r/\Delta R)$	E
2	461,000	127,000	139	8	147	0.00367	2.5
3	588,000	112,000	123	8	131	0.00327	3.5
4	700,000	96,000	105	8	113	0.00282	4.5
5	796,000	87,000	95	8	103	0.00258	5.5
6	883,000						

method. Optimum design is set so the last increment of investment yields a specified return.

The usual elements of cost make up the factors $(\Delta s/\Delta n)$, $(\Delta t/\Delta E)$ and $(\Delta r/\Delta R)$. These in turn determine $(\partial R/\partial n)$ and $(\partial R/\partial E)$. You must examine each case to determine how much each element contributes.

This method uses changes in costs as E and n change, rather than absolute costs; a great simplification because many costs don't change very much with changes in E and n .

What's the Range of the Chart

Although the chart is designed for linear distributions, you can use it, with some accuracy, on systems that are only moderately linear—if the number of stages is small. In these cases, use an average distribution coefficient. Verify the accuracy by comparing recovery predicted from the chart with that calculated from an operating diagram.

Using Eq. (1) for solvent extraction and absorption is well recognized,^{5,6} and similar equations for countercurrent decantations have been proposed.^{7,8,9}

In countercurrent decantation, the concentration of solute in the underflow and overflow solutions are equal and the distribution coefficient m is therefore equal

to 1. If the amount of solution in the feed pulp and underflow slurry are equal, then the ratio of wash liquor (or overflow) to underflow solution is equal to B/A . This becomes the extraction factor E .

Actually, the feed and underflow pulps don't often have the same solution content. Cahalan¹⁰ calculated such cases and found the difference doesn't affect the optimum design point determined with this method (except in extreme cases).

For example: In a three-stage system with an extraction factor of 1.5, the ratio of feed to underflow was varied from 0.63 to 1.25. Optimum point shifted less than 10%.

Example 1: Countercurrent Decantation

You want to design a system to recover uranium from a leach pulp containing 60% solids by countercurrent decantation with wash water. Plant capacity is 1,000 tons of solids/day with soluble uranium content of 5 lb./ton of solids.

Uranium in the number one overflow (pregnant) solution is worth \$8.00/lb. Thickener underflows are 60% solids and thickener design area is 4,000 sq. ft.

Soluble uranium treated in the plant at 100% recovery ($R = 1$) is worth:

$$\Delta r/\Delta R = (1,000 \times 5 \times 8)/1 = \$40,000/\text{day}$$

Capital investment per thickener, including auxiliaries and installation, is estimated at \$75,000. We'll take the cost of capital, for this example, at 40%/year (30% return plus 10% depreciation).

Cost/stage-day then becomes:

$$(75,000 \times 0.4)/365 = \$23.00/\text{stage-day}$$

Except for the cost of additional flocculating agent, we'll assume operating costs for each added stage are negligible. Flocculant requirements are 0.02 lb./ton at a cost of \$1.00/lb. Flocculant requirements are:

$$1,000 \times 0.02 \times 1.00 = \$20.00/\text{stage-day}$$

Total cost for each added stage is:

$$\Delta s/\Delta n = (20.00 + 82.30)/1 = \$102.30/\text{day}$$

And, for optimum conditions:

$$\partial R/\partial n = 102.30/40,000 = 0.00255$$

Number one overflow (pregnant) solution B is processed by solvent extraction; cost of this depends on



Meet Your Author

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In 1951 and '52 Olson spent time in South Africa to help develop the ion exchange process now used in the uranium industry. He received his education—interrupted by war duty in the Navy—at San Francisco City College, Texas Christian University and the University of California at Berkeley, where he received a B.S. in Chemistry in 1948. Olson is a member of the ACS, AIME and the AAAS.

Data for Example 2: Solvent Extraction

E	B , Gpm.	I , \$	ΔI , \$	Invest., \$/Day, $(\Delta I / \Delta E)$	$(\partial R / \partial E)$, $(\Delta I / \Delta E)$ $(\Delta r / \Delta R)$	E
2	60	46,640	12,840	14.08	0.0174	2.5
3	90	59,480	11,240	12.33	0.0152	3.5
4	120	70,720	10,120	11.09	0.0137	4.5
5	150	80,840	9,360	10.14	0.0125	5.5
6	180	90,200				

the size of the stream processed. Plant investment for this portion of the plant is estimated as:

$$I = \$18,000(B, \text{gpm.})^{0.6}$$

Operating costs, other than solvent loss, are assumed independent of B . Entrained solvent losses are 0.02% of the volume of B . Solvent cost is \$0.25/gal. Volume of solution in the underflow A , at a density of 1.0, is:

$$A = 1,000 \text{ ton solids/day} \times \text{ton pulp/0.6 ton solid} \times 0.4 \text{ ton solution/ton pulp} \times 2,000 \text{ lb./ton} \times \text{day}/1,440 \text{ min.} \times \text{gal./8.34 lb.}$$

$$A = 111 \text{ gpm.}$$

Since $E = (mB/A)$, and $m = 1$, number one overflow $B = 111$ gpm./unit extraction factor E .

Cost of entrainment is then:

$$111 \times 60 \times 24 \times 0.0002 \times 0.25 = \$7.98/\text{day}\cdot E$$

Cost of extraction factor E , in terms of investment cost (40%/year) and entrainment loss, as well as optimum $(\partial R / \partial E)$ are calculated and shown in Table 1.

From these values, we've plotted $(\partial R / \partial E)$ as a function of E on the chart as line L . Optimum $(\partial r / \partial n)$ is also plotted and the intersection of the two lines gives you the optimum economic design as 5.1 theoretical stages at an extraction factor of 3.1. Recovery is 99.7%.

From this:

$$B = 111 \times 3.1 = 344 \text{ gpm.}$$

Example 2: Solvent Extraction

You want to recover vanadium by solvent extraction from a 300-gpm. by-product stream containing 1.0-gm. V_2O_5 /liter. Solvent cost is \$0.25/gal. and the distribution coefficient m between the solvent and solution is 10. Feed solvent contains 1.0-gm. V_2O_5 /liter because of incomplete stripping. Value of vanadium in the extract is \$0.25/lb. of V_2O_5 (value of product minus cost of process from extract to product).

Recoverable vanadium is:

$$\frac{x_F - (y_F/m)}{x_F} = \frac{1.0 - (1.0/10)}{1.0} = 0.90 \text{ or } 90\%$$

Plant stream contains:

$$300 \times 1.0 \times 0.00834 \times 60 \times 24 = 3,600 \text{ lb. } V_2O_5/\text{day}$$

Of this, 90% is recoverable:

$$3,600 \times 0.90 = 3,240 \text{ lb. } V_2O_5/\text{day}$$

With an increase in recovery the increase in value will be:

$$\Delta r / \Delta R = (3,240 \times 0.25)/1 = \$810/\text{day}$$

Installed cost/stage for the extraction plant is estimated at \$28,000 and this is independent of the solvent feed rate B . Any increase in operating costs with an increase in number of stages is assumed negligible. Taking the cost of invested capital at 40%/year, the cost of each added stage is:

$$\Delta s / \Delta n = (28,000 \times 0.40)/365 = \$30.70/\text{day}$$

And, at optimum conditions:

$$\partial R / \partial n = 30.70/810 = 0.0379$$

Operating costs of the stripping step, where the solute is removed from the extract, are assumed independent of the feed rate B . However, plant investment cost for this stripping operation is a function of the feed rate B . It's estimated as:

$$I = 4,000(B, \text{gpm.})^{0.6}$$

Investment costs as a function of E are shown in Table 2 along with optimum values of $(\partial R / \partial E)$.

Optimum values of $(\partial R / \partial E)$ as a function of E are plotted on the chart as line M as well as the optimum value of $(\partial R / \partial n)$. Design conditions that give the optimum economic points are found at the intersection of these two lines and are: 2.4 theoretical stages with an extraction factor of 3.9. Solvent feed is:

$$B = (3.9 \times 300)/10 = 117 \text{ gpm.}$$

Recovery of vanadium is 0.98. This corresponds to an 87% over-all recovery since 90% is the maximum recoverable.

Both examples shown contain several simplifying assumptions; but you can easily handle more complex problems by this same method. In some cases a series of approximations is necessary.

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Since experimental measurements are necessary . . .

- Where do we get rate coefficients?
- When and how do we use experimental values?
- What are the limitations of these rate coefficients?

Correlate Mass Transfer Coefficients

JAMES O. OSBURN, State University of Iowa, Iowa City, Ia.*

IN PREVIOUS articles, we have reviewed methods of making mass transfer calculations. Now suppose that we're ready to do a design calculation for an absorber. The next question is: What shall we use for our rate coefficients?

This article covers mass transfer coefficients and transfer units; the next of three covers stage efficiency and in the third, we'll show how the analogy between heat transfer and mass transfer is used in predicting mass transfer rates.

Experimentation Is Still the Rule

The size of mass transfer coefficients depends on three basic factors:

- Kind of equipment used and its design.
- Flow rates of the two phases.
- Physical properties of the fluids.

There have been many articles published which contain data and correlations of mass transfer coefficients. As enough information becomes available, some day we may be able to calculate the coefficient for any desired combination of the three factors. However, we haven't reached this state yet. Where a lot depends on our answer, some experimental measurements must still be made.

At best, we must have some data on the performance of the kind of equipment we are going to use. With caution, we may be justified in extrapolating to other flow rates and to fluids other than those used in the experiments. If we may do this, we may be able to get enough information from the literature to proceed with the design.

However, there are a number of factors which may cause errors if we try to avoid actual measurements.

If we calculate a rate coefficient and use it for design, there are two basic factors which may cause our design to fail.

- Deviations due to equipment.
- Deviations due to substances being treated.

When there are complicating factors due to either of these causes, we may expect that the actual coefficients

obtained will be quite different from those we calculate from correlations.

What Factors To Watch in Equipment

In an experimental program for measuring mass transfer coefficients in packed towers, special precautions are taken to make sure that the packing is wet and that there is no channeling. This may not be done in full-scale equipment. Even in experimental equipment, the coefficients depend on the roughness of the tower wall because of the tendency for liquid to flow along the wall rather than over the packing.

There are end effects which are often neglected. This can lead to serious error, especially in spray columns where most of the mass transfer takes place immediately after the drops of dispersed fluid are formed.

Packing which is supposedly the same as the standard may give different coefficients because of differences in arrangement. In some installations, packing is stacked in a regular arrangement; while in others it is dumped in a random fashion. The rate of transfer will be different, depending on the manner of dumping, whether the tower is empty or full of liquid or whether shaking is used.

Change in System Causes Unexpected Effects

Correlations of mass transfer coefficients depend on the effect of the gross properties of the substances involved. In many cases the coefficient changes in a simple manner for changes in the diffusivity, viscosity and density. Sometimes, however, there are effects which are not anticipated. These are caused by an almost undetectable change in the physical properties of the fluid. Often, these effects make a very great change in the rate of mass transfer.

Some examples of these changes in physical properties are well-known, others are just coming to light. The attempt to absorb sulfur trioxide in water fails because of the reaction between the sulfur trioxide and the vapor above the liquid water. The resulting fine fog of sulfur trioxide is not easily condensed.

* To meet your author see *Chem. Eng.*, Mar. 24, 1958, p. 169.

The rate of absorption of SiF_4 is slower than would be expected because a film of solid silica forms in the liquid and inhibits further absorption. [Whyness, *Trans. Inst. Chem. Engr.*, 34, 12-17, London (1956)].

The inhibiting effect of surface-active molecules in absorption, extraction and evaporation is well recognized. In extraction, the presence of as little as 0.001 mole per liter of a wetting agent reduces the rate of extraction by a factor of ten. In Fig. 1, we show a typical case [Garner and Skelland, *Ind. Eng. Chem.*, 48, 51 (1956)].

The presence of impurities in ordinary water and impurities dissolved from plastic tubing has been found to change both the equilibrium and the rate of extraction for some systems. Certain substances such as alcohols destroy this inhibiting effect.

We may conclude that it sometimes isn't good enough to measure rate coefficients experimentally unless the materials we use have the same impurities that will be found in full scale operation.

After the warning of putting too much confidence in correlating transfer coefficients, we can now show that correlations of mass transfer coefficients do have some value. They can be used to calculate a coefficient for preliminary design. Also, they can serve as a guide and a comparison when measuring coefficients experimentally.

Therefore, let's explore some of the data on mass transfer coefficients to point out unifying features.

Films and Area Control Rates

For design, over-all coefficients $K_g a$ or over-all height of transfer units H_{eq} are most useful. If we neglect a resistance at the interface, we find that these qualities depend on three independent factors: the resistance of the two fluid films and the interfacial area per unit volume.

We have to predict the effect on each of these factors. Then combine them into an over-all coefficient by an equation such as the following which applies to gas absorption.

$$\frac{1}{K_g a} = \frac{1}{k_g a} + \frac{H}{k_l a} \quad (1)$$

In terms of transfer units, Eq. (1) becomes:

$$H_{eq} = H_g + mGH_l/L \quad (2)$$

Film resistances depend on the diffusive properties of the solute in the phases which are present and on factors such as turbulence which reduce the film thickness. In the remainder of this article, we'll examine how the film coefficients and interfacial area vary with conditions in some types of mass transfer equipment.

When To Use Wetted-Wall Columns

Although not of industrial importance, the wetted-wall column is a favorite experimental device because the interfacial area is measurable. For mass transfer from a liquid to a gas, the effect of the liquid film

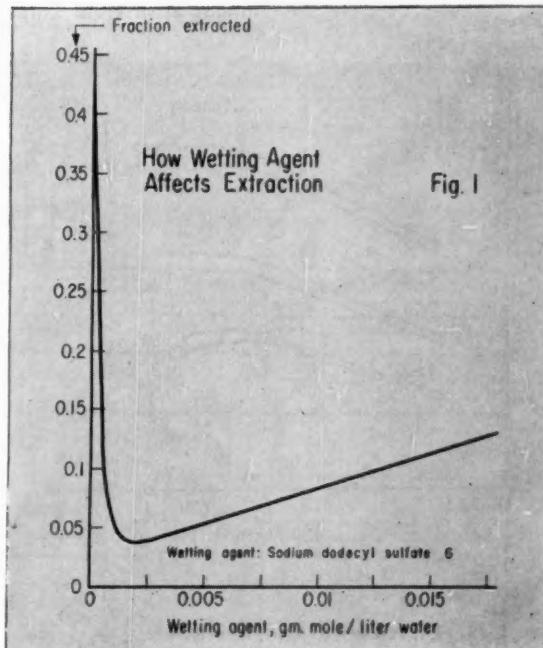


Fig. 1

coefficient is eliminated by using pure liquids and measuring the vaporization rates.

For turbulent flow, the gas-film coefficient for wetted-wall towers can be correlated by Eq. (3) [T. K. Sherwood and R. L. Pigford, "Absorption and Extraction," 2nd. Ed., p. 77, McGraw-Hill Book Co. (1952)].

$$k_g = 0.023 R e^{0.83} \left(\frac{\mu}{\rho D_e} \right)^{0.44} \left(\frac{P}{p_{bm}} \right) \left(\frac{D_e}{dRT} \right) \quad (3)$$

From Eq. (3), we may conclude that the gas-film coefficient varies with the 0.83 power of the gas velocity G ; inversely as the 0.17 power of the tube diameter d ; directly as the 0.56 power of the diffusion coefficient D_e at constant temperatures; directly with the 0.44 power of the pressure because of its effect on the density ρ . The ratio P/p_{bm} will not change very much as the pressure changes.

The effect of temperature is obscured by its effect on the diffusion coefficient and density. Diffusion coefficient D_e varies with the 1.5 power of the temperature. Hence, the over-all effect is that k_g varies directly with the 0.28 power of the temperature at constant mass velocity.

Consider Packed Column Behavior

Gas-film coefficients in packed columns act much the same as in wetted-wall towers, except for the effects of the packing and the liquid flow over it.

We show typical plots of H_g vs. gas rate for the absorption of ammonia in water in Figs. 2 and 3. [Sherwood and Pigford, previous reference, p. 282]. Typical values for a variety of packings are also available in J. H. Perry, "Chemical Engineers' Handbook," 3rd Ed., McGraw-Hill Book Co. New York (1950) and Max Leva, "Tower Packings and Packed Tower Design," U. S. Stoneware Co., Akron (1950).

Slope of the curve at low velocities is different for different water rates but is in the neighborhood of 0.3

How Transfer Unit Height Changes With Fluid Rates

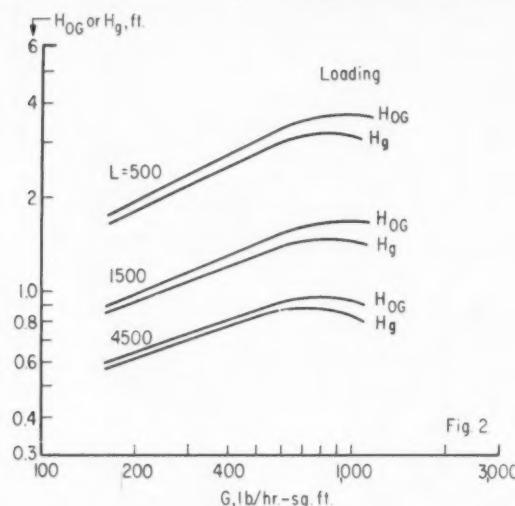


Fig. 2

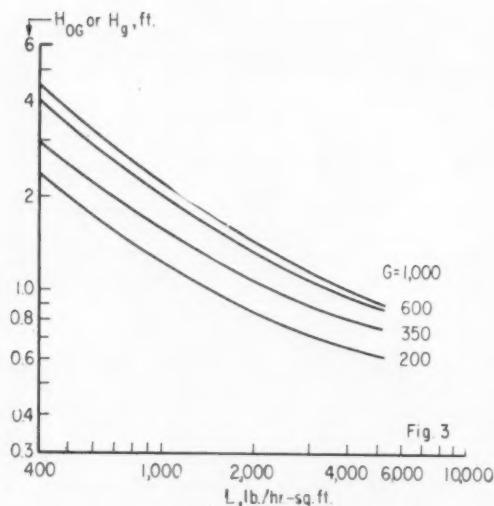


Fig. 3

Extraction Coefficient Stable Over Flow Range

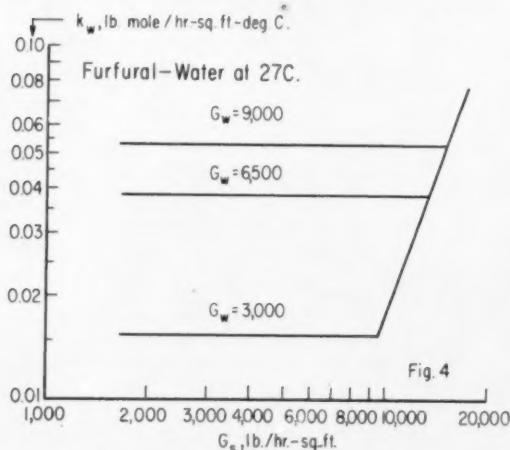


Fig. 4

to 0.5. Since $H_s = G_m / (k_s a)$ (P), the $k_s a$ corresponding to these data vary only with the 0.7 to 0.5 power of the gas velocity; compared to 0.8 power for the wetted-wall towers. Near the loading point, the height of a transfer unit falls but operation may be unstable.

Other factors which affect H_s are:

- Liquid rate, H_s varies as $L^{-0.5}$
- Different gases, H_s varies as $(\mu/\rho D_s)^{0.5}$
- Different sizes of packing, H_s varies inversely as the surface area of the packing per unit volume.

How To Use the Correlations

These correlations are approximate. Also, there is not complete agreement between different investigators. However, if we keep this in mind we can do a fair job of estimating how a coefficient varies for moderate changes in conditions or for different substances. If we combine the information given above, we get this equation:

$$H_s = \frac{CG^{0.4}}{A^{0.5}L^{0.5}} \left(\frac{\mu}{\rho D_s} \right)^{0.5} \quad (4)$$

The constant C depends on the packing. Use of this correlation is shown by the following examples.

Example 1—For the absorption of ammonia from air into water, $H_s = 1.3$ for $G = 500$ lb./sq.ft.-hr. and $L = 1,500$ lb./sq.ft.-hr. Calculate H_s for operation at $G = 1,000$ and $L = 500$.

$$H_s = 1.3 \left(\frac{1,000}{500} \right)^{0.4} \left(\frac{1,500}{500} \right)^{0.5} = 2.4$$

Experimental value for $H_s = 2.8$

Example 2—From the data of Example 1, calculate H_s for the absorption of oxygen from air into water when $G = 500$ and $L = 1,500$.

For ammonia, $\mu/\rho D = 0.61$ and for oxygen, $\mu/\rho D = 0.74$. Hence, $H_s = 1.3(0.74/0.61)^{0.5} = 1.4$. Most of the resistance in oxygen absorption is in the liquid film. This calculated value of H_s is satisfactory for correcting over-all values to find H .

Example 3—The data in Example 1 are for 1½-in. Raschig rings. Calculate H_s for ½-in. Raschig rings.

For 1½-in. rings, area per cu. ft. = 36 sq. ft. and for ½-in. rings, area per cu. ft. = 114 sq. ft. Hence, $H_s = 1.3(36/114)^{0.5} = 0.73$. Experimental value is 0.80.

For Liquid Film in Packed Columns

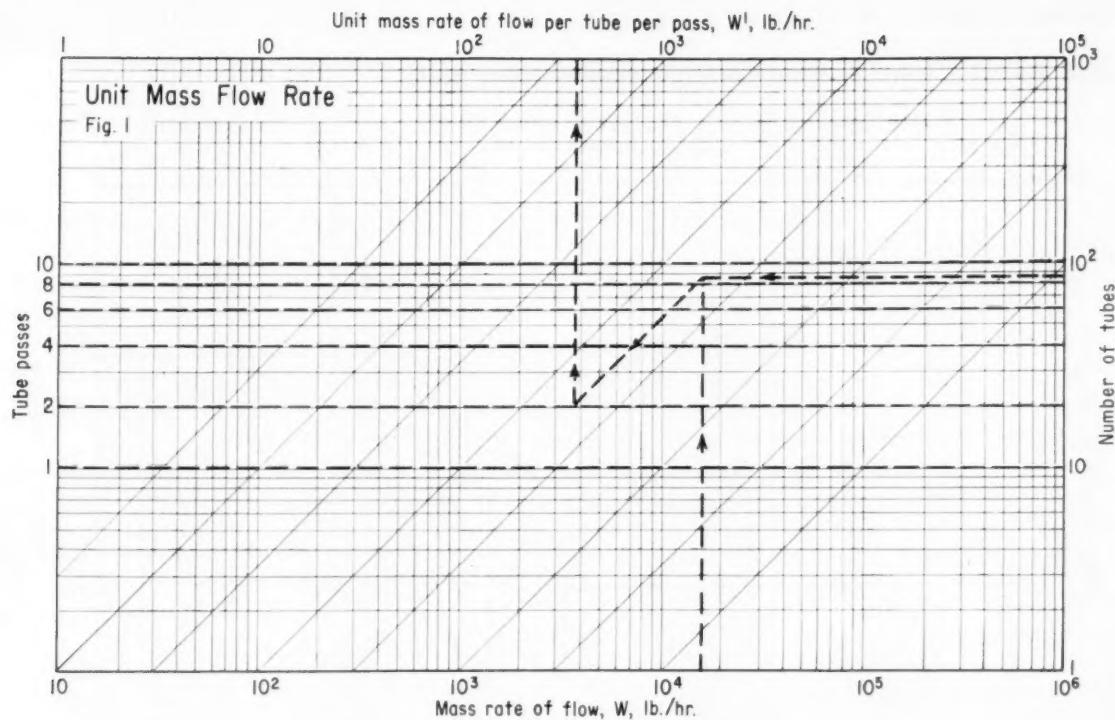
Leva (previous reference) gives this equation for liquid films in absorption:

$$H_l = \frac{1}{a'} \left(\frac{L}{\mu'} \right)^n \left(\frac{\mu'}{\rho' D'} \right)^{-0.5} \quad (5)$$

Here, D' , μ' and ρ' are liquid diffusion coefficient, viscosity and density respectively. The values of a' and n depend on the type of packing used. Values for several types of packing are given by Leva and others can be calculated from experimental data.

Recent experiments [Murphy, Lastovica and Skrzec, *AICHE Journal*, 2, 451 (1956)] with a horizontal extraction column, where the area can be measured, show that the water-film extraction coefficient k_s is a function of G_w , $\sigma^{0.07}$, $\rho^{1.46}$, $\mu_w^{-1.0}$ and $D_s^{1.8}$. It is independent of G_s up to a point; then increases rapidly as shown in Fig. 4.

Many more data must be collected and correlated before we can predict the effect of different systems on the extraction rates.



Speed Heat Exchanger Computations

Use these new charts to find tubeside heat transfer coefficients and pressure drops in the tubes only when streamline flow occurs.

NING HSING CHEN, Heat Transfer Div., M. W. Kellogg, Jersey City, N. J.*

By using these new charts, we can rapidly evaluate tubeside heat transfer coefficients and pressure drops through the tubes of tubular heat exchangers during streamline flow. For methods showing the corresponding quantities for turbulent flow, see *Chem. Eng.*, June 30, 1958, p. 110 and Sept. 22, 1958, p. 160.

Find Tubeside Heat Transfer Coefficient

Find the heat transfer coefficient on the tubeside for a fluid flowing through a 1-2 exchanger at a rate of 16,000 lb./hr. The fluid is heated in two passes from 95 to 145 F. inside 86 tubes each 1-in. O.D. \times 14 BWG and 12 ft. long. At the average temperature of 110 F., the fluid shows the following properties: viscosity Z is 4.8 centipoises, thermal conductivity K is 0.0775 Btu./hr.-sq.ft.-deg.F./ft. and specific heat C is 0.485 Btu./hr.-deg. F.

Step 1—First, obtain from Fig. 1 the unit mass rate of flow per pass per tube. Erect a line perpendicularly through W' of the 16,000 lb./hr. to meet the line drawn horizontally from 86 which is the number of tubes. Through this intersection draw a line at 45° to meet

the number of tube passes line of 2. Through the last intersection draw a line perpendicularly to the rate of flow per tube per pass. Read the value of W' as 370.

Step 2—Check the Reynolds number from Fig. 2 to determine if streamline flow occurs. Reynolds number must be less than 2,100. Erect a line perpendicularly through W' of 370 to meet the line drawn horizontally from inside tube diameter of 0.834 in.

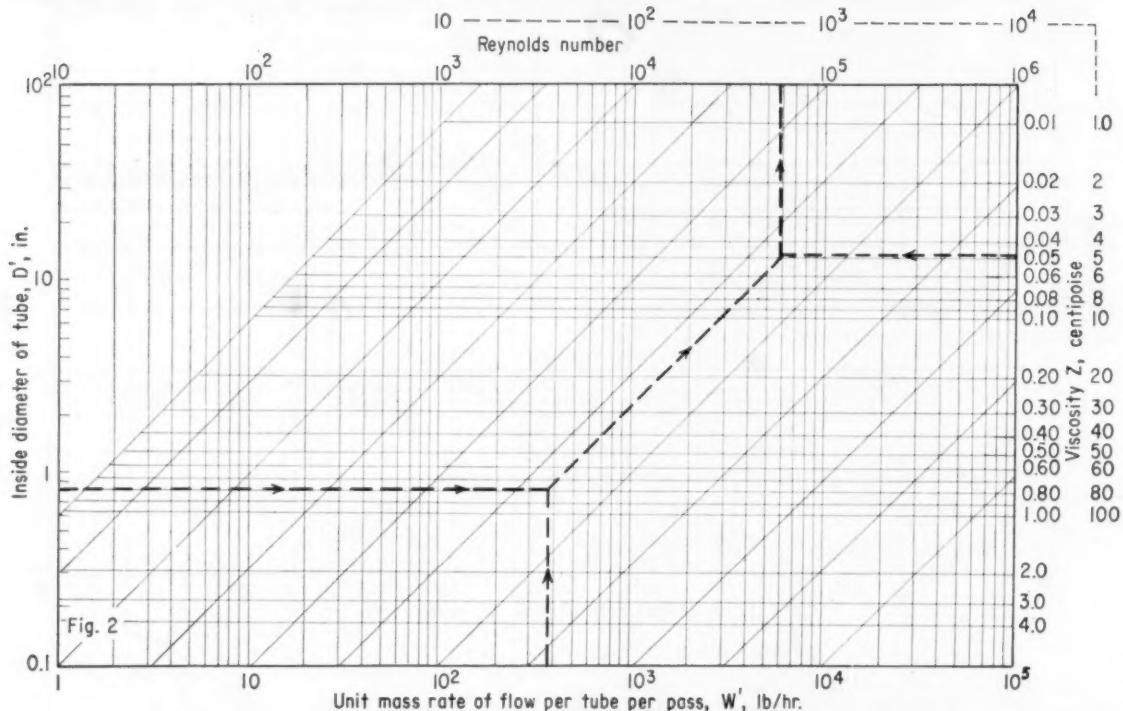
Through this intersection, draw a line at 45° to meet the line drawn horizontally from viscosity Z of 4.8. Then through the last intersection, draw a line vertically to the Reynolds number which is 590. Note that viscosity-Reynolds number coordinates must correspond.

Step 3—Finally, find the heat transfer coefficient from Fig. 3. Erect a line through W' of 370 to meet the specific heat line C equal to 0.485. Then move horizontally to meet thermal conductivity line K equal to 0.0775.

The abscissa of this point found at the top of the chart is the heat transfer coefficient h corrected for viscosity and is equal to 16.0. Correct this value for tube length and for tube size. Correction factor for 12-ft. tube length is 1.10 and for tube size is 0.744.

* To meet your author, see *Chem. Eng.*, June 30, 1958, p. 140.

Find Reynolds Number From Corresponding Viscosity Scale



Hence, corrected heat transfer coefficient $h = 16.0 \times 1.10 \times 0.744 = 13.1 \text{ Btu./hr.-sq.ft.-deg. F.}$

Here are the equations used for correlating the variables and constructing the charts. The Sieder and Tate equation⁶ for streamline flow is:

$$\frac{hD}{k} = 1.86 \left[\left(\frac{DG}{\mu} \right) \left(\frac{C\mu}{k} \right) \left(\frac{D}{L} \right) \right]^{1/3} \left(\frac{\mu}{\mu_w} \right)^{0.14} \quad (1)$$

However, before we can use Eq. (1) to find heat

transfer coefficients, we must first determine whether streamline flow takes place in the tubes. Hence, we convert the usual form of Reynolds number DG/μ into the following form:

$$Re = 6.31 W'/D'Z \quad (2)$$

From Eq. (2) we construct Fig. 2 which enables us to read Reynolds number directly. In Eq. (2), W' is the mass rate of flow per pass per tube in lb./hr. and is correlated to the mass rate of flow in lb./hr., the number of passes and the number of tubes as:

$$W' = WP/N_T \quad (3)$$

We use Eq. (3) to construct Fig. 1 from which we obtain the value of W' directly.

In common engineering units, we can express Eq. (1) as:

$$\left(\frac{Z}{Z_w} \right)^{-0.14} = 24.2 \left(\frac{1}{D'} \right) \left(\frac{W'}{L} \right)^{1/3} C^{1/3} k^{2/3} \quad (4)$$

To construct Fig. 3, we use Eq. (4).

How To Find Pressure Drop

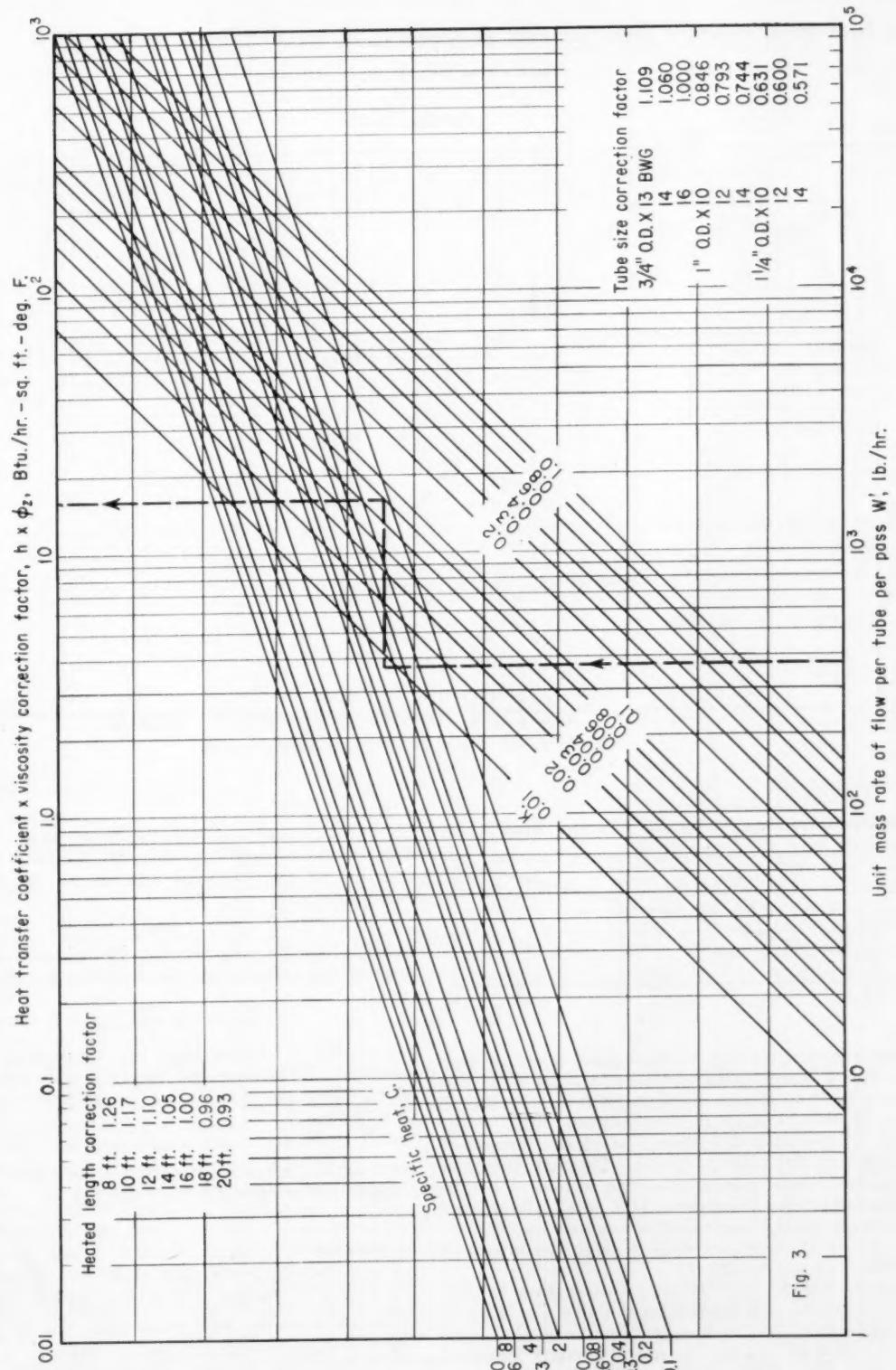
Find the pressure drop through the tubes for a fluid flowing through a 1-2 exchanger at a rate of 16,000 lb./hr. Fluid is heated in two passes inside 86 tubes each 1-in. O.D. \times 14 BWG and 12 ft. long. Properties of the fluid at the average temperature are: viscosity $Z = 100$ centipoises and specific gravity is 0.8. Viscosity at the wall temperature is 50 centipoises.

Step 1—Find the unit mass rate of flow from Fig. 1. Here, W' equals 370 lb./hr. per tube per pass.

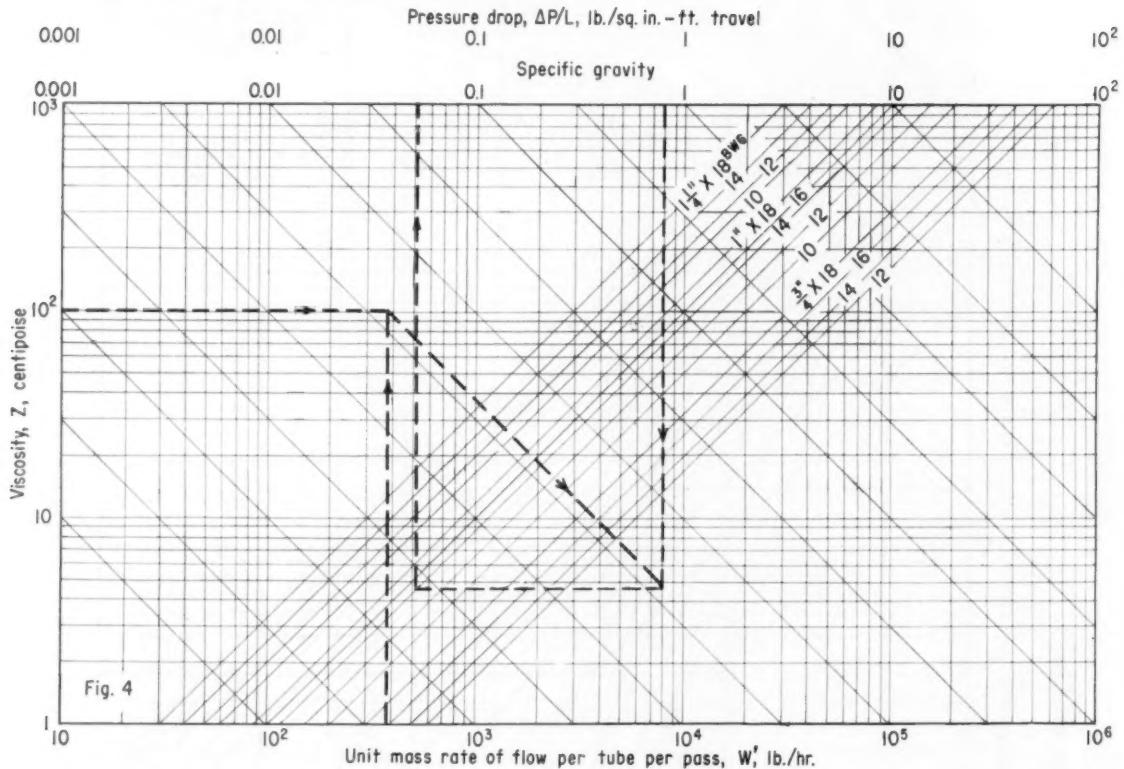
Nomenclature

C	Specific heat, Btu./lb.-deg. F.
D	Inside tube diameter, ft.
D'	Inside tube diameter, in.
f	Friction factor.
g	Gravitational constant, 32.2 ft./sec. ²
G	Mass velocity inside tube, lb./hr.-sq.ft.
G'	Mass velocity inside tube, lb./sec.-sq.ft.
h	Heat transfer coefficient, Btu./hr.-sq.ft.-deg. F.
K	Thermal conductivity, Btu./hr.-sq.ft.-deg. F-ft.
L	Tube length or length of travel, ft.
N_T	Number of tubes.
P	Number of tube passes.
S.G.	Specific gravity.
W	Mass rate of flow, lb./hr.
W'	Unit mass rate of flow per tube per pass, lb./hr.
Z	Viscosity at average fluid temperature, centipoise.
Z_w	Viscosity at tube wall temperature, centipoise.
ΔP	Pressure drop, lb./sq.ft.
ΔP'	Pressure drop, psi.
μ	Viscosity at average fluid temperature, lb./hr.-ft.
μ_w	Viscosity at tube wall temperature, lb./hr.-ft.
ρ	Density, lb./cu. ft.

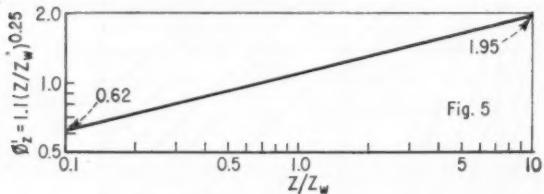
Read Heat Transfer Coefficient From Scale at Top of Chart



Find Isothermal Pressure Drop per Foot of Travel



Viscosity Correction Factor for Pressure Drop



Step 2—Next, we find the isothermal pressure drop from Fig. 4. Erect a line vertically through $W' = 370$ to meet the line drawn horizontally from viscosity Z which is 100. Through this intersection, draw a line at 45° to meet the line drawn vertically downward through specific gravity of 0.8. Through this last intersection, draw a horizontal line to meet the tube size line which for this case is 1-in. \times 14 BWG. Read the abscissa of this point on the top scale as $\Delta P/L = 0.052$. Then the pressure drop through the tube only is $0.052 \times 12 \times 2 = 1.25$ psi.

Step 3—Finally, find actual pressure drop by correcting for tube wall temperature. Using Fig. 5 $\phi_s = 1.32$ when $Z/Z_w = 100/50 = 2$. Therefore, the actual $\Delta P' = 1.25/1.32 = 0.95$. If we use a safety factor of 1.25, then $\Delta P' = 0.95 \times 1.25 = 1.20$ psi.

To calculate the pressure drop, we can use the Fanning equation, which is

$$\Delta P = 2fL(G')^2/gD \quad (5)$$

For streamline flow, the friction factor is a linear function of the Reynolds number as the following equation shows.

$$f = 16\mu/DG \quad (6)$$

Substituting Eq. (6) into Eq. (5) and converting to engineering units, we get the following equation:

$$\frac{\Delta P'}{L} = \frac{5.46ZW'}{10^7(D')^4(S.G.)} \quad (7)$$

We use Eq. (7) to construct Fig. 4 assuming isothermal flow. To account for the tube wall temperature effect, divide the result $\Delta P/L$ by the following correction factor:

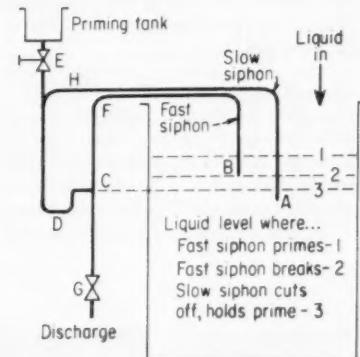
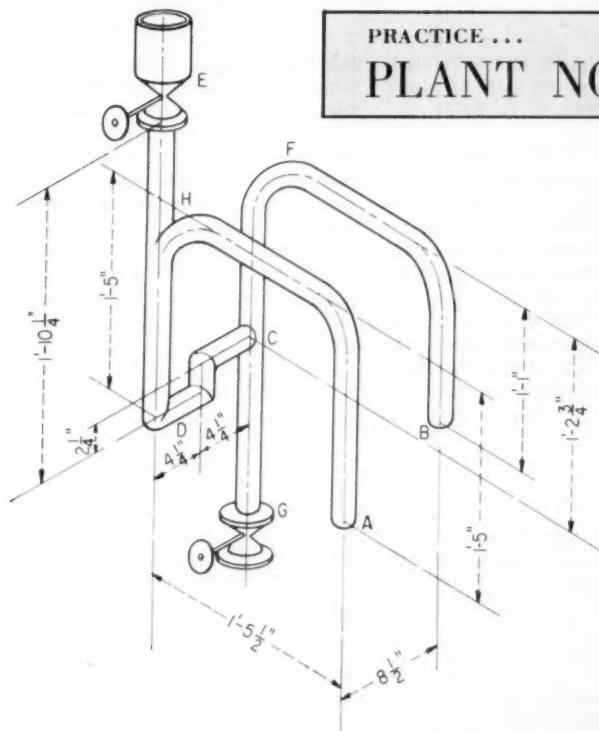
$$\phi_{Z'} = 1.1(Z/Z_w)^{0.25} \quad (8)$$

Here ϕ_x' is the viscosity correction factor for streamline pressure drop and is shown in Fig. 5.

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PRACTICE . . .
PLANT NOTEBOOK EDITED BY T. R. OLIVE



Always-ready siphon makes a convenient way of controlling tank level in cases where under-liquid connections are difficult or impossible to make.

Tank Siphon Never Loses Prime

★ Winner of the July Contest by

C. F. A. Roberts

Superintendent, Plant Investigations Dept., Orr's Zinc White Ltd.
 Imperial Smelting Corp. Ltd., Widnes, Lancs., England.

It is often necessary in chemical plant operations to have a means of maintaining liquid level in a tank between working limits. This usually presents no problem when new equipment is being installed, but may involve a difficult situation in modifying existing equipment, especially if glass- or rubber-lined.

The sketch at the left shows an ever-primed siphon which is easy to construct and suitable for existing tanks. The righthand sketch shows how the siphon rests on the tank and also shows the approximate levels between which it works.

After the tank has been filled the siphon is primed by filling through valve *E*, with valve *G* closed. Closing valve *E* and opening valve *G* then starts the siphon, as long as the tank level is above *B* (Level 2). Priming is easier if the siphon ends are plugged during filling. When the level drops to *B* the fast siphon *BFC* breaks and empties.

For a short time, or until the level drops to *C* (Level 3), the slow siphon will continue a slow discharge through *AHDC*. When the level reaches *C* (Level 3), the slow siphon

will cut off, but will hold its prime due to the liquid seal at *D*.

When further liquid is added to the tank and the level rises above Level 3, slow flow will resume through the slow siphon, the rate of flow increasing as the level continues to rise. At Level 1, a short way above *B*, the flow will have increased enough so that the liquid

NEXT ISSUE: Breather Vents HCl From Solvent Tanks

By C. W. Hamilton, Winner of the August Contest

★ How Readers Can Win

\$50 Prize for a Good Idea—Until further notice the Editors of *Chemical Engineering* will award \$50 each four weeks to the author of the best short article received during that period and accepted for Plant or Design Notebook.

Each period's winner will be announced in the second following issue and published in the third or fourth following issue.

\$100 Annual Prize—At the end of each year the period winners will be rejudged and the year's best awarded an additional \$100 prize.

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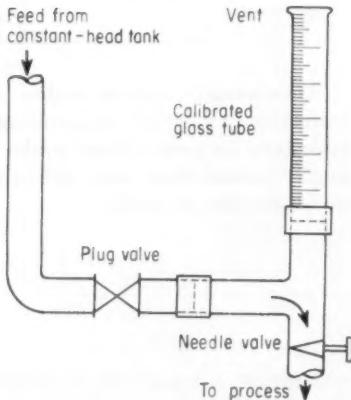
Articles should interest chemical engineers in development, design or production. They may deal with useful methods, data, calculations. Address Plant & Design Notebooks, *Chemical Engineering*, 330 W. 42nd St., New York 36, N. Y.

discharging at *C* into the riser *FG* will act like a laboratory water aspirator and will create enough vacuum to prime the fast siphon *AFC* rather suddenly. At this point the entire section *BFCG* will be full and rapid siphoning will resume. The cycle of operations thus starts all over again.

The dimensions shown have worked satisfactorily in practice, though considerable latitude is possible. However, I do not recommend a larger tubing diameter than 2 in., while dimension *EH* should be as short as possible. The lower that end *B* is, the sharper will be the cut-off

action of the siphon, but the siphon will not work at all if *B* is lower than *D*.

(Editor's Note—Dr. Roberts sent a small glass model of the siphon with his manuscript. With the aid of some of his wife's cooking utensils and the kitchen sink, the editor gave the siphon a thorough work-out. It really works as stated. Watching the fast siphon suddenly pick up its prime as the level rises carried the editor back to one phase of his youth when he went in heavily for the black arts and legerdemain.)



Meter Without Orifice Handles Small Flows

C. M. Fair

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Description of a simple flow meter using an orifice plate and glass standpipe for visual determination of the head (Bierbower, *CE*, Feb. 10, 1958, p. 152) recalls a similar device we once used, but without the orifice plate. In our case the restriction was a needle valve.

Our meter also took flow from a constant-head tank but varied the flow with the needle valve. We calibrated it by closing the plug valve and then, with a stopwatch, determined the volume per unit of time by drop in level in the glass tube.

The meter was simple and accurate, yet flexible owing to the possibility of instantaneous flow rate variation with the needle valve.

One limitation lay in the fact that variation of level in the glass tube during measurement had to be small in comparison with the total head of the feed system.

The meter was also useful in measuring pumped feed flows to a process by connecting it into the suction side of the injecting pump. Here, the limitation described would not apply.

One great virtue of the meter as we operated it is that the fluid dynamics factors of specific gravity, viscosity, Reynolds number, temperature, etc., can be neglected. In calibrating it as described it is easy to make up a table to convert sec./unit volume to any desired flow units such as gpm. or lb./gal. or other units.

Teflon Caulking Prevents Leaks in Threaded Joints

Robert A. Snedeker

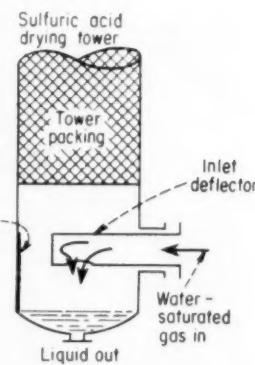
Photo Products Dept. E. I. du Pont de Nemours & Co., Parlin, N. J.

In medium pressure service screwed fittings often leak, even when the threads appear perfect and the joint is carefully made. The same thing happens even more frequently when stainless steel pipe and fittings are used. Sweating the joints with silver solder is effective in most cases, although to hold mercury or corrosive chemicals requires something other than silver solder.

An easy way to make an inert threaded joint is to caulk it with a thread of Teflon polytetrafluoro-

ethylene plastic. The thread is simply wrapped around the female member and the joint assembled.

Such a joint will hold mercury, for example, at 1,500 psig. at room temperature. Small quantities of thread can be made by turning down a Teflon rod on a lathe and collecting the thread. The proper speed and depth of cut of the lathe, and the amount of thread needed for each joint, are easily discovered by trial and error.



Inlet Deflector Reduces Weak Acid Corrosion

Jerome A. Seiner*

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When using sulfuric acid to dry gases, both the temperature and the concentration affect the rate of corrosive attack on the tower wall. In normal operation of such a drying tower the momentum of the entering gases carries across from the inlet nozzle to the liquid film running down the opposite side. Hence, a disproportionate part of the moisture is taken out in this film.

The result is that there is a greater increase in temperature due to dilution and a greater decrease in concentration in the film than in the bulk of the acid, with accelerated corrosion in a relatively small area of the tower wall. A simple solution is to install an inlet deflector as in the sketch. This deflects the moisture-laden gas toward the large acid pool in the bottom where the effects of dilution are dissipated.

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Use Specific Gravity Like Molarity

C. L. Murray

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Idaho

It is a little appreciated fact that specific gravities can be used like molarities in concentration calculations on solutions. Hence, many solutions can be made in the plant by the use of a simple hydrometer, without need for a laboratory analysis. But first, let's review the use of molarity.

The familiar expression $(M_1)(V_1) = (M_2)(V_2)$ is fine if you want to dilute a given solution to something weaker. However, it is of no help if the problem is to increase the strength of the solution. The general expression:

$$(M_1)(V_1) + (M_2)(V_2) = (V_1 + V_2)(M_3) \quad (1)$$

can be used either to increase or decrease the molarity of a given solution by adding a stronger or weaker stock solution. Here M_1 and V_1 refer to the molarity and volume of the present solution; M_2 and V_2 refer to the molarity and volume of the correcting solution; and M_3 refers to the desired molarity. In using the equation all factors except V_2 will be known and the equation can therefore be solved for that value.

For example, we have 1,000 liters of a solution having a molarity of 1.20 M in a given component. The desired solution is 1.25 M. The correcting solution has a molarity of 13.0 M. Then, using Eq. (1):

$$(1,000)(1.20) + (V_2)(13.0) = (1,000 + V_2)(1.25)$$

and $V_2 = 4.26$ liters

Of course, if the strength of the correcting solution is much greater than the desired molarity, then the volume of correcting solution will be small compared to the main solution. If the two molarities are quite close together, then volume V_2 becomes appreciable.

In training chemical operators I always urge them to use the full formula, Eq. (1), in spite of any extra work involved, since it fits all situations and always gives the correct result.

When it comes to using specific gravity rather than molarity, we must subtract 1.000, the specific gravity of water, from all specific

gravities before calculation. So, using the symbol sp. gr.^* to mean $(\text{sp. gr.} - 1)$ we have:

$$(V_1)(\text{sp. gr.}_1^*) + (V_2)(\text{sp. gr.}_2^*) = (V_1 + V_2)(\text{sp. gr.}_3^*) \quad (2)$$

which is used exactly like Eq. (1).

Additions of stock solutions of known specific gravity, or of water, to single component solutions are easy with Eq. (2). In a multicomponent solution, one must resort to a molarity analysis of each component and then calculate the necessary corrections from Eq. (2).

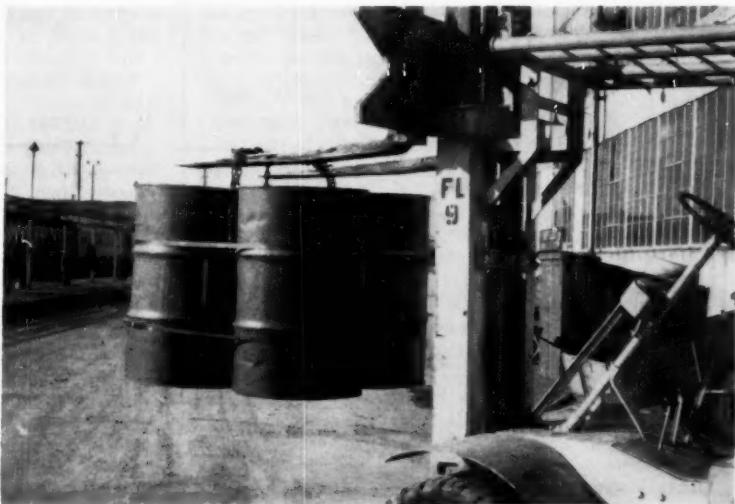
There are several short-cut variations of Eq. (2) which are very handy. For instance, in making a simple dilution the final volume of the solution is merely the ratio of the abbreviated specific gravities:

$$(V_1)(\text{sp. gr.}_1^*/\text{sp. gr.}_2^*) = \text{final volume} \quad (3)$$

And in increasing the specific gravity by evaporation, the reverse ratio holds true:

$$(V_1)(\text{sp. gr.}_2^*/\text{sp. gr.}_1^*) = \text{final volume} \quad (4)$$

Eqs. (3) and (4) apply equally well to either single- or multicomponent solutions.



Handling Drums Without Pallets

Western Pacific Railroad Co., San Francisco, has developed a money-saving method of handling 55-gal. drums without pallets, thus saving on pallet cost and avoiding the problem of pallet return.

As the photograph shows, the drums are steel-strapped together with a small amount of rough lumber dunnage so that four can be lifted and handled as a unit by means of a standard fork truck or crane.

The four drums are put together and separated into pairs by two pieces of lumber. One is placed between the wedges and the other

between the bottom chine and the bottom swedge. Then the drums are bound with steel straps just above and below the wedges, as the illustration shows.

The upper piece of lumber serves as a lifting beam. A chain sling or a simple hook arrangement secured under the beam and over the truck forks does the trick. An alternate arrangement is to use a piece of I-beam across the top of the forks, with scrap-metal hooks, instead of the chain sling.

Western Pacific has been testing the method on shipments and has found it highly successful.

PRACTICE ...

YOU & YOUR JOB

EDITED BY R. F. FREMED

Electrical engineers, mostly, were the principals in this particular situation. However, this bipartisan report will be interesting reading for every engineer.

The Story of Engineers on Strike

What the Union Asked For

Engineers and Scientists of America
341 Munsey Building
Washington 4, D. C.

July 15, 1958

THE 1,800 professional engineers and scientists employed by the Radio Corporation of America at its Camden, N. J. area operations, who are represented by the Assn. of Professional Engineering Personnel—ESA, struck the RCA plants on Tuesday morning, July 8. The strike is still continuing. All 1,800 engineers and scientists involved in the strike are in the Research and Development Dept. at RCA.

Since the commencement of the strike, there have been a number of meetings between the parties held at the offices of Commissioner John Murray of the Federal Mediation Board. Thus far, however, the only change of position on the part of the parties is that APEP has reduced its salary increase demand from 19.5% to 10.5%. The company has offered a salary increase of 4%.

Other issues in the dispute relate to a merit program and a layoff and recall program.

APEP has asked for a guaranteed merit kitty of 5.7% of the engineering payroll/yr.; the merit kitty to be distributed in accordance with a merit rating program. This program takes into account such factors as: adequacy of technical knowledge; application of technical knowledge; evaluation of technical results; imagination and creativity; ability to meet project objectives; follow-through on assignments; breakdown of difficult assignments into manageable portions; clarity of communication of technical information; etc.

To date, the company has resisted this proposal. The company has offered a counter-proposal whereby it would set up a merit review plan by Nov. 1, 1958. Pilot studies of the plan would be made between Nov. 1958 and Feb. 1959, at which time the plan would be used to determine individual merit increases to be granted after that date. The plan would be established by the company. Its provisions would not be subject to collective bargaining. APEP has rejected the company's counter-proposal.

APEP has proposed that the layoff program, which is now almost completely discretionary on the part of the company, be revised and predicated on a

Information Released by the Company

Radio Corporation of America
30 Rockefeller Plaza
New York 20, N. Y.

July 8, 1958

MEMBERS of the Association of Professional Engineering Personnel, an independent union, today struck RCA facilities at Camden, Cherry Hill and Moorestown, N. J. Picket lines were established at employee entrances of the three locations.

The walkout, involving some 1,500 design and development engineers, began at 6 A.M. while a negotiating session was continuing at the Philadelphia office of Commissioner John Murray of the Federal Mediation and Conciliation Service.

Picketing was peaceful and the 15,000 RCA employees in the Camden area not members of the striking union reported for work this morning with no delay. Several hundred engineers who are members of the striking union also reported to work.

The company has offered a substantial general salary increase plus improvements in insurance and retirement plans and other contract benefits.

An RCA spokesman said that the principal issue discussed today was a proposed revision of the merit increase review program, with the union demanding a guaranteed fund for merit increase expenditures. The company offered a liberalized merit increase program.

The RCA spokesman said considerable progress was made during the all-night negotiations, with the union's demand for a guaranteed merit increase fund the major remaining issue.

Negotiation sessions were recessed at noon after 26 hours with plans for RCA and union representatives to meet again at Commissioner Murray's office tomorrow at 9 A.M.

July 9, 1958

The Association of Professional Engineering Personnel today postponed a meeting with Radio Corporation of America representatives at the Philadelphia office of Commissioner Murray, Federal Mediation and Conciliation Service.

An RCA spokesman said that APEP's postponement of the meeting came two hours before it was scheduled to start. Commissioner Murray later directed that representatives of both APEP and RCA

Union, continued

formula which takes into consideration economic value, career value and merit value of an engineer.

The economic value would recognize that salary is a measure of an engineer's value. The career value would recognize that an engineer's value can also be measured by the relation between his salary and the salaries of other engineers with equal experience. Merit value would recognize that an engineer's value can also be measured by the size of his merit increase.

The plan would also take into consideration education and experience—a certain number of points being given for a B. S.; a higher number of points for an M. S.; and the maximum number of educational points for the Ph. D. Experience would be calculated on the basis of 0.1 points/yr. of tenure. No agreement has been reached on this proposal.

Members of APEP are picketing the RCA plants at Moorestown, Camden and Cherry Hill. They are also picketing the RCA Building in New York. Thus far, picketing has been without incident. Virtually none of the engineers and scientists represented by APEP have crossed the picket lines to go to work, in spite of the fact that RCA management has vigorously been attempting to organize a back-to-work movement.

What the Union Settled For

July 22, 1958

THE Assn. of Professional Engineering Personnel (APEP) reached an agreement with RCA management at 9 P.M. on Saturday, July 19. The agreement was reached in the Philadelphia offices of Federal Mediator John R. Murray.

The settlement in brief is as follows:

New Salary Schedule—An average 6% general increase will be applied to all APEP personnel immediately; applied on a graduated basis. The 42 engineers and scientists now earning less than \$6,000/yr. will receive an increase of 4%. 291 now earning between \$6,000 and \$7,000/yr. will receive 4.6%. An increase of 5.08% for 315 earning \$7,000-\$8,000/yr. An increase of 5.5% for 350 earning \$8,000-\$9,000/yr. An increase of 6% for 282 earning \$9,000-\$10,000/yr.

The 204 engineers and scientists now earning \$10,000-\$11,000/yr. will receive an increase of 6.5%. The 366 engineers and scientists now earning in excess of \$11,000/yr. will receive an increase of 7%. All increases are effective as of July 21, 1958.

With the new increases, the average earnings of engineers and scientists represented by APEP will be approximately \$10,000/yr. The top earnings will be \$18,700/yr., with 15 people in the bargaining unit at the top of the salary range.

Another Increase Jan. 1, 1959—Effective Jan. 1, 1959, a 1% across-the-board increase will be applied to the entire bargaining unit.

Merit Review Plan—APEP and the company will jointly develop a merit review plan to be instituted sometime early in 1959. The agreement stipulates that merit increases in the future are to be determined by the score on the merit review form to be developed as part of this plan. This score system will

Company, continued

be present for a further meeting in his office at 11 A.M. tomorrow.

All RCA employees not members of the striking union again were on the job today, although picketing continued at the RCA plants in Camden, Cherry Hill and Moorestown, N. J. An apparent back-to-work movement developed with some sections reporting as high as 50% engineering personnel attendance.

Meanwhile, the principal unsettled issue remains a merit increase plan, the RCA spokesman said. He said the union continues to demand a guaranteed merit increase fund.

The company agreed that it would develop and install a formalized merit increase program and in the interim period individual merit increases granted by the company would not fall below an estimated minimum.

All other prime issues virtually have been settled, the RCA spokesman said, including the matter of a general wage increase. The union has reduced its general salary increase demand from 15% to 6%. RCA originally offered a 4% general raise.

With a 6% general increase the average salary of the employees, reported by the association, would be over \$10,000/yr. with a maximum in the bargaining unit in excess of \$18,500 annually.

July 10, 1958

The Radio Corporation of America today asked the Federal District Court in Camden to rule whether the amount of merit increases to members of APEP is subject to arbitration under the labor agreement between the company and the union.

Before the recent contract negotiation commenced, the union filed a grievance with the company claiming that the merit increases granted by the company last September were not satisfactory. The union is now attempting to take this grievance to arbitration despite the company's position that the amount of such increases is not subject to arbitration under the agreement, although the eligibility of personnel for merit increases is.

When informed of RCA's position the American Arbitration Assn. indicated that under its established rules the union's grievance must go to arbitration unless halted by appropriate court action.

After an Enforced Silence

July 18, 1958

BOOTH RCA and the APEP union are under an unqualified commitment to the federal mediator not to issue statements to the press concerning current negotiations. Nonetheless, for its own reasons APEP has seen fit to violate this agreement repeatedly.

When, in contradiction to the actual facts, we are being blatantly and repeatedly accused of refusing to bargain in good faith, we feel that in all justice we must break our silence at least to the extent of making clear the following facts.

RCA has for many long weeks, extending through marathon sessions into the present, sought to negotiate an equitable settlement with the APEP union.

We have always believed that it was unnecessary for the union to have called out on strike the profes-

Union, continued

also be used to determine retention credit in the event of a layoff. Merit review score of any individual will be subject to the grievance procedure.

The company has agreed that any reduction in the amount of merit increases as a result of economic conditions will not affect members of APEP more adversely than other groups at RCA. It has also agreed to discuss the reasons for reduction in merit increases with APEP before such reductions are instituted.

Layoff and Rehiring—The layoff and rehiring procedure which was agreed to by the parties permits bumping between locations in the Camden area of RCA's works against anyone within the same job classification with less than 1 yr. of service credit.

Within any one location any individual may bump down into a lower classification.

The parties have also agreed to establish an area-wide recall pool. The company has agreed that it will not hire into any given classification for any location within the bargaining unit until this pool is exhausted.

Retention Credits—Retention credits for layoff and rehiring procedures will be based on:

1. Engineering value points computed on the basis of the engineer's salary relative to the salary of other engineers within the same classification with comparable years of experience.

2. Merit review points as determined from the merit review form. The average of the last three merit ratings, or the last one, whichever is the higher, will be used in the determination of retention credit.

3. Points earned by education, length of service and engineering experience.

Medical Benefits—Hospitalization and medical-surgical benefits are improved in the new agreement.

Retirement Plan—Improvements were made in the retirement plan in the agreement.

Insurance Benefits—It was agreed by the parties that all of the insurance benefits which the members of APEP enjoy are to be considered to have been in effect during the strike.

Grievance Procedure Improved—The grievance procedure was improved to provide definite time limitations for each step in the procedure.

Definition of an Engineer—The definition of an engineer is to be expanded in the new contract to include engineers and scientists in the Research and Development Depts. of RCA who have not in the past been represented by APEP by virtue of the fact that they were not engaged in research and developmental work. The unit will now include human engineers (combination engineer-psychologist), certain classes of high-level mathematicians, etc.

Payment for Invention—The parties agreed that any engineer or scientist represented by APEP will be paid the sum of \$50.00 for each invention.

Overtime to Be Optional—The parties have agreed that overtime work shall be optional to the extent that any engineer or scientist can refuse to work overtime when requested to do so by the company without adverse affect on his merit review or promotability.

No Reprisals, Contract Term—The parties agree that there shall be no reprisals against any individual because of activities during the strike. The contract expires on July 1, 1959.

Company, continued

sional engineers, most of whom were engaged in work on critical defense contracts.

We deplore the irresponsible distortion of facts to which the striking engineers and the community have been subjected. For example, in a special note APEP accuses the company in intemperate language of bringing pressure against those union members who have a deferred draft status because of their critical work on defense contracts. The truth is that we have done nothing of the sort. One draft board on its own initiative notified one of the striking engineers that because his status has changed he was being re-classified to 1-A.

When he notified his supervisor of this action, RCA applied to Selective Service for continuation of the deferred status of this man.

As Interpreted by Professional Engineers

National Society of Professional Engineers
2029 K Street, N. W.
Washington 6, D. C.

Aug. 5, 1958

THE recent two-week strike of engineers and scientists employed by RCA in its Camden area operations is further confirmation of NSPE's long-held viewpoint that professionalism and unionism are incompatible, according to a statement issued today by Clark A. Dunn, P. E., president of NSPE.

In response to requests* for NSPE comment upon the strike, Dunn said that wherever unionism has spread to engineers, it has been followed by strikes, picket lines and other usual union tactics.

"It has long been obvious that if engineers want unions they must be prepared to accept the consequences," Dunn said. "It is foolhardy to pretend that the concepts of professionalism can survive or flourish in an atmosphere of collective bargaining. This latest strike is nothing new in proof of our comment. It was, in fact, the sixth strike by an engineers' union in the past five years."

The NSPE spokesman added that the society has urged upon professional engineers a realization that they cannot have their cake and eat it too. He said that the evidence shows that many of the present engineering unions proclaim their devotion to professional concepts, but the recent strike, added to others, plus demonstrations and other union tactics, show that such a claim, even if sincere, is a mirage and a delusion.

"These comments are not intended to indicate any opinion regarding the validity of the matters at issue in the strike or to say which party was at fault. The purpose of these statements is to emphasize the firm belief of NSPE that the only professional method of solving grievances between professional engineer and employer is through the development of effective communication between the engineers and management."

* The above statement by an official representative of NSPE was initiated by a request from *Chem. Eng.* to Milton F. Lynch, Legislative Counsel for the society. The American Institute of Electrical Engineers referred us to Engineers Joint Council for comment. EJC, while declining to comment on this particular situation, referred us to their May 1956 report, "Raising Professional Standards and Improving Employment Conditions for Engineers," which summarizes EJC policy in the general area of employment conditions for engineers.

APPLICATION HINTS:

Ways to simplify construction and cut costs with **Flexpipe**



Flexpipe helps meet tough piping problem in air conditioning an existing building

THE PROBLEM: Air conditioning an existing office building usually calls for a bit of ingenuity in design. One large New York office building decided to air condition by making provision for packaged, water-cooled units to be installed on any floor as tenants required.

This called for four 10-inch risers, running the height of the building, to carry cooling water between the cooling tower and the branch pipes at each floor level. Because of structural conditions, the risers could not be run down through the basements and supported from below. The combined weight of pipes and the water was so great that they could not be anchored at any one point on the structure.

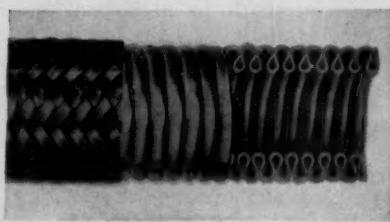
So the consulting engineers, Zimmerman Engineering, New York, floated the risers on spring hangers, distributing the

weight evenly over all floors. This meant, however, that the risers were free to move. A riser full of water weighs several tons more than an empty one and settles about two inches.

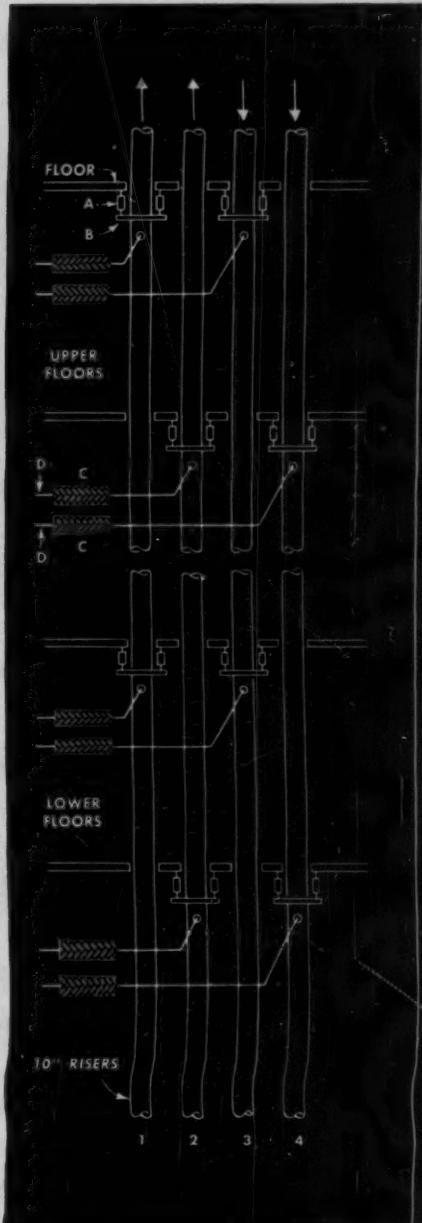
Therefore connections between risers and branch pipes had to be flexible. They also had to have strength, because water pressure at the lower floors approaches 400 psi.

THE SOLUTION: Flexpipe connectors were the answer. They provided the flexibility and the strength required. Furthermore, they were available in the sizes needed—from 5" diameter at the lower floors to 2" at the top floors.

WHERE TO BUY: Flexpipe connectors come in convenient standard sizes and are sold by leading distributors. They can show you samples and answer questions about service applications. For the name and address of the one serving your area, or for more detailed information, write to: The American Brass Company, American Metal Hose Division, Waterbury 20, Conn. In Canada: Anaconda American Brass Limited, New Toronto, Ont. 54220



FLEXPIPE'S flexible core can be either tin bronze, hot dipped galvanized steel or stainless steel. End fittings (attached): flanges, threaded males and welding nipples.



SCHEMATIC DIAGRAM showing how cooling-water risers were installed. A: spring hangers. B: pipe clamps. C: Flexpipes. D: branch pipes at each floor. 1, 2, 3, and 4: risers, 10 inches in diameter. Upper left: Photo of Flexpipe installation at a lower floor.

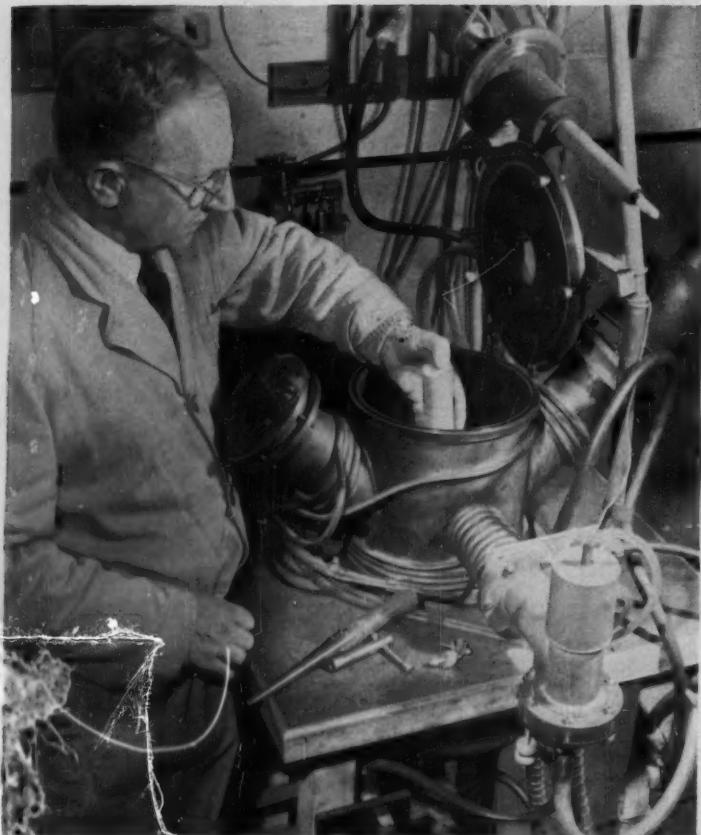
Flexpipe® an **ANACONDA®** product

made by The American Metal Hose Division
of The American Brass Company

PRACTICE . . .

CORROSION FORUM

EDITED BY R. B. NORDEN



New chromium-based alloys, under development, promise to solve many high-temperature problems.

Cr-Based Alloy Breakthrough?

A promising development in high-temperature alloys is shaping up in Australia. Scientists at the Aeronautical Research Labs. and the Defense Standards Labs. in Melbourne are working on new chromium-based alloys which stand up to temperatures of 1,750 F. and higher. In the picture above an operator is removing a chromium alloy from a melting pot.

Most of our present cobalt and nickel superalloys have a top operating limit of 1,500-1,600 F.

Intended for jet aircraft gas-turbine rotor blades, the new alloys will also find many high-temperature chemical applications. It's known that Du Pont has expressed interest in getting an option on the Australian chromium-alloy processes.

► **Chromium Isn't Brittle**—Chromium, with a melting point of about 3,450 F., has already been tried as a basis for high-temperature alloys by research workers in England and the U. S. This work was largely discarded, mainly because chromium was nearly as brittle as glass at room temperature and no way could be found to make it ductile or malleable.

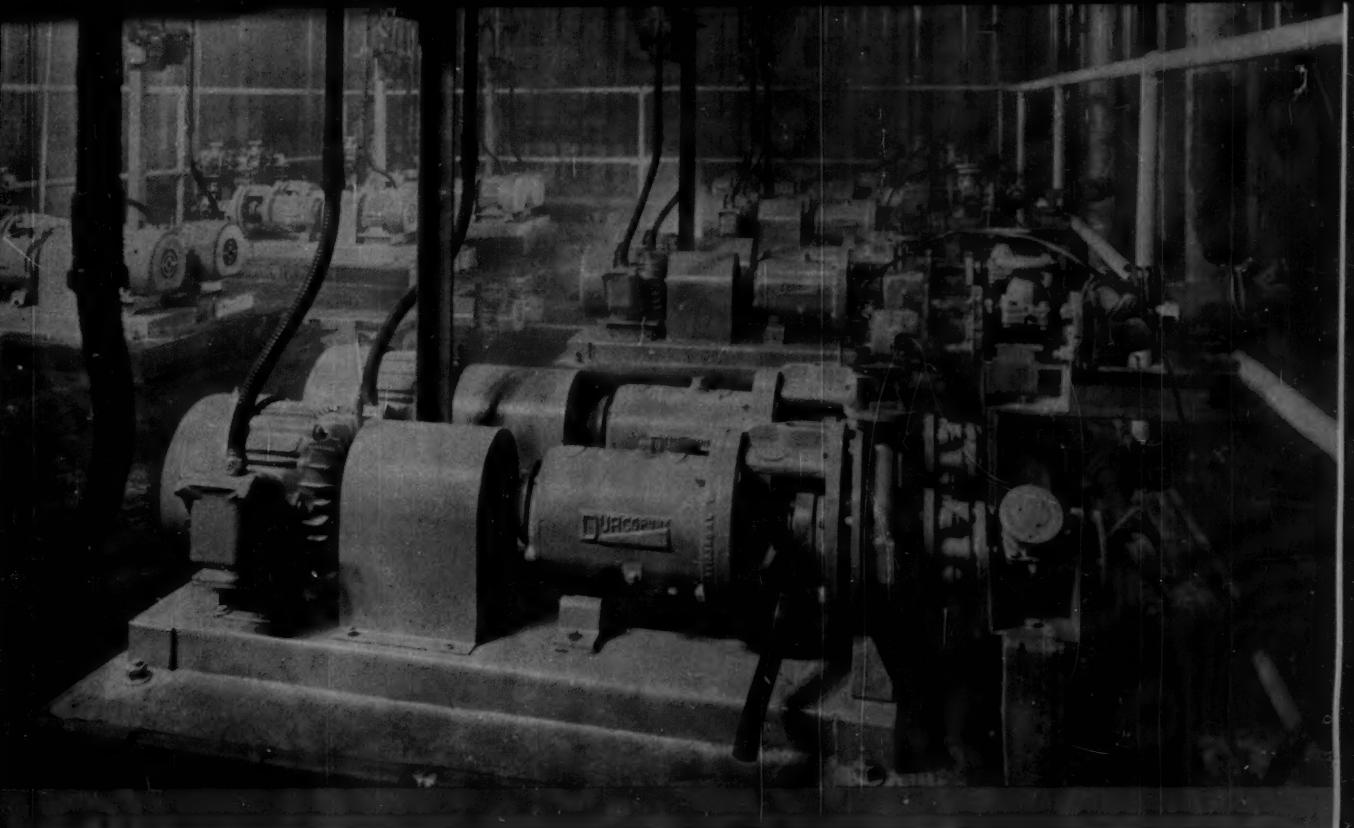
The Australian scientists have proved that chromium is not inherently brittle. They've found more than one way of removing brittleness.

In studying the reasons for brittleness of chromium at temperatures as high as 570 F., the Australians first discovered the metal could be made ductile by mechanical working at temperatures which did not permit it to become fully re-crystallized. Further studies showed pretty clearly that brittleness was largely due to very minute amounts (a few parts per million) of nitrogen in solution. When the metal was treated to precipitate the nitrogen into a suitable distribution, it became quite ductile at room temperatures.

► **Alloy Developments**—Considerable progress has been made on a program designed to find out how alloying additions affect the high-temperature properties of chromium. So far simple alloys have been made with high-temperature strengths better than those for the best of conventional alloys.

The teams say there is "every reason for confidence that further alloying will greatly increase strength in high temperatures and extend the feasible temperature range upward."

► **New Process Techniques**—The program has included design of a semi-automatic plant to produce, by a carefully controlled electrolytic process, chromium of the high purity required for fundamental studies. There is a new furnace design for melting the chromium under



THIS IS A PUMPING STATION AT CARBORUNDUM METALS COMPANY. HERE ARE A FEW OF THE MORE THAN FORTY SERIES H DURCOPUMPS USED IN THE PRODUCTION OF ZIRCONIUM. THESE PUMPS HANDLE $ZrOCl_2$ TWENTY-FOUR HOURS A DAY, SEVEN DAYS A WEEK. THE AIR IN THIS AREA IS CONSTANTLY FILLED WITH CORROSIVE CHEMICAL VAPORS. EVEN WITH THIS HARD USE AND CHEMICAL ABUSE, DURCOPUMPS REQUIRE AN ABSOLUTE MINIMUM OF MAINTENANCE.

Series H Durcopumps are chemical pumps all the way. They are designed and built to give long, trouble-free life when handling tough corrosives. They have a large, rugged shaft with minimum deflection, heavy duty bearings, integral suction and discharge with casing support. Durcopumps are adaptable to

either packing or mechanical seal.

These pumps are available in twelve standard alloys with interchangeable wet end parts. Capacities range from $\frac{1}{2}$ to 3500 gpm, and heads to 345'. When you have a chemicals handling problem, and want long, dependable pump life, call the Durco service engineer.



The mark of dependability in tough chemical service . . . everywhere

THE DURIRON COMPANY, INC. / DAYTON, OHIO

Branch Offices: Baltimore, Boston, Buffalo, Chicago, Cleveland, Dayton, Detroit, Houston, Knoxville, Los Angeles, New York, Pensacola, Philadelphia, and Pittsburgh.

a mixture of argon and helium, in addition to procedures for introducing alloying additions and for working down the ingots to rod, wire and sheet form for testing purposes.

What's Your Rust Index?

Comparative rates at which rust proceeds in different parts of the country, have been established for the first time for all

U. S. cities over 10,000 population.

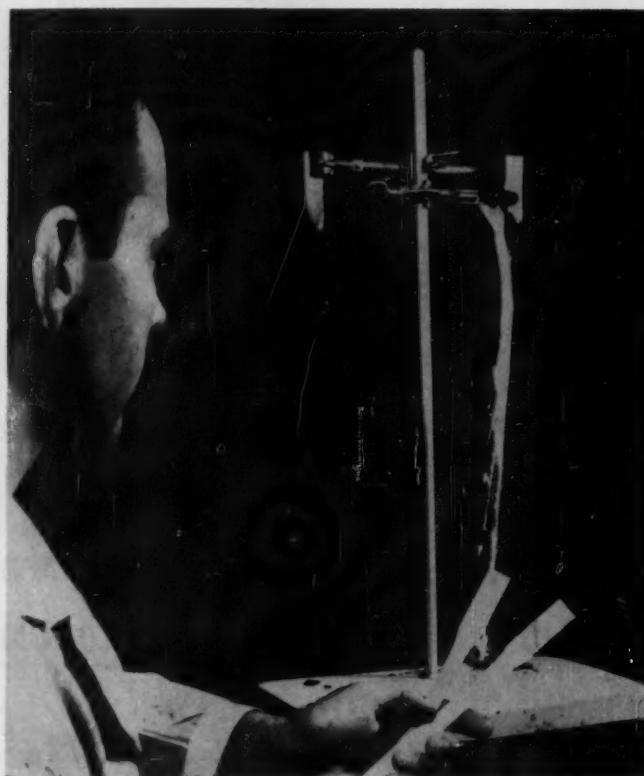
It takes three years, the fastest rate in the country, for rust to corrode a standard, uncoated steel test panel, the size of an auto license plate, in four different cities—Buffalo and Rochester, N. Y.; Erie, Pa.; and Miami, Fla. Slowest rust rate, more than 15 yr., is in Tucson, Ariz.; Roswell and Santa Fe, N. M. In all the nation's major industrial centers the rust rate is under four yr.

This was disclosed in the first Rust Index of the U. S., prepared by the Rust-Oleum Corp., Evanston, Ill. The Index, the result of a 25-year research program, lists the 523 cities of the country with a population of more than 10,000 and the comparative rust rate for each city. Variations in rate result from the different amounts of rainfall, wind, corrosive gases, sunlight, and salt water present in each locality.

The rust rate is three yr., one mo. in Pittsburgh; three yr., two mo. in Los Angeles; three yr., three mo. in Cleveland; three yr., five mo. in Chicago; three yr., six mo. in New York City; three yr., eight mo. in Philadelphia and Detroit; three yr., nine mo. in San Francisco; and three yr., 10 mo. in Boston and St. Louis.

Rust-Oleum Corp., which produces rust-preventing coatings, estimates the nation's rust bill as currently about \$7½ billion per year, an increase of \$2 billion over the annual toll 10 yr. ago.

The index was compiled in a large research program, in which dated and uncoated steel panels were left exposed at industrial sites throughout the country. The panels were of 28 gage, low carbon, cold-roll sheet steel. Thousands of panels were dated and left exposed. Periodic examination of the panels provided the data for the Rust Index. Criterion for the Index was the time it took for the uncoated steel panel to rust to a severe degree.



New Polyethylene Resists Combustion

A new flame-retardant high-density polyethylene is immediately self-extinguishing after removal of a 30-second applied flame (left). Ordinary untreated high-density polyethylene continues to burn (right).

Developed by W. R. Grace (N. Y.) and now commercially available in a range of colors, the novel material has been used in tanks (cylinder heads) containing nitrogen, oxygen and acetylene. Other possible applications: ducts, piping, linings.

International Plastics Standardization Meeting

Plans are now complete for an International Symposium on Plastic Testing and Standardization to be held in Philadelphia Oct. 30-31, 1958.

The program is sponsored by ASTM on behalf of the American Group for the International Organization for Standardization (ISO). Sessions will include such topics as test methods for engineering properties; thermal properties of plastics; methods for molecular characterization (Continued).



USCOWELD PLASTIC PIPE FITTINGS

Greater Joint Strength—Faster Insertion—Thanks to THE ONLY SOLVENT-WELD FITTING WITH AN INTERFERENCE FIT!

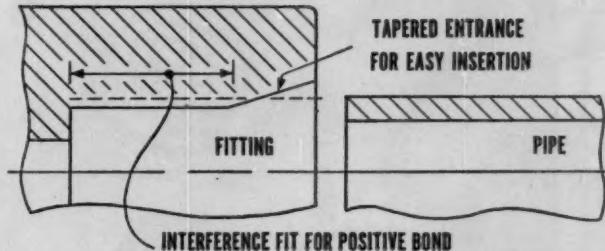
To get maximum joint strength, interference fit is a must! UscoWeld fittings are designed to provide at least a .005 inch *interference fit*. And UscoWeld fittings are a cinch to install because of a specially designed *tapered entrance socket*. U.S. Rubber has developed the unique UscoWeld fitting of the same tough, lightweight, corrosion-resistant thermoplastic as famous Uscolite® CP plastic pipe.

All UscoWeld fittings can safely handle the pressures recommended for the corresponding size of extra-heavy Uscolite pipe. Maximum recommended operating temperature is 170°F. Pipe can be cut to exact length, is easily installed in close quarters.

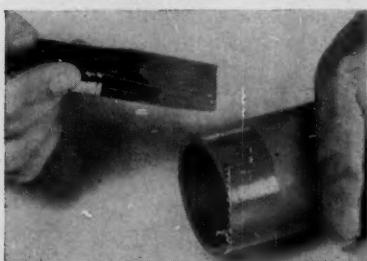
UscoWeld®—plus the most complete line of plastic pipe and fittings in America—is obtainable through your local "U. S." Distributor, any "U. S." Branch, or write us at Rockefeller Center, New York 20, N. Y. In Canada: Dominion Rubber Co., Ltd.

*Patent applied for

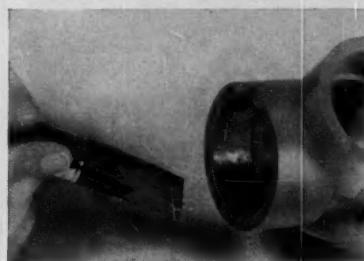
THE USCOWELD PRINCIPLE



By combining tapered entrance socket and a .005 inch interference fit—even when the pipe is at the small limit of the diameter tolerance and the fitting at the large limit of its diameter tolerance—UscoWeld is easily installed, and the strongest solvent-weld joint available.



Apply Uscolite CP cement to the outside area of the pipe that is to be in contact with the socket.



Next apply cement uniformly to entire inside area of tapered entrance socket.



While both cemented surfaces are still wet, insert pipe in fitting and push until pipe bottoms against shoulder in the fitting.

ADVANTAGES

- fast, easy to assemble—tapered entrance provides easy insertion of pipe
- strong joint—interference fit provides for optimum fusion of pipe and fitting into homogeneous mass; joint strength not dependent on cement alone
- automatic alignment of pipe and fittings
- chemical resistance of the UscoWeld joint is the same as for Uscolite pipe

- UscoWeld takes maximum advantage of the inherent "solvent-weldability" of plastic pipe and fittings
- no threading required—just cut pipe square
- not necessary to allow for thread make-up variation—pipe can be cut to exact lengths
- easy to install in close quarters
- resists fatigue due to vibration or thermal stresses by elimination of stress concentration at thread roots.



Mechanical Goods Division

United States Rubber

WORLD'S LARGEST MANUFACTURER OF INDUSTRIAL RUBBER PRODUCTS

Rockefeller Center, New York 20, N.Y.

In Canada: Dominion Rubber Company, Ltd.

Ultra-High Strength Steel Available

Looking for an ultra-high strength metal? U. S. Steel has developed a new steel with a tensile strength of 280,000 psi. Called Airsteel, it's made by a novel air cooling technique.

Most steels call for oil or salt quenching to develop good me-

chanical properties. USS metallurgists have come up with a steel containing alloying elements which allow it to harden in the open air after heating.

Commercial heats have been produced. U. S. Steel believes the new product is highly suitable for missile and chemical process applications. It's available in bars, plates and sheets.



How Zirconium Fabricating Difficulties Were Solved

Zirconium is a tough customer to work with. The problems Pfaudler ran into when fabricating the first zirconium heat exchanger point up some of the difficulties and solutions.

It's not easy to cold-form zirconium, so it had to be heated to 600-900 F. before forming. Also zirconium can't be welded to any other metal; and like titanium it has a strong affinity for oxygen and nitrogen, which makes it brittle. Tungsten-arc welding had to be performed

in an inert argon atmosphere using a specially constructed welding chamber (above).

The final 11½-sq. ft. exchanger has solid zirconium bonnets and tubing, and zirconium-lined tube sheets. The 4½-in. I.D. shell is of polished Type 304 stainless steel. Tube sheets were welded to the stainless shell with the tubing protruding slightly. The tubes were then roller expanded, zirconium tube sheet lining placed over the protruding ends and seal-welded to the tubes.

New Process Sprays Any Metal

Can any known element be sprayed onto a supporting material? The answer is yes, according to the Giannini Plasmadyne Corp. (Santa Ana, Calif.) They've coated cold steel with tungsten using a new spraying technique, based on the "plasma-energy" principle.

Energy from an electric arc is transferred to an ionized gas medium creating temperatures up to 25,000 F. The hot gas forms a jet traveling at about 13,000 ft./sec. This jet is used to heat the metal to be sprayed.

Some immediate process applications (besides missiles and nuclear power) include coating of high-temperature pump and bearing surfaces, combustion chamber valves, high-speed grinding and cutting surfaces.

Butyrate Plastic Easy to Strip

A peelable butyrate plastic coating, developed for metal plating operations, should also solve some tough corrosion problems.

Previously, in metal plating, parts to be partially plated were usually dipped in a lacquer coating which calls for a relatively long drying time. Also, such coatings are difficult to remove.

Now a part is partially plated by first dipping in a bath of molten butyrate. Then it's withdrawn. The plastic coating solidifies within 60 seconds and it's easily trimmed or peeled away from the area to be plated.

After plating, the coating is readily stripped off and returned to the melt tank for re-use.

Result has been a substantial reduction in plating time and labor costs over conventional methods.

The coating is non-exuding—it doesn't leave any residue.

Such a coating should prove useful as a protective lining for parts which will be stored in a corrosive atmosphere or as masking agents for painting.

Coating was developed by Seal-Peel, Inc., Royal Oak, Mich., using Eastman Chemical butyrate.

When Castings Become an Engineering Problem...

REMEMBER THAT

WE
CAST
ALL

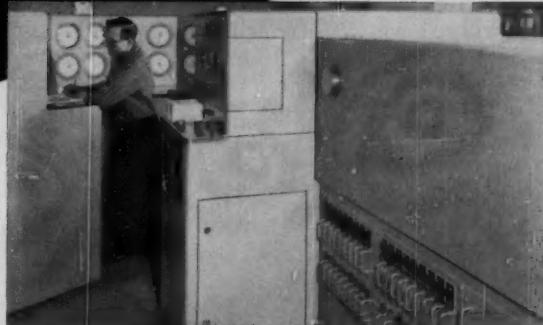
3

There are two facts which may be highly important to you. First, WAUKESHA is comprised of three separate foundries with expert experienced, *specialized* management for each.

1. One foundry casts only Stainless Steel, 300-400 series, Ni-resist and special corrosion resistant formulations.
2. Another casts only "Waukesha Metals" (copper base, high nickel alloys), pure nickel, Monel, brass, bronze, Everdur.
3. The third casts only Aluminum — as cast and heat-treated.

Second, over all three foundries are two laboratory operations, one for quality control and the other for metallurgical research. Both work for your interests. As examples of quality control: a spectrometer checks every heat; formulations can be corrected before the metal is poured. The laboratory also controls all supplied materials.

But perhaps more important to you when you have any problem such as corrosion resistance, heat resistance, galling or machining, is the Research Laboratory. Let it suffice to say that we have solved intricate metallurgical problems for many WAUKESHA customers. And this we offer — without charge — to you. Simply send a print or a pattern and tell us your need. You have everything to gain.



The spectrometer at WAUKESHA for quality-control



Part of the metallurgical laboratories for quality-control and research

Waukesha
FOUNDRY COMPANY

5805 Lincoln Ave. • Waukesha, Wis.

FIRMS IN THE NEWS

R. A. LABINE

NEW FACILITIES

October's Top Projects:

Chemical Construction Corp. will build a new ammonia-urea plant for Cooperative Farm Chemicals of Lawrence, Kan. Ammonia unit, rated at 100 tons/day, will be based on natural gas; urea plant will produce 30 tons/day for urea-ammonium nitrate solutions.

Union Carbide Chemicals plans to erect new plant at Institute, W. Va., to produce 10 million lb./yr. epoxides and other hydrogenated chemicals. Unit is scheduled for completion in mid-1959.

Columbia-Southern is building a large cement plant at Barberton, Ohio—capacity 1.5 million bbl. cement annually. Plant will use wet process, will include rotary kiln 450 ft. long and 13 ft. in dia.

Harvey Aluminum has started regular production at its new aluminum reduction facility at The Dalles, Ore. Plant capacity is more than 100 million lb./yr., features many automatic operating techniques.

Dow's Texas Div. is producing aluminum chloride in a "small facility" at Plant B in Freeport. Initial production of this catalytic agent is being consumed internally, principally in production of ethyl benzene.

Louisiana Chemical Corp. has awarded a \$3-million contract to Delta Engineering Corp. for expansion of natural gas extraction plant near Magnolia, Ark. Firm operates plant for Columbia Products; expansion will add ethane recovery facilities to the installation.

Monsanto's Lion Oil Div. plans a multimillion-dollar expansion of its El Dorado, Ark., refinery. Program will boost rated crude throughput from 29,000 to 33,000 bbl./day and will include new hydro-desul-

furization, decarbonization and tetramer units.

Aluminum Co. of America's Massena, N. Y., smelting operation became first industrial consumer of electricity from long-awaited St. Lawrence Seaway Project. Alcoa built new facilities to utilize new power source, brings total capacity at Massena to 54,000 tons/yr. aluminum.

Dow has started production of iminodiacetic acid at its Midland, Mich., plant; is believed to be only commercial producer. Acid finds use as intermediate for surface active agents, complex salts and chelating agents.

Carborundum's expanded facilities at Niagara Falls for manufacturing boron carbide are now in full operation. Accelerated production was precipitated by industrial advances demanding this abrasive—exceeded only by the diamond in hardness.

General Electric is building a \$1-million radiochemistry building at the 300-acre

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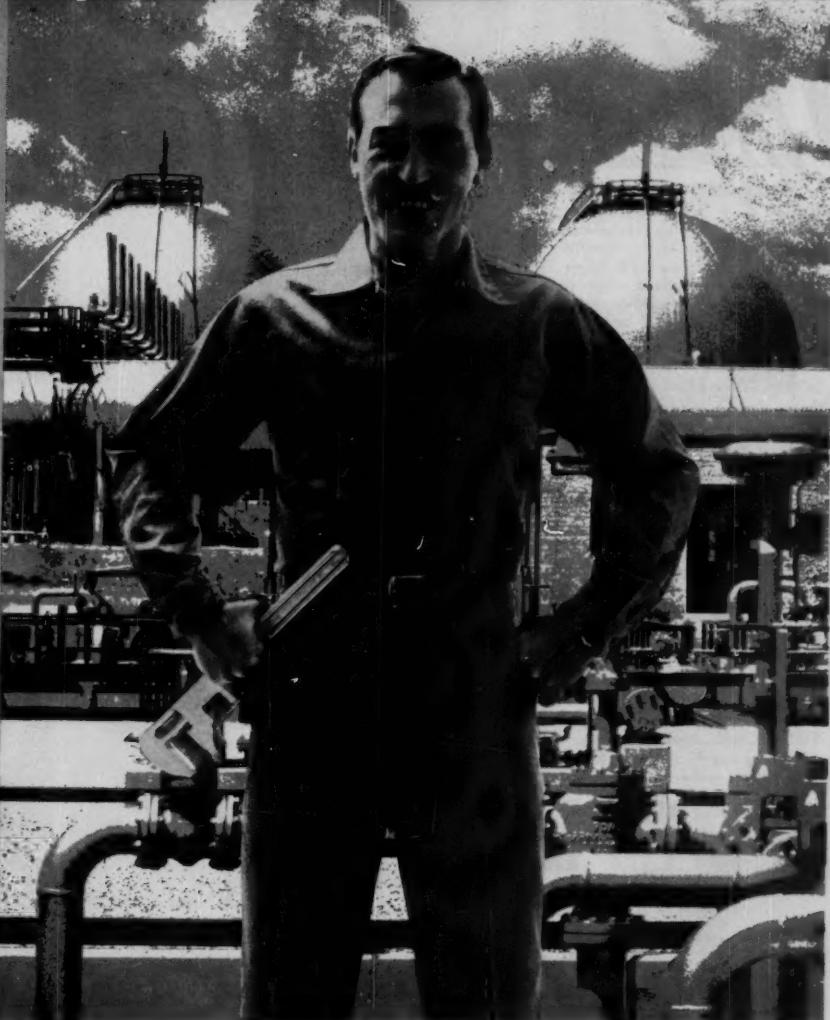
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Dynel resists chemical deterioration, laundering and abrasion...delivers important use economy.

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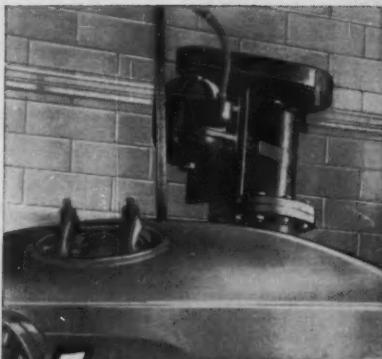
DYNEL • a



textile fiber

Textile Fibers Department, Union Carbide Chemicals Company, Division of Union Carbide Corporation, 100 East 42nd Street, New York 17, N. Y. Offices in Boston, Mass. at 300 First Avenue, Needham Heights; Charlotte, N. C. at 1213 Liberty Life Building; Montreal, Que.; Toronto, Ont.

"Union Carbide" is a registered trade-mark of UCC



ADVANCED Engineering - and better SELECTION -- with

"International" MIXERS

SIDE ENTERING

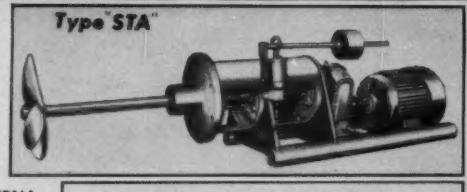
Each of these different types of Mixers has its particular mechanical advantages which make it more efficient for specific purposes. There are many considerations in every application where a wide range of types and materials must be available.

With the complete "INTERNATIONAL" Line of Mixing Machinery to choose from, you can be sure of our unbiased recommendation of the right type mixer for each specific job.

Special Metals used in Mixer construction are available—iron, bronze, stainless steel, high nickel alloys, etc.—You pick the sealing arrangement, either standard packed or New Mechanical Seal. Your choice of Power drive—Garmotor, V-Belt or Silent Chain.

MOTOR Selection—Any standard motor with NEMA frame—any current, insulation or enclosure.

GUARANTEED PERFORMANCE—25 Years of continuous building, testing, study and research experience goes into every "INTERNATIONAL" application—it assures you of getting exactly the right Mixer for top performance and economy.



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"INTERNATIONAL" Vertical Drive Heads are made in various types and sizes from 1 to 100 H.P. for Propeller and Turbine agitation,—slow speed or high speed—and for Open or Closed Tanks and vessels. Standard Stuffing Box or New Mechanical Seal.



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The most adaptable Mixer ever built. Patented. High Speed, Slow Speed and Intermediate. Production and Laboratory Models—Special Bulletin 74 B



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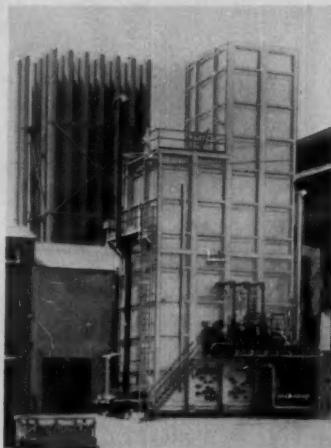
DAYTON 1, OHIO

New Catalog of Mixing Equipment No. 83, Sent on Request

FIRMS . . .

atomic plant in Hanford, Wash. New structure will house advanced research including high-level radiation work up to 1 million curies.

Heyden Newport's Nuodex Products Co. is expanding production facilities at Elizabeth, N. J., for nickel catalysts and plating salts. Line now includes nickel sulfate, chloride, formate, carbonate, nitrate and acetate.

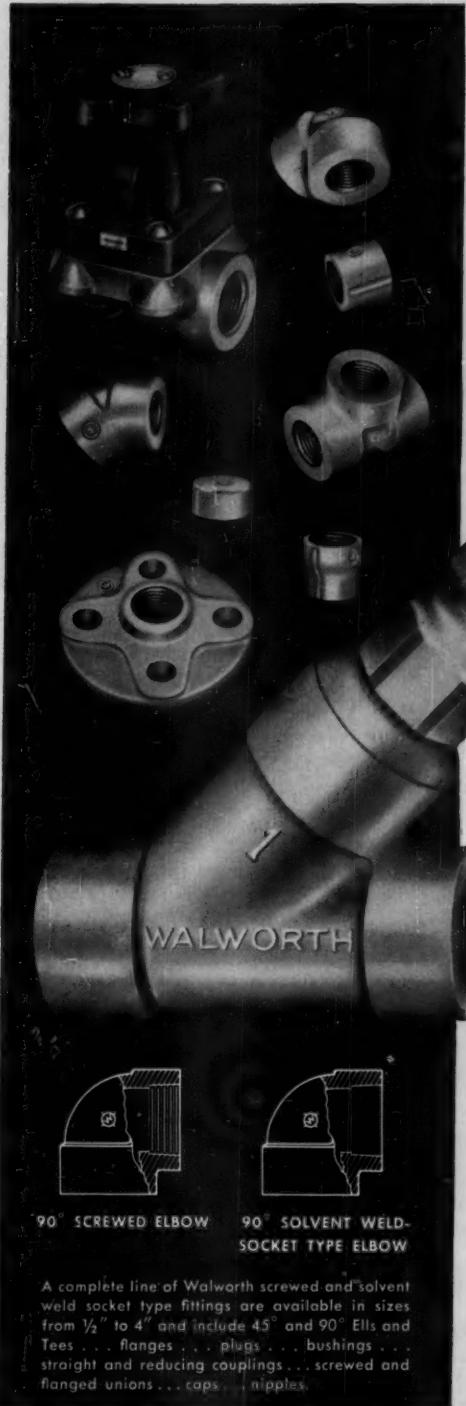


Granite City Steel Co.'s latest addition is a 60-million-cu.-ft./mo. oxygen generating unit built by Air Products. Most of output is being piped to company's seven open hearth furnaces.

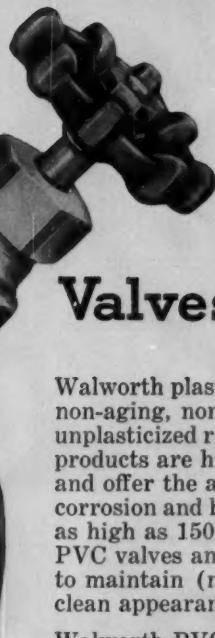
Air Reduction has upped daily production capacity at its Lorain, Ohio, gaseous and liquid oxygen plant to 100 tons/day. Most of increased output will be soaked up by local steel makers.

British American Oil Co. is about to open two plants this month valued at \$50 million: B-A's natural gas processing plant at Pincher Creek in southern Alberta will be dedicated Oct. 15th. Company's new 20,000-bbl./day refinery just outside Vancouver, B. C., is going through test runs for its official opening Oct. 17th.

Manhattan Adhesives Corp., Brooklyn, N. Y., has placed its new polyvinyl acetate and



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WALWORTH
PVC
(rigid polyvinyl chloride)

Valves and Fittings !

Walworth plastic valves and fittings are made of non-aging, non-corrosive and non-toxic unplasticized rigid polyvinyl chloride (PVC). These products are highly resistant to chemical attack and offer the advantages of immunity to galvanic corrosion and high impact strength at temperatures as high as 150°F. Durable and light, Walworth PVC valves and fittings are simple to install, easy to maintain (no painting), and add a smooth, clean appearance to your piping system.

Walworth PVC Y-Globe Valves are designed to regulate the flow of alkalies, acids, and similar corrosive fluids. Walworth PVC Diaphragm Valves* are commonly used in systems handling corrosive fluids, especially those containing suspended materials, and can be furnished with diaphragms suited to your application.

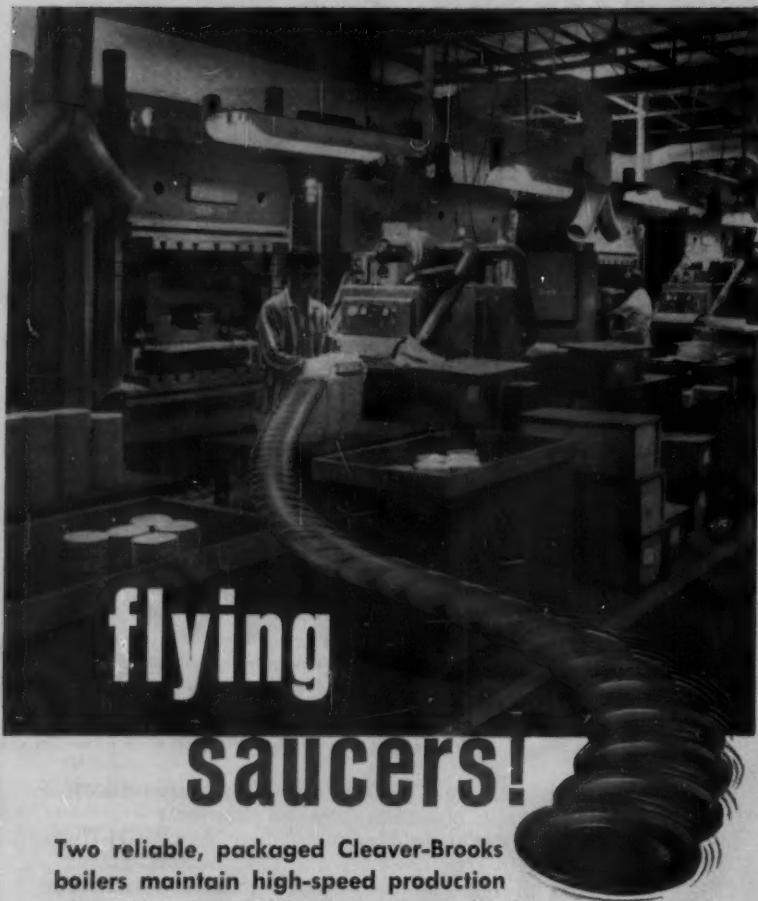
*Hills — McCanna (Saunders Patent)

SEND FOR THIS BOOKLET. It describes mechanical and thermal properties, working pressures, sizes and dimensions, application and assembly data for the complete line of Walworth PVC Valves and Fittings. Please use company letterhead.



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flying saucers!

Two reliable, packaged Cleaver-Brooks boilers maintain high-speed production of Texas-ware and Dallas-ware melamine dishes for Plastics Mfg. Co., Dallas

Chief engineer, W. L. Cone, Jr., states: "Consistently dependable steam supply is keynote of our plant operation. That's why we chose two Cleaver-Brooks gas-fired boilers for our steam source.

"One feature we appreciate about these new boilers is the easy access to their internals. Not only does this facilitate frequent inspections but also it greatly reduced their cost. There are no joints that require resealing every time the boiler is opened. Being hinged and davited, the doors and heads do not have to be hoisted for removal. Six bolts can be removed in less than two minutes."

Guided by experience

"Based on nine years of unfailing performance delivered by two 50-hp Cleaver-Brooks boilers we used in our former plant, there never was any question that we would install their equipment in our new plant," said Mr. Cone.

Architects for the new plant were: Thomas, Jameson and Merrill; Consulting engineers: Zumwalt and Vintner; General contractor: Carpenter Bros.; Mechanical contractor: Beard Plumbing Company, all of Dallas.



"Our 125-hp, 250-psi design pressure, gas-fired Cleaver-Brooks boilers provide all steam for compression-molding presses, office space heating and hot water heating" — W. L. Cone, chief engineer.

Cleaver-Brooks packaged boilers are America's largest selling packaged boilers. Available in 19 sizes, 15-600 hp, 15-250 psi. Oil, gas or combination oil/gas fired. For complete information contact nearest representative or write: Cleaver-Brooks Co., Dept. L, 345 E. Keefe Ave., Milwaukee 12, Wisconsin, USA.

Originators and largest producer of packaged boilers

Cleaver  **Brooks**®

FIRMS . . .

resins plant in full production to furnish complete line of polyvinyl solutions and emulsions.



U. S. Steel's Gary, Ind., Works boasts a new 94-million-cu-ft./mo. oxygen plant built, maintained and operated by Linde Co. Oxygen will be used in cutting, scarfing, scrap preparation and other metallurgical processes.

Texaco announces completion of "world's most fully equipped industrial radiation research laboratory" at firm's research center in Beacon, N. Y. Lab will probe atomic structure of petroleum and its derivatives with view towards improving fuels, lubricants and petrochemicals.

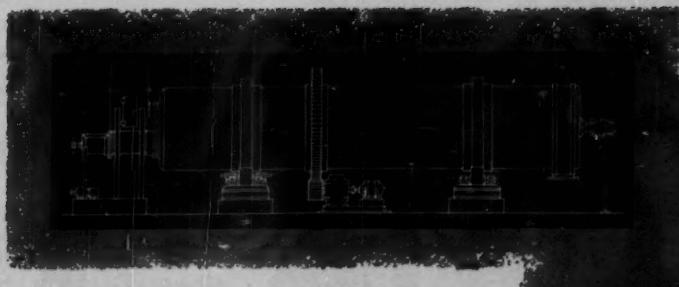


MERGERS &

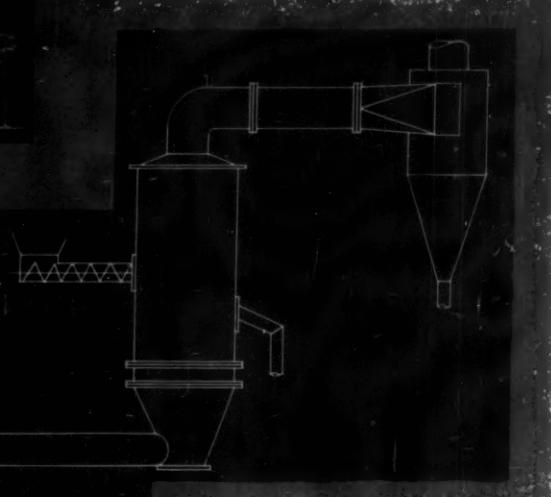
ACQUISITIONS

Chromalloy Corp., White Plains, N. Y., has acquired Propelllex Chemical Corp. of Edwardsville, Ill., through a stock exchange. Continuing as Propelllex Chemical Div., firm is producer of solid propellant rockets and fuels, and other propellant and explosive devices.

A. E. Staley Mfg. Co. of Decatur, Ill., has purchased the Hipolite Co. of St. Louis. Manufacturing facilities for Hip-O-Lite Marshmallow Creme are being moved from St.



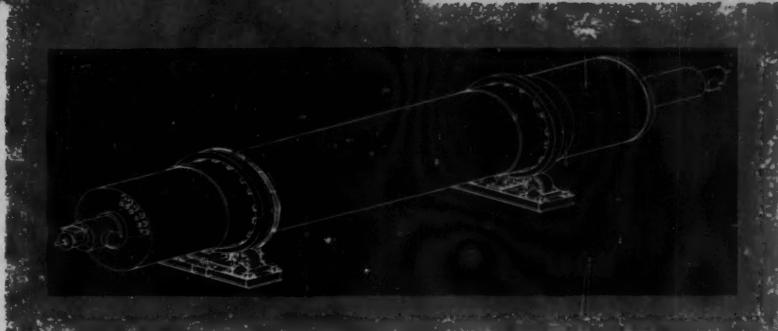
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Now, at one convenient location, you can test-dry your materials in a variety of equipment

At General American's East Chicago pilot plant, you can test the drying or reacting of your materials in the widest range of drying equipment ever assembled in one place.

Louisville Dryer engineers will work with you—study your materials and needs, make recommendations for type of equipment, size and heating medium. You can check these recommendations for yourself through practical tests. Your Louisville Dryer is then engineered for most efficient and economical service—built specifically to meet your needs.

To test the drying of your materials in all these different types of drying equipment, call in a Louisville Dryer engineer. There is no cost or obligation.



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APPROACHES



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The CROSS-BORE exchanger is a new design which reflects all of the advantages of impervious graphite, particularly its property of possessing one of the highest rates of thermal conductivity of any commercially available material of construction. In addition, the CROSS-BORE is unaffected by all corrosives except a few highly oxidizing agents, features strong, shock resistant construction, possesses 20% higher overall heat transfer coefficient than tube and shell design, provides for fast, positive cleaning of shell side as well as tube side holes, is immune to thermal shock, accommodates working pressures to 200 psi at temp. to 340°F., (specials to 400°F.) and is available in 14 standard capacities to 470 sq. ft. of transfer surface.

New bulletin available on request.

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Completely
assembled
CROSS-BORE
exchanger

FIRMS . . .

Louis to Decatur and product will be added to Staley's grocery line.

Du Pont has purchased the idle Cornwells Heights, Pa., sulfuric acid plant of Cornwell Chemical Corp. Plant will become part of Grasselli Chemicals Div. after modernization.



NEW COMPANIES

Plastic Coated Paper Corp., with headquarters in Hicksville, L. I., is a new firm specializing in polyethylene coatings. New plant, to be finished by late 1958, will coat paper, board and foil in addition to other materials.

Union Bag-Camp Paper Corp. has established a new chemical products division emphasizing the increasingly important role that chemicals are playing in company operations.



NEW LINES

Pacific Vegetable Oil Corp. is diversifying in the urethane polymer field through its recently acquired interest in Polytron Corp. New affiliate will manufacture urethane polymers and will conduct research on new urethane derivatives.

S. C. Johnson & Son, wax makers, has purchased patent rights to Porelon, a new synthetic material with "abundant product possibilities." Porelon is claimed to be first synthetic in which liquid can be trapped during manufacture, then given off at predetermined rate. Product possibilities include marking stamps and self-lubricated bearings.

WASTE DISPOSAL PROBLEMS?



HAS THE ANSWER . . .

John Zink Waste Disposal Units are custom designed to your specifications, for your individual application. Any size or capacity can be furnished for use in reducing liquid and semi-liquid wastes, or obnoxious gases. Available as a complete unit or burners only. John Zink Waste Disposal Units have been field-proven in process service throughout the world.

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. . . and 33 other platinum group metal chemicals.

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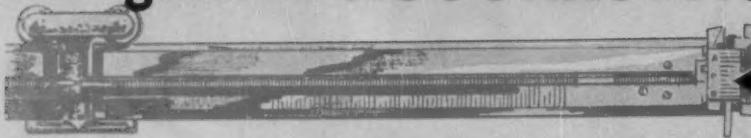
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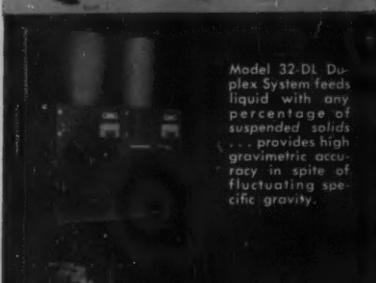
New gains in ACCURACY...



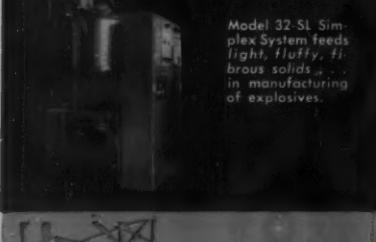
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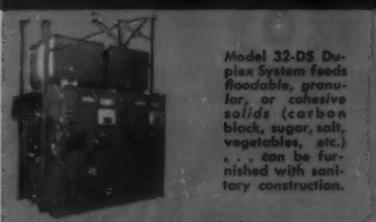
Model 32-SL Simplex System accurately feeds volatile liquid food flavoring. Total charge is contained in small tank.



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Accurate feeding of solid and liquid materials is the key to successful, economical continuous processing. Using the most advanced engineering principles, Omega Model 32 Continuous Loss-in-Weight Feeding Systems outperform ordinary feeding methods by setting accuracy standards never before attainable. That's why more and more processes are depending on Omega:

ACCURACY:

Guaranteed $\pm \frac{1}{2}\%$ by weight of set feed rate (NOT of "full scale load" as many other systems are rated).

AUTOMATIC CONTROL:

A full closed loop . . . with feedback and memory features.

FLEXIBILITY:

Handles difficult materials easily — granular, floodable, slurries, volatile, explosive, others. Typical examples are shown at left.

AUTOMATIC SELF-CALIBRATION:

No sampling required. Totalizes weight delivered. Positively prevents cumulative over or underfeeding.

VERSATILITY:

Feeds any flowable solid or liquid material by proper selection of feed mechanism.

CAPACITY:

Simplex and Duplex Systems to feed 1#/hr. to 60,000 #/hr.

RANGE:

As required: 10:1 up to 50:1

NEW BULLETIN

32-R2 describes Omega Continuous Loss-in-Weight Feeding Systems — their design, operation, capacities, dimensions, and applications. Write for your copy, today.

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FEEDERS
CONTROLS

OMEGA MACHINE CO.
DIVISION OF
B-I-F INDUSTRIES

CALENDAR

American Society of Mechanical Engineers—American Society of Lubrication Engineers, Lubrication Conference, Statler Hotel.
Oct. 13-15 Chicago, Ill.

American Gas Assn., annual convention.
Oct. 13-15 Atlantic City, N. J.

Packaging Institute, 20th annual forum, Edgewater Beach Hotel.
Oct. 13-15 Chicago, Ill.

Society of Industrial Packaging and Materials Handling Engineers, annual national exposition, Coliseum.
Oct. 14-16 Chicago, Ill.

National Assoc. of Corrosion Engineers, North Central Regional Conference.
Oct. 15-17 Cincinnati, Ohio

Instrument Society of America, National Rubber and Plastic Symposium.
Oct. 20-21 Akron, Ohio

Technical Assn. of the Pulp and Paper Industry, 13th Plastics-Paper Conference, Sheraton-Kimball Hotel.
Oct. 20-22 Springfield, Mass.

American Oil Chemists Society, fall meeting, Sheraton Hotel.
Oct. 20-22 Chicago, Ill.

National Assn. of Corrosion Engineers, South Central Regional Conference and Exhibit.
Oct. 20-24 New Orleans, La.

American Vacuum Society, 5th National Vacuum Symposium, Sir Francis Drake Hotel.
Oct. 22-24 San Francisco, Calif.

American Institute of Chemical Engineers, New York Section, All day symposium: Cost Engineering, Foams and Froths, Petroleum Chemicals; luncheon speaker: George Holbrook, AIChE President; Hotel Statler.
Oct. 23 New York, N. Y.

National Society of Professional Engineers, fall meeting, St. Francis Hotel.
Oct. 23-25 San Francisco, Calif.

National Metals Exposition, Cleveland Public Auditorium.
Oct. 27-31 Cleveland, Ohio

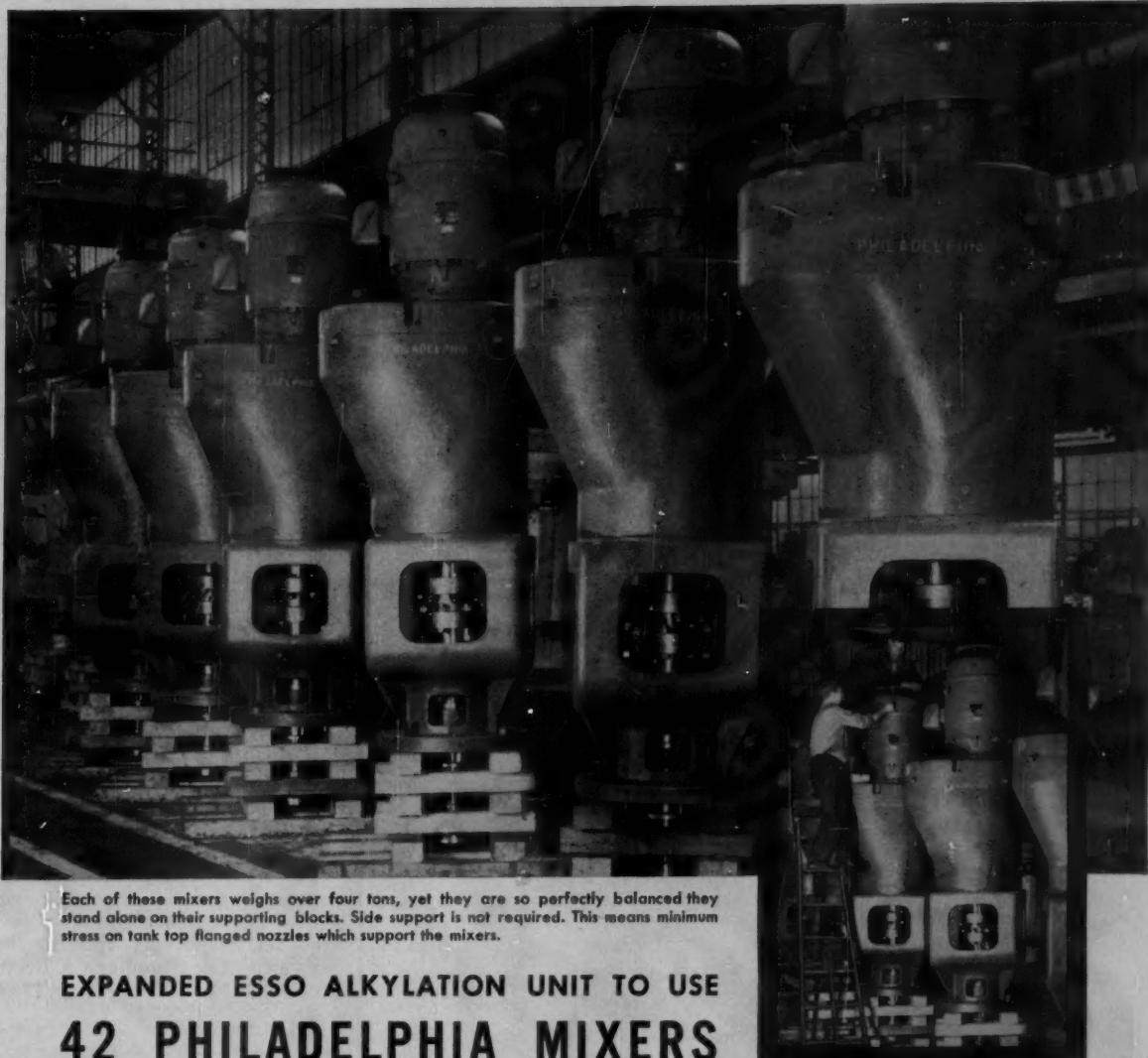
Assn. of Consulting Chemists and Chemical Engineers, annual meeting, Biltmore Hotel.
Oct. 28 New York, N. Y.

National Agricultural Chemicals Assn., 25th annual meeting, Bon Air Hotel.
Oct. 29-31 Augusta, Ga.

American Society for Testing Materials, International symposium: Plastics Testing and Standardization, Benjamin Franklin Hotel.
Oct. 30-31 Philadelphia, Pa.

Industrial Management Society, 2nd annual seminar on Executive Techniques of Industrial Engineering.
Oct. 4-5 Hotel Sherman.

Chicago, Ill.



Each of these mixers weighs over four tons, yet they are so perfectly balanced they stand alone on their supporting blocks. Side support is not required. This means minimum stress on tank top flanged nozzles which support the mixers.

EXPANDED ESSO ALKYLATION UNIT TO USE 42 PHILADELPHIA MIXERS

Forty-two vertical Philadelphia Mixers like the ones shown are being installed at the Baton Rouge Refinery of Esso Standard Oil Company by Foster Wheeler Corporation. They are part of an alkylation process in which concentrated sulfuric acid serves as a catalyst to unite light olefins and isobutane to produce high octane gasoline blend stock. Installed in the various reaction zones of the reactors, they insure optimum contact of reactants.

These units are equipped with a shut-off device below the mechanical seal which permits seals to be changed with reactor vessels held at full pressure. This can be done simply and quickly, and requires *no external lifting equipment*.

For this, or any other fluid mixing job, Philadelphia Mixers offer many important design advantages.

- Extra large, heavy duty bearings throughout permit every drive component to be designed to required

degree of stiffness. The strength and rigidity of drive assemblies keep gearing effectively isolated from unbalanced output shaft loads which might cause damage.

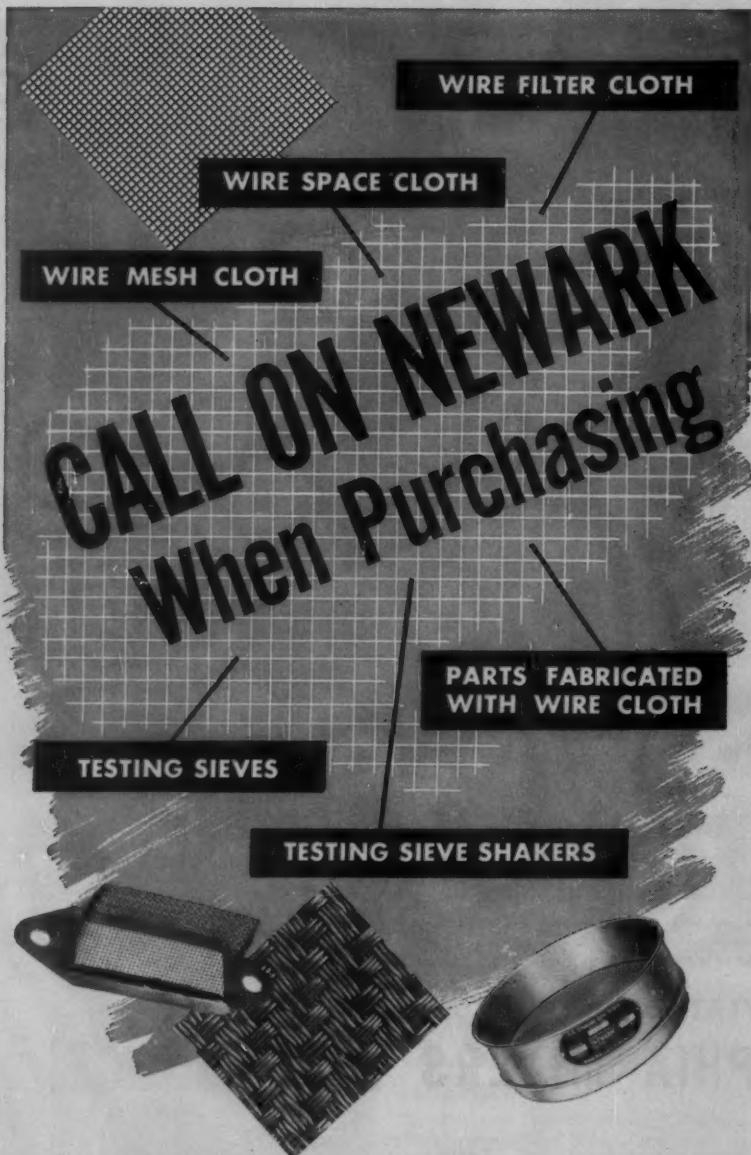
- Extremely heavy output shafting keeps shaft deflection to an absolute minimum, even under heavy unbalanced mixing loads.
- Extra long output shaft bearing span insures precision shaft operation and minimum runout in the seal area.
- All gearing is induction hardened and ground or crown shaved for long, quiet, trouble free life.
- Quick change gear sets are available from stock to furnish 14 standard AGMA output speeds.

To select the exact mixer for your process needs, write for Catalog A-27. It contains all the information needed to make a catalog selection of a complete mixer assembly.

PHILADELPHIA GEAR CORPORATION
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Make NEWARK your source of supply for Wire Cloth and Wire Cloth Products. We weave all of our own cloth from which we fabricate parts for our customers...thus insuring both quality of cloth and accuracy of construction.

Newark Wire Cloth is available in all standard widths, all meshes, all commercial metals...the Newark line is a complete line even up to 400 mesh cloth. And if your problem is one of parts design, our engineers will be glad to aid. May we quote on your requirements?

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NEW EQUIPMENT . . .

(Continued from p. 74)

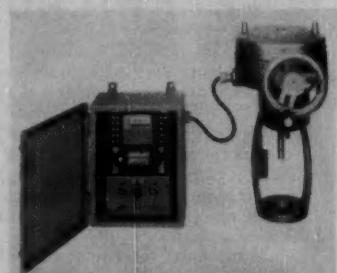


Glass Tester

Electronic unit checks glassed-steel continuity.

Known as the Pfaudlertron, a new constant-voltage electronic tester checks the surface continuity of glassed-steel equipment. The non-destructive instrument is claimed to be the first unit available for such service in the field.

Testing procedure consists of methodically sweeping the brush-type probe over the glassed surface. When a defect is present, a neon bulb in the probe handle glows with unmistakable brightness. Prolonged inspection will not endanger equipment or personnel. Stabilized output is 3,500 v., a.c.—The Pfaudler Co. Rochester, N. Y. 176A



Valve Positioner

Designed to operate from electric controllers.

All electric, a new valve positioner eliminates need for auxiliary hydraulic and pneumatic systems. Transistorized and explosion-proof, the positioner incorporates a unique braking system that prevents valve oscillation and assures repeatability to within $\frac{1}{2}\%$. A 1/40-hp, 2-

phase induction motor drives the unit's actuating shaft through an efficient gear train and ball-screw mechanism. Built-in limit switches prevent valve damage.

Stroke is field-adjustable from $\frac{1}{2}$ to 2 in.; stem speed is 0.15 in./sec. and maximum thrust is 1,000 lb. — Norwood Controls Div., American Standard Products, Norwood, Mass. 176B



Remote Firefighter

New system quenches intensely hot fires.

An urgent outgrowth of the U. S. missile program, the new Akron system for remote fire fighting may soon find application in the process industries. Designed for rapid combat of fires that are too hot or too dangerous to allow human firefighters to work at close range, the foam-throwing units now stand guard at Cape Canaveral.

Mounted at the base of the launching stands, the systems are claimed to be completely automatic. Remote controls, placed in the observation bunker about $\frac{1}{2}$ mile away, raise, lower, and rotate the units, and also change stream widths.—Akron Brass Mfg. Co., Wooster, Ohio. 177A

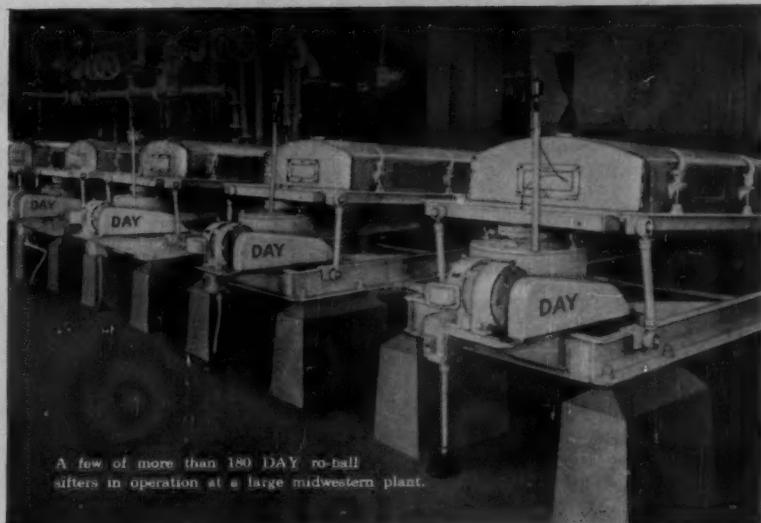
Dry Classifiers

Two new machines feature high efficiency.

No moving parts, virtually no required maintenance and exceptionally low power requirements are just some of the advantages claimed by the

SIFT finer-faster-cleaner

with **DAY** ro-balls



A few of more than 180 DAY ro-ball sifters in operation at a large midwestern plant.

Today thousands of products wet or dry, from flour to wood chips, are sifted through efficient, low-cost, high-production DAY ro-ball sifters. Superbly engineered, built for trouble-free operation under the severest service conditions, they insure longer life with lower maintenance costs.

The exclusive super active ball cleaning device provides rebound points in each ball compartment, assuring fast, thorough sifting of your product. Gyrating action brings material into constant contact with every square inch of screen surface. A stabilizer maintains screen in horizontal position and insures smooth operation.



DAY standard ro-ball, available in six sizes, single or multiple screens. Single screen models in stock.



Stainless steel units available to meet food and dairy sanitary codes.

Many models are available so it is easy to choose one which will exactly suit your requirements. They can be used separately or in combination with DAY mixers or blenders to save product handling. A completely equipped lab is available for testing your product.

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RECIRCULATION MAY BE KEY TO FUTURE GROWTH OF CHEMICAL AND INDUSTRIAL PROCESSES

How much water do you need to make: a ton of steel? a ton of synthetic rubber? a ton of bromine? a barrel of beer?

These are not empty questions. They point to a critical problem which confronts management today in its plans for tomorrow. It is more critical than most of us realize... for industry today uses as much water as all other users.

Industry's Needs in 1975

Water is vital for chemical and industrial growth. By 1975, industry will require 215 billions of gallons daily. That is a 100% increase over our current industrial consumption... more than we currently consume for all uses combined.

Competing for this water will be irrigation farmers and the general public. Their combined needs by 1975 will be up 40 billion gallons a day... possibly even more.

What is the Supply Picture

More than 40% of the communities in the United States already have a critical water supply problem. Yet, to meet the 1975 needs, our supply must be expanded by 50%, at an estimated cost of \$50 billion.

Indications are that industry is going to have to bear its part of this cost. Certain communities are already moving to place flat water rates on all users... regardless of the volume used. Other groups are demanding a national water policy with full Federal Government regulation of natural sources.

Chemical Industry's Stake

Shortage of water can be a most serious threat to the expansion hopes of the chemical industry. A glance at the following table shows why. You need approximately:

20,800 tons of water per ton of Bromine
2,500 " " " " " Synthetic rubber
830 " " " " " Viscose rayon
300 " " " " " Newsprint
208 " " " " " Smokeless powder
15 " " " " " Coke from coal

CONSERVE WATER, OUR MOST VALUABLE NATURAL RESOURCE

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O-58

We have a problem involving liquid filtration. Ask your local representative to call on us.

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NEW EQUIPMENT...

manufacturer for two new dry classifiers. Designed for high-efficiency separation of dry fines from coarse materials, both machines can handle from 100 lb. to 100 tons of feed per hour.

One unit, the Gravitational-Inertial classifier, operates best in the 200- to 50-mesh range. Air- or gas-entrained feed enters through a top inlet and cascades down a set of inclined vanes through which air and fines are drawn off. Secondary air introduced below the vanes scrubs remaining fines from the coarse material leaving the classification zone. Regulation of the velocities of exhaust and secondary air establishes the cut point.

Initial installations of the other classifier, a centrifugal-type unit, indicate mill output increases from 10 to 300%. This machine will extract more than 98% of the particles smaller than 325 mesh from most feeds, and with no oversize material in the fines. In operation, the combined action of centrifugal and drag forces on each feed particle affects the separation.—Buell Engineering Co., Inc., New York, N. Y. 177B

Shutoff Valve

Less than 10 lb. torque controls 5,000 psi.

An in-line shutoff valve, known as the Ez-O-Trol, offers easy on-off control for hydraulic circuits operating at pressures to 5,000 psi. Designed for applications where the liquid is not subject to flow reversals, Ez-O-Trol comes in sizes from $\frac{1}{2}$ to 2 in. Standard valve body is aluminum alloy; internal parts are stainless steel.

In operation, back pressure seats the valve in a balancing pressure chamber. Actuation of the pilot by application of about 10 lb. torque to the valve handle allows back-pressure escape, thus unbalancing the unit. This quickly opens the valve to flow with low pressure drop. If desired, air-operated diaphragms or direct-acting solenoids provide remote control of the pilot.—Republic Mfg. Co., Cleveland, Ohio. 178A

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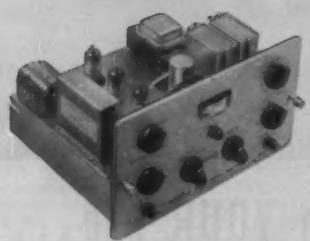
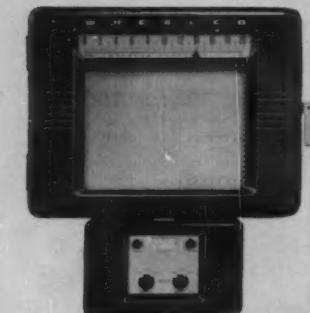


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MMC-Current Output Type—Flexible in adaptation to final control elements including saturable reactors, electropneumatic transducers, electro-hydraulic transducers, etc. . . . proportional band adjustable from 2 to 200% of controller range . . . reset action from 0 to 63 repeats per minute . . . rate action adjustable from 0 to 5.5 minutes.

MMP Position Type—Together with potentiometer can position a valve, valve positioner, or other positioning device . . . reset action adjustable from 0.6 to 100 repeats per minute . . . proportional band adjustable from 2 to 200% of controller range . . . rate action adjustable from 0 to 5.5 minutes.

MMD Duration Type—With potentiometer regulates input by adjusting on-time of a contactor on either electrical or fuel-fired installations . . . particularly adaptable when upsets are fast and recovery slow and when they are frequent and of large magnitude . . . keeps overshoot at startup or control point to minimum.

MP Proportional Positioner—Transistorized and printed circuit unit (not shown) where constant voltage source is available as reference voltage . . . mounts inside instrument . . . adjustable from 2 to 40% of recorder range.

*Also usable with Wheelco 2000 and 9000 Series.

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NEW EQUIPMENT . . .



Flow Rate Regulator

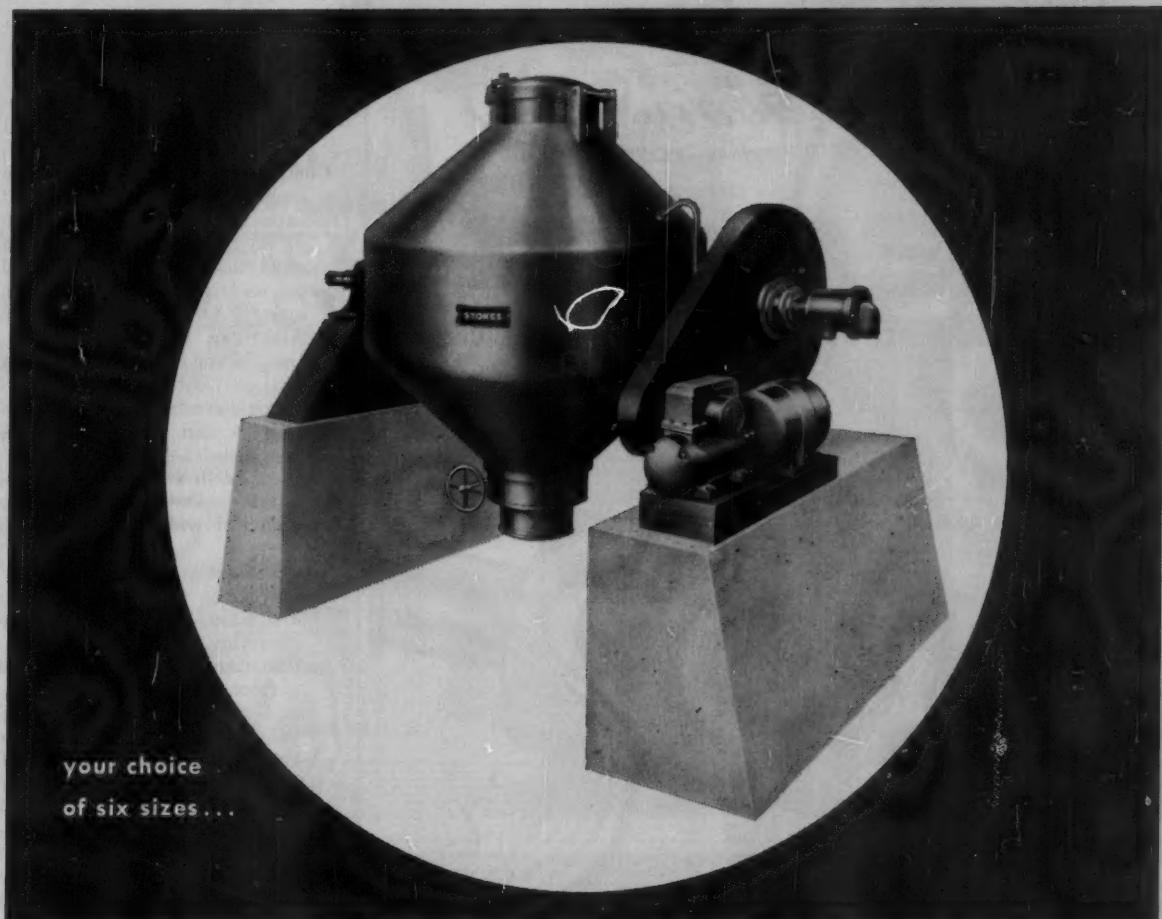
Simple, compact unit measures, controls flow.

Available for control of a wide variety of liquids and light slurries, the new Type F flow-rate regulator operates with a minimum pressure differential of less than 10 psi. It requires no outside source of power, no straight approach nor downstream piping section, and has only two-moving parts. Flow is controlled with split-second response to within 3% of set point, despite fluctuations in line pressure.

Type F regulators come in carbon steel, Type 316 stainless and special alloys for flows from 0.02 to 550 gpm. Each size provides 15:1 flow-rate adjustment by means of a calibrated dial.—W. A. Kates Co., Deerfield, Ill. 180A

BRIEFS

Thermistor beads, presently available in bare form with attached leads and without glass coating, function continuously at 1,200 F. Previous temperature limit was about 600 F.—Fenwal Elec-



Stokes Conical-Shaped Rotating Vacuum Dryers

As part of the extensive line of vacuum drying equipment offered by Stokes, this rotating cone dryer is available in six sizes. Built to Stokes' high vacuum standards, they are especially suited for those materials which require the tumbling action and/or the charging and discharging features offered by this type of dryer.

Stokes conical-shaped dryers are double-walled, and include provisions for steam or hot water heating. The interior surfaces can be supplied in carbon steel or in 304 or 316 stainless steel for use with corrosive products. The large, full-opening charging inlet is provided with a quick-acting hinged cover. The discharge port features a self-wiping

vacuum-tight valve, worm-gear actuated. Every drum is vacuum tested by mass spectrometer.

STANDARD SIZES

(special sizes and materials available)

Model No.	159-1	159-2	159-3	159-4	159-5	159-6
Working Cap.*	3	10	25	75	100	150
Approx. Wt.	1,750	2,400	3,200	7,700	11,500	12,700

*In cubic feet—normal working capacity is 65% of total volume

Call on Stokes Engineering Advisory Service for complete information and application data on these and other Stokes vacuum dryers as applied to your own production requirements.

Vacuum Equipment Division
F. J. STOKES CORPORATION
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HIGH-PRESSURE, HEAVY-DUTY EXPANSION COMPENSATOR

Inch for inch, the lowest-cost way
to take care of pipe motion



Never needs maintenance,
because it's completely
packless



Heliarc welded construction...
and steel-encased for protection
from external damage



Its 2-ply stainless steel
Flexon bellows is designed
to outlast the building



INSTALL IT...FORGET IT!

You can bank on it... Flexon Model H Expansion Compensators cost much less per inch of stroke than *any other method* of absorbing pipe expansion! Yet the Model H is built for hard service, with its 2-ply stainless steel Flexon bellows, positive internal guide and anti-torque device, and full protection from external damage.

This is why engineers and piping contractors are specifying the Model H for thousands of industrial piping jobs—in heating systems, process piping, steam tracing, power piping—that use pipe up to 3" and require up to 2" total movement at each Expansion Compensator. Working pressures to 175 p.s.i. for $\frac{3}{4}$ " and 1" sizes; to 125 p.s.i. for larger sizes up to 3".

Make the Flexon Model H Expansion Compensator a cost-cutting part of your next piping job. Write for design and cost data, and the name of your Flexon representative.

NEW EQUIPMENT . . .

tronics, Inc., Framingham,
Mass. 180B

Compressors, with pressures from 50 to 15,000 psi. and capacities to 60 cfm., handle all types of corrosive, toxic and radioactive liquids and gases. Distributor is sole U.S. agent for French line.—American Instrument Co., Inc., Silver Spring, Md. 182A

Graphic symbols for control centers and panelboards are available in metals and plastics. No limitation is made on finish.—Devco Engineering Inc., Caldwell, N. J. 182B

Strip chart recorder-controller, featuring continuous standardization and unitized construction, comes in d.c. potentiometer, a.c. or d.c. bridge versions, and both single-pen and multi-record types. Null balance.—General Electric Co., Schenectady, N. Y. 182C

Centrifugal pumps for filtrate and transfer applications have a high degree of parts interchangeability. Three new designs are available: type LH for capacities of 350 and 100 gpm. at heads of 200 and 275 ft., respectively; type LR for slurries and volatile liquids; and type LX for easy removal from service without disturbance of piping.—Dorr-Oliver Inc., Stamford, Conn. 182D

Vertical gearmotors, rated at 3 to 30 hp. and 25 to 280 rpm., provide rugged, dependable, internally-gearred power for agitator applications. Three types of motor enclosures available.—U. S. Electrical Motors Inc., Los Angeles, Calif. 182E

Integrator provides continuous means of automatically totaling flow. Designed for use in flowmeters receiving signals from conventional sensing elements.—Librascope, Inc., Burbank, Calif. 182F

Drying feeder features a cascade of heated panels that afford simultaneous rate-controlled vibratory feeding and

EC-120



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DUSTEX miniature cyclone tubes, cast of white iron, provide an ultra-hard, cling-free, self-cleaning surface to assure maximum material recovery at a constant, high-speed rate.

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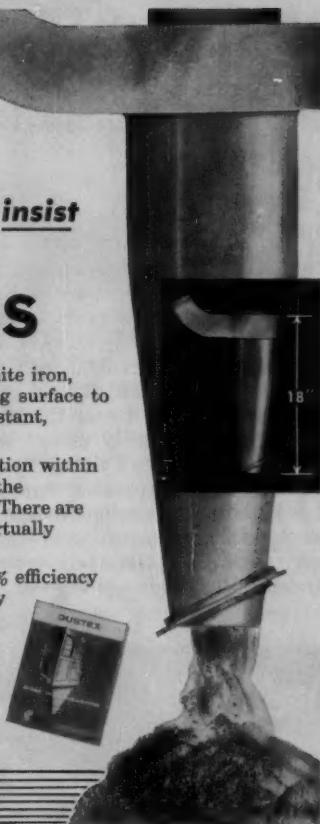
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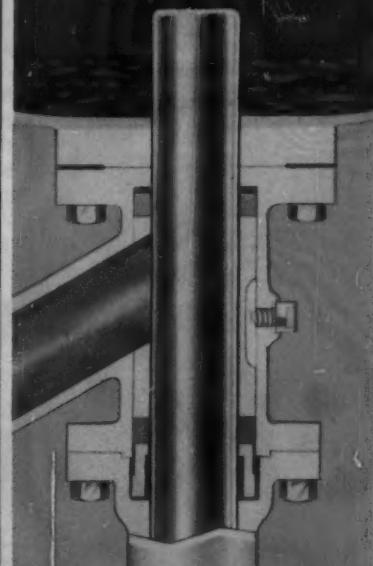
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In the open position, full and unobstructed flow is assured as the piston is drawn down into the bonnet leaving a completely open passage for the material passing through.

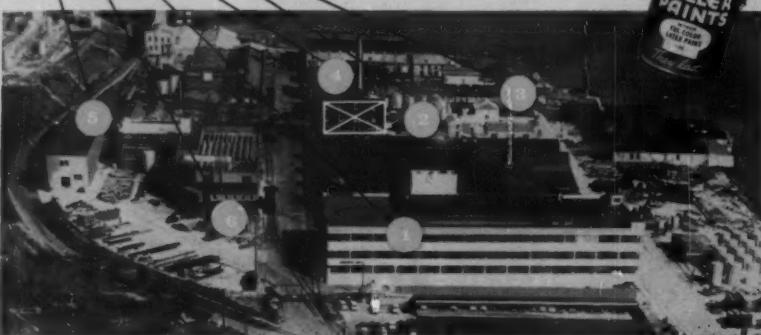
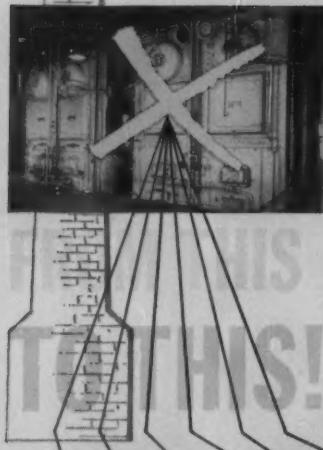
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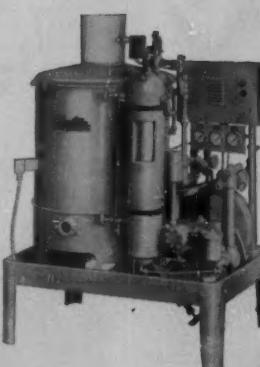
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NEW EQUIPMENT . . .

efficient bulk-materials, in-transit drying.—Syntron Co., Homer City, Pa. 182G

Vacuum dryer line features conical rotating drums. Double-walls facilitate steam or hot-water heating. Size range varies from 3 to 150 cu. ft.—F. J. Stokes Corp., Philadelphia, Pa. 184A

Dust collector manufacturer is converting its cyclone-separator dust collector line to radial fans. No increase in horsepower requirements or price.—Torit Mfg. Co., St. Paul, Minn. 184B

Motor stators, produced by casting open-type stators in an epoxy resin, are impervious to moisture and resistant to solvents, oils and most other chemicals.—Allis-Chalmers Mfg., Milwaukee, Wis. 184C

Equipment Cost Indexes . . .

Industry	March 1958	June 1958
Avg. of all	231.2	230.7
Process Industries		
Cement mfg	222.9	222.2
Chemical	232.4	231.7
Clay products	216.6	216.0
Glass mfg	219.4	218.8
Paint mfg	223.8	223.1
Paper mfg	223.9	223.3
Petroleum ind	228.6	227.9
Rubber ind	231.4	230.7
Process ind. avg	228.8	228.2

Related Industries	March 1958	June 1958
Elec. power equip	234.2	234.3
Mining, milling	233.8	233.1
Refrigerating	261.5	260.7
Steam power	219.5	218.4

Compiled quarterly by Marshall and Stevens, Inc. of Ill., Chicago for 47 different industries. See Chem. Eng., Nov. 1947, pp. 125-6 for method of obtaining index numbers; Feb. 24, 1958, pp. 143-4 for annual averages since 1913.

For More Information . . .

about any item in this department, circle its code number on the

Reader Service

postcard (p. 197)

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... gives most accurate temperature control



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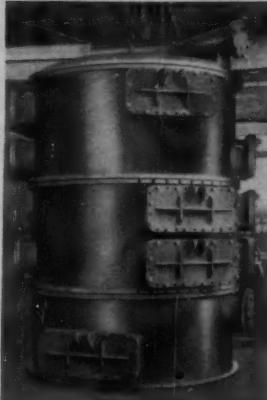
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Mallinckrodt misch metal, an alloy of rare earth metals, does provide magnesium casting alloys with certain qualities particularly applicable to jet engine parts. Misch metal decreases the porosity of the alloy, giving it pressure tightness, and increases its high-temperature creep resistance — the ability to withstand long periods of stress at high temperatures without distortion.

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Remember... you might be better served by Mallinckrodt.

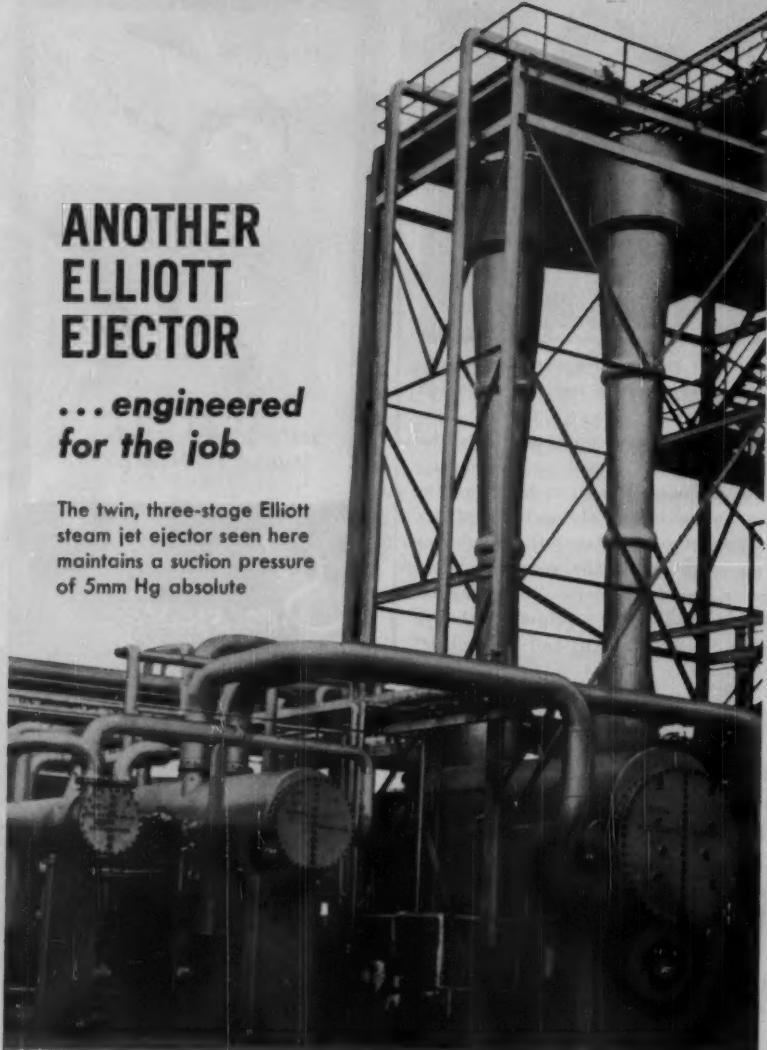
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The twin, three-stage Elliott steam jet ejector seen here maintains a suction pressure of 5mm Hg absolute



designed to serve world's largest crude oil unit

This unique, giant-sized ejector is the largest vacuum installation ever built. The design problem here was to engineer a unit which would efficiently and economically maintain the specific suction pressure required by the application. To accomplish this, Elliott engineers designed a twin-type ejector with two vertical first-stages which are 40 ft long, have 60-inch diameter inlets, and discharge to a 20,000-sq ft intercondenser. The two 20-inch second-stage ejectors discharge to a 6000-sq ft intercondenser and the third-stage ejectors discharge to a 3000-sq ft aftercondenser.

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Available literature on single-stage, multistage and corrosion-resisting types illustrate Elliott's versatility in ejector design and construction for all sorts of

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64-2



TECHNICAL

Comprehensive File

THE PROPERTIES OF GASES AND LIQUIDS. By Robert C. Reid and Thomas K. Sherwood. McGraw-Hill Book Co., New York. 386 pages. \$10.

Reviewed by Lawrence N. Canjar, Department of Chemical Engineering, Carnegie Institute of Technology, Pittsburgh, Pa.

The average engineer, particularly the process engineer, has a file of useful information that he has accumulated over years of practice which serves as his personal reference in estimating physical properties of engineering materials. These are often coveted by the young engineers who are forced to search through countless texts and articles in order to obtain the most recent information on the estimation of a given property for some compound.

Now authors Reid and Sherwood have made such a file available to all process engineers. Not only does this text present the latest and most useful techniques for estimating physical and thermodynamic properties but quite often it discusses the relative merits of one method over another when several are presented.

In general the text is comprehensive in its coverage and complete. However, there are two areas where the authors have condensed their material to a point where the text loses its utility. In the chapter on P-V-T properties, reference is made to the latest generalized correlations but the reader is forced to refer to the original papers for the working charts and tables. There is also virtually nothing offered for the estimation of thermodynamic properties of real gases. Chapter on vapor-liquid equilibrium is complete except for multi-component mixtures.

It is understandable that the text would be lengthened considerably by more extensive

BOOKSHELF

J. B. BACON

coverage of this material. But process engineers will be disappointed to find convergence pressure correlations missing.

For all other properties, particularly the transport properties, the coverage is excellent and manner of presentation is simple and clear. Bibliography of some 480 references is in itself a very useful compilation. Reviewer predicts enthusiastic acceptance of this text by all process engineers and advanced students in chemical engineering.

BRIEFLY NOTED

INSTRUMENT AND CONTROL ENGINEERING—Vocational and Professional Monograph. 46 pp. By Lloyd Slater. Foundation for Instrumentation Education Research, Inc., New York, N. Y. \$1. Describes career opportunities in the field, includes 5-page bibliography.

KNOCKING CHARACTERISTICS OF PURE HYDROCARBONS. 100 pp. American Society for Testing Materials, 1916 Race St., Philadelphia 3, Pa. \$6. Contains data on knock characteristics of a wide variety of hydrocarbons, relates structures and physical characteristics to knock limitations.

NONDESTRUCTIVE TESTS IN THE FIELD OF NUCLEAR ENERGY. 420 pp. American Society for Testing Materials, 1916 Race St., Philadelphia 3, Pa. \$10; \$7.50 to members of sponsoring societies. Proceedings of a symposium held in Chicago, Ill., April 16-18, 1957.

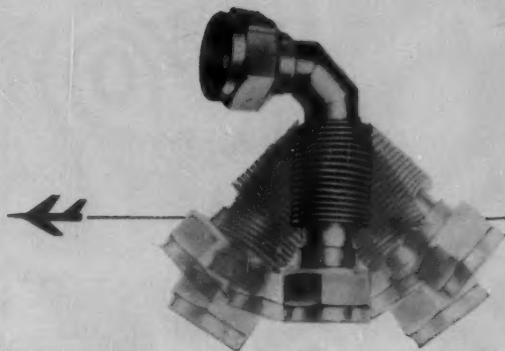
MORE NEW BOOKS

NUCLEAR ENGINEERING HANDBOOK. Edited by Harold Etherington. McGraw-Hill. \$25.

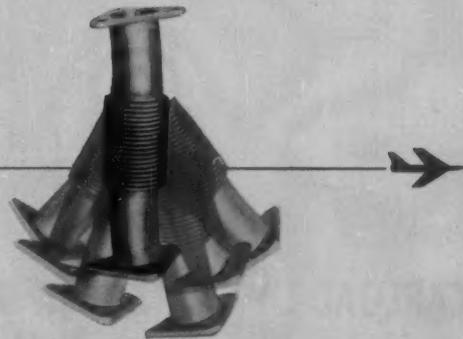
FLUID DYNAMICS AND HEAT TRANSFER. By James G. Knudsen and Donald L. Katz. McGraw-Hill. \$12.50.

ENCYCLOPEDIA OF CHEMISTRY SUPPLEMENT. By George L. Clark and G. G. Hawley. Reinhold. \$10.

NUMERICAL MATHEMATICAL ANALYSIS, 4th ed. By James B. Scarborough. Johns Hopkins. \$6.

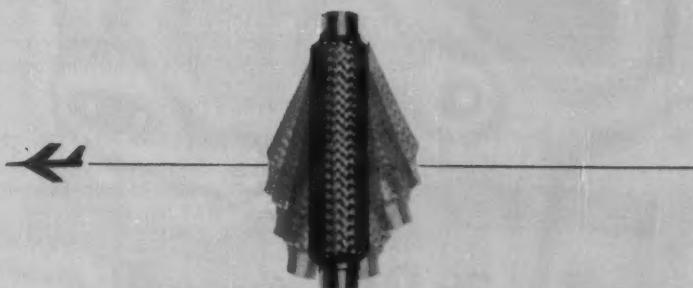


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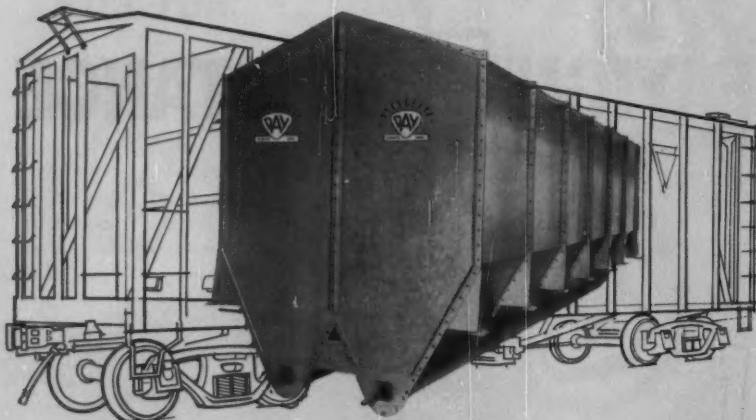
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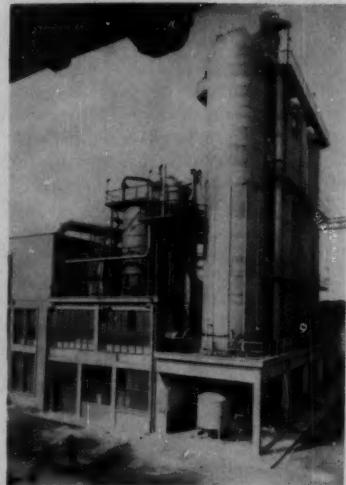
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LETTERS:



No Laughing-Gas Matter

Sir:

On p. 58 of your July 28 issue, I was puzzled by the frequent references to "nitrous" oxide in your review of Kuhlmann's new nitric acid process.

There was no sign of N_2O in the relevant equation; all the evidence indicated that nitric oxide, NO, was being discussed. I believe that the reader should substitute "nitric" for "nitrous" throughout.

A. T. WILLIAMSON
Canadian Industries Ltd.
McMasterville, Que.

► Mr. Williamson is entirely correct. Our editor must have been temporarily under the influence of laughing gas (nitrous oxide).—ED.

Today's Job Market

Sir:

Your Aug. 25 article, "Nationwide Job Pools Place Professionals" (pp. 133-134), whatever may have been its purpose, fails totally to picture the current employment situation among chemical engineers. Your mention of (October 1957) some 7,000 unfilled professional and managerial job openings simply has little meaning today.

Using myself as a typical unemployed job-seeker, I have since

PRO & CON

C. H. CHILTON

May 15 made a total of 257 contacts, including 165 letter-resume applications to possible employers. Total yield to date: two interview invitations, no job offers. This extreme buyers' market in technically trained bodies promises no good for our profession and should not be misrepresented or naively ignored.

Wouldn't it have been more meaningful to have printed more timely, pertinent statistics, with perhaps some analysis and forecast for the future? It would have been in keeping with the remainder of your valuable magazine.

M. A. SHELBENBARGER
Wilmington, Del.

Protect the P.E.!

Sir:

I fear you dealt, if not too harshly, at least too unsympathetically with Ralph J. Winters, who did so nobly protest (*Chem. Eng.*, Aug. 11, p. 186) when you docked the precious appendage "P.E." from the signature of Mr. Malmsten.

Would that your heart, like mine, bled profusely for those who rightly demand titular recognition. It would be far better for you to steal from the tender Sunday school tot the bright gold star he is proudly bearing home to his Mummy.

But let us not be satisfied with mere words. I propose the following compound action to remedy the grievous situation:

- Let Congress quickly pass and let Mr. Eisenhower sign a law inflicting a \$10,000 fine, or ten years in the hoosegow, or both, upon any adult who willfully ignores, in speech or in writing, a title properly bestowed upon the holder by any accredited educational institution or established official body.

- Tattoo the granted title, in suitably embellished letters, upon the forehead of the recipient, so that all who gaze upon him shall immediately be aware of the dignitary they face. (*Continued*)



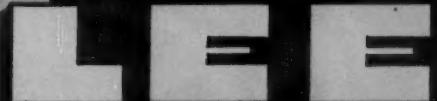
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Two-thirds Jacketed
5 to 500 gal.



Style B Kettle
Full Jacketed
10 to 300 gal.



Style C Kettle
Two-thirds Jacketed
5 to 100 gal.

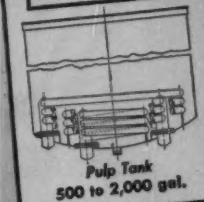


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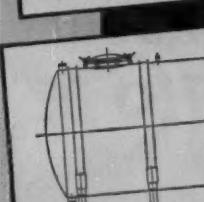
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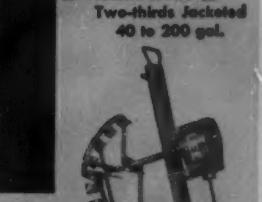
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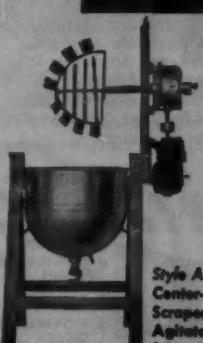


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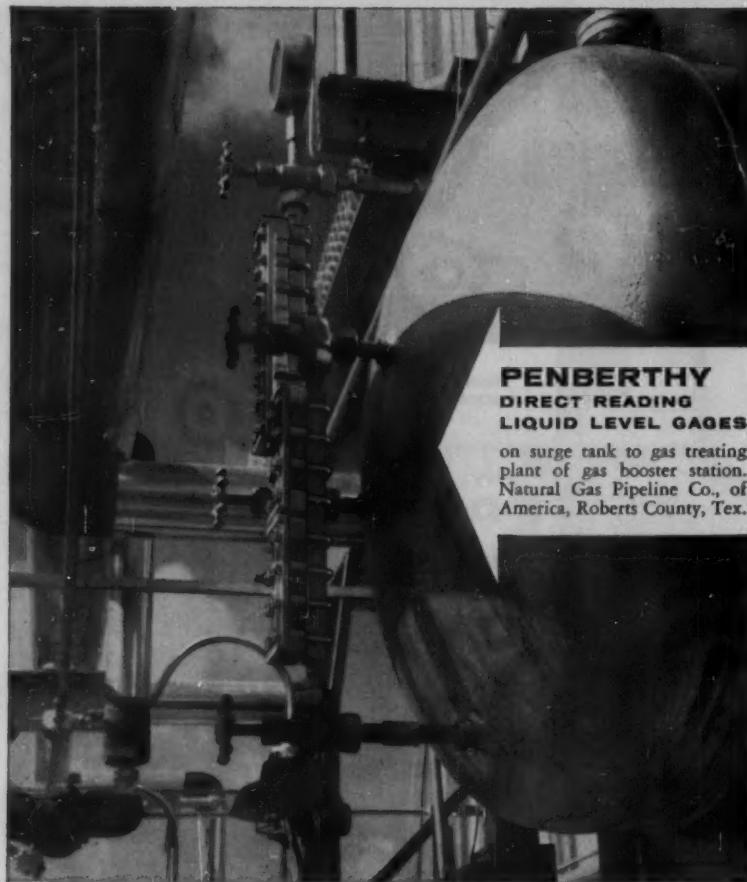
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PRO & CON . . .

• Authorize and require the title-bearer to wear on the seat of his pants a regal purple patch with his title embroidered thereon in letters of gold, so that persons who approach him from the rear shall likewise be aware of the sacred presence.

As an interim measure I suggest starting a Society for the Prevention of Cruelty to Title-Holders (SPCTH), and I trust you will deign to be counted with me among the charter members thereof.

JOHN E. VISCARDI
White Plains, N. Y.



Con: Eternal Secrets

Sir:

In your *Clementator* item, "Court holds trade secrets sacro-sacred" (June 2, p. 43), use of the word "forever" is rather disturbing.

Patents at least have a time limitation. What makes employee contracts so binding?

L. C. CURLEY
Detroit, Mich.

► Key statement in our story was, "The judge's decision apparently established trade secrets as a matter of common law. This means that, even without an employment contract, unauthorized use of trade secrets is just as wrong as misappropriation of money or any other private property."

We took no stand in our news story as to whether or not we agreed with the judge. But the comments we have received from readers indicate that most of them, like Mr. Curley, are disturbed by Judge Christensen's decision.—ED.

(Continued on p. 194)



One of Claymont's multi-torch automatic flame-cutters.

by d'Arcais

Main feature of the Claymont story is integration. For instance, consider one phase of our operation—the new Fabrication Shop. First, steel from Claymont's own open hearth is formed into plate on Claymont's own rolling mills and sent to the Fabrication Shop. Here, modern equipment welds, shears, presses, rolls, cuts or machines the plate to produce fabricated products for many industries.

CLAYMONT FABRICATED STEEL PRODUCTS



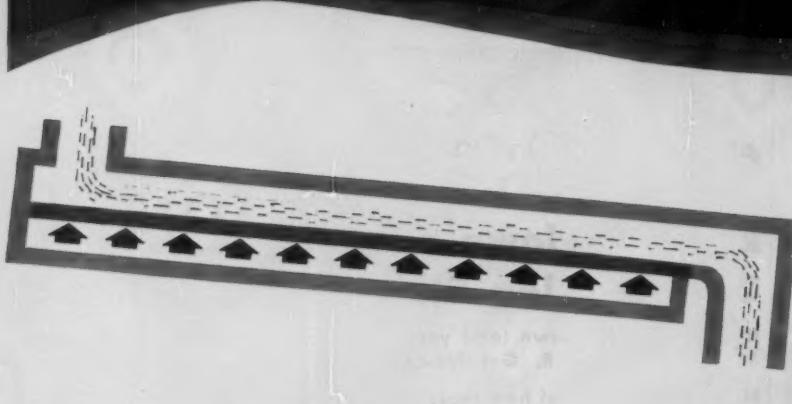
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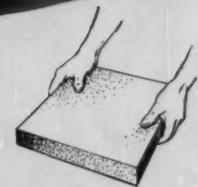
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equipment and com-
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Q. How does AIR-FLOAT work?

A. The dry material to be conveyed is fed on to a smooth, rigid, porous plate through which low pressure air continuously diffuses. Because the conveyor is inclined about 6 to 8°, the aerated material flows by gravity.

Q. What distinguishes the KENNEDY AIR-FLOAT from other air-gravity conveyors?

A. Primarily, the special porous plate. Also the casing is of heavier construction, flanged and channelled for greater rigidity.

Q. How is this special plate better than other porous media?

A. The AIR-FLOAT porous plate has literally millions of tiny pores through which the air diffuses uniformly for thorough aeration of the conveyed material. The plate is thicker, stronger, temperature- and wear-resistant, and has a very smooth surface texture.

Q. How does this improve conveying?

A. AIR-FLOAT has a much higher capacity than competitive air-gravity conveyors. Blind spots are eliminated and the angle of inclination is less critical.

Q. What about maintenance?

A. The KENNEDY AIR-FLOAT is the nearest thing to a completely maintenance-free conveyor that has ever been devised.

Q. Can turns be made?

A. Direction changes up to 45° are made with standard pieces. These can be combined for greater angles.

Q. Are accessories available?

A. Yes. End and side discharge boxes, splitters, control gates, transitions, bin extractors and required blowers can be provided.

Q. Have KENNEDY AIR-FLOAT Conveyors been fully tested and proven?

A. Yes. For more than 12 years AIR-FLOAT Conveyors have been successfully used in KENNEDY-designed cement and lime plants. With this background of experience, KENNEDY is now making AIR-FLOAT available to industry, mass producing it to sell at competitive prices.

For more information on AIR-FLOAT, ask for Bulletin 58-K.



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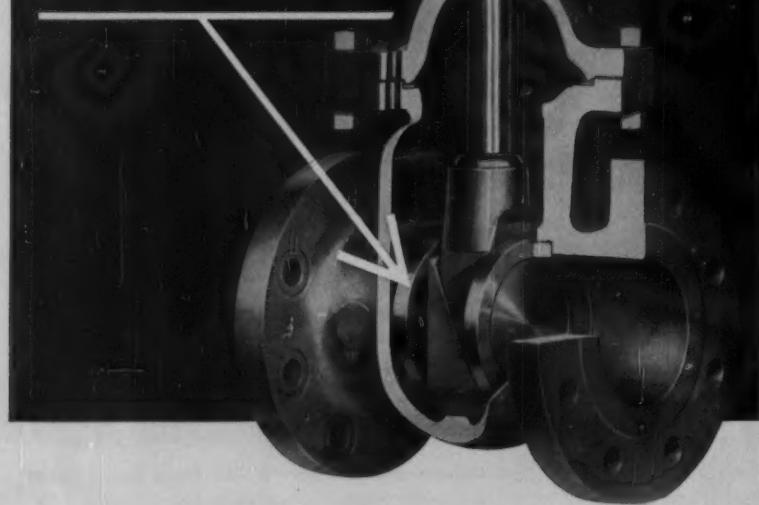
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PRO & CON . . .

Con: Economic Pitfalls

Sir:

In connection with two articles in your July 28 issue, I believe it desirable to warn your readers of limitations in their application.

First, Jelen's article on the use of capitalized cost evaluations (pp. 116-118) omits consideration of profits tax. Because the fictitious capital amount resulting from the capitalization operation may be relatively large, the tax credit on depreciation may be sufficient to reverse completely a decision made without tax consideration.

Second, Lammers' article on the use of continuous compounding (p. 126) should also include a word regarding its application. The variation of $(1+i)^n$ from e^{in} (where n is a discrete integer in the first form as usually employed in finance considerations) can be quite large, even at reasonable values of i and n .

For example, at $n = 10$ years and $i = 20\%$ (which is not a rare combination in profitability comparisons), the discrete form for the factor $(1+i)^n$ has a value of 6.192, whereas e^{in} is 7.389, or an increase of about 19%.

Continuous compounding has certain advantages mathematically in dealing with interest. However, it should be employed with full knowledge of its possible variation from the numbers that management has been trained to think about.

H. E. SCHWEYER
University of Florida
Gainesville, Fla.

Butyl Alcohol Producers

Sir:

In your recent review of the solvents picture (Aug. 11, pp. 90-92) you stated that Carbide was the only producer of normal butyl alcohol during the greater part of last year.

What was Celanese doing all this time?

AL BUTYL
New York, N. Y.

► Celanese Corp. of America informs us it has been in continuous production of synthetic normal butyl alcohol for the past several years. We apologize for our inaccurate and misleading statement.—ED.

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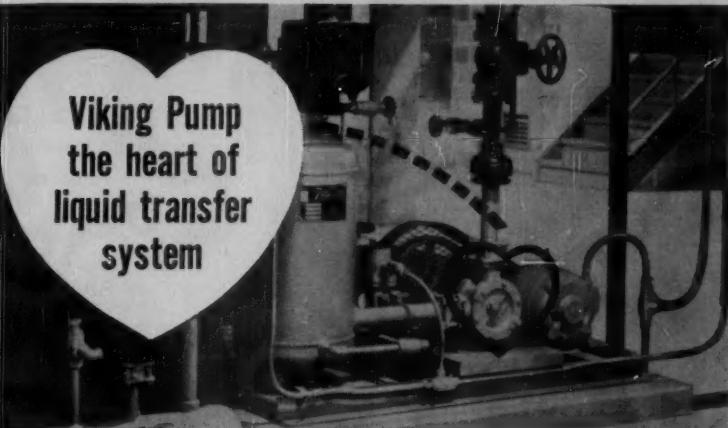
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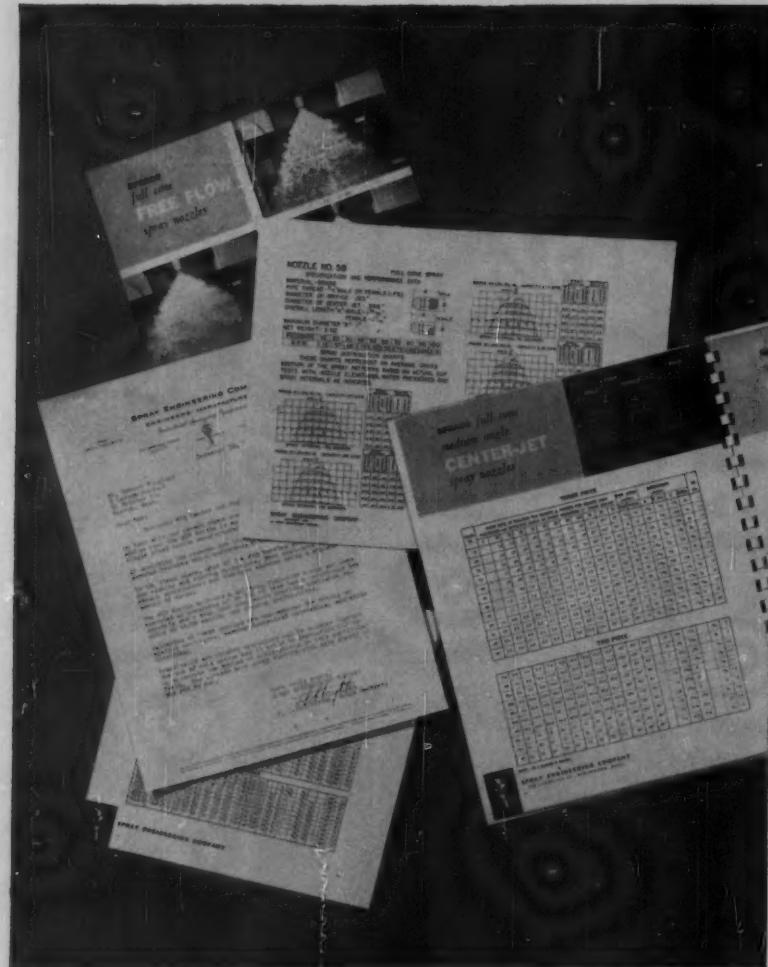
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10-11	38	68A	74B	86	105	128	176A	182F	189d	200B	202d	207B	212	218D						
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189a—Mixing Tank
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189h—Pressure Kettle

189i—Style CW Kettle—two-thirds jacketed
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202c—Top-Entering Mixers
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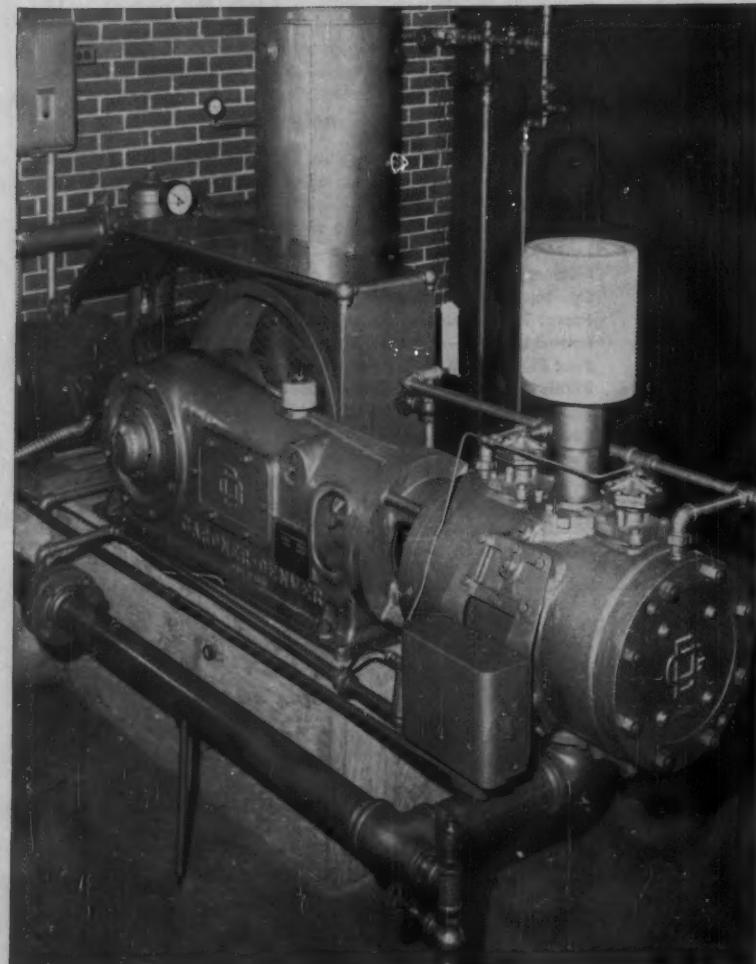


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42 *Hooker Chemical Corporation

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202A Water Consultants

Construction Materials

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69 *Aluminum Co. of America

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46-47 Reynolds Metals Co.

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202B Minnesota Mining & Mfg. Co.

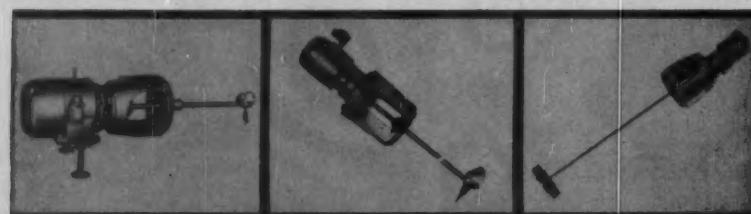
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88 *Eagle-Picher Co.

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R205 *Federated Metals Div. of Asarco

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2. Indiana Arsenal, Charlestown, Ind.
3. Jefferson Proving Ground, Madison, Ind.
4. Lima Ordnance Steel Foundry, Lima, Ohio
5. Marshall Plant, New Martinsville, W. Va.
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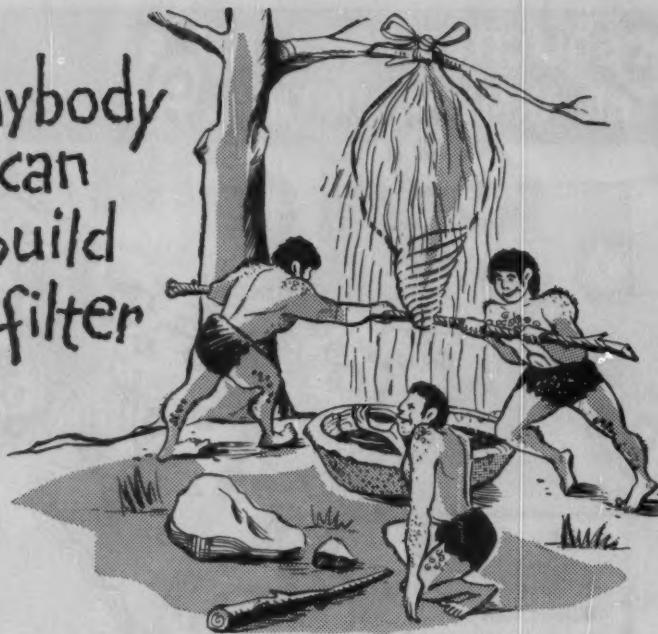
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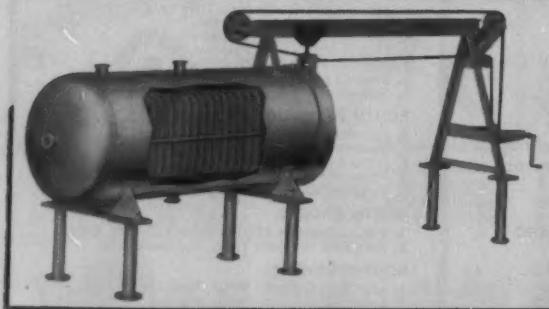
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22-23 *E. I. du Pont de Nemours & Co.

Titanium . . . available now for sound high-quality castings which are resistant to many corrosive environments. Booklet gives properties & applications of titanium.

8-9 *E. I. du Pont

Wire Cloth . . . is available in all standard widths, all meshes, all commercial metals . . . a complete line even up to 400 mesh cloth. Answers to any problems.

176 *Newark Wire Cloth Co.

Electrical & Mechanical

Bonded Pistons . . . on pneumatic vibrators bring you lower precipitator maintenance & operating costs. Complete information on the "K-30" is available.

67 *Koppers Company, Inc.

Cutters, Knife . . . Bulletin App. 216 gives details on designs, sizes and speeds of the 700 series. Main bearings are available in different types.

204D Taylor, Stiles & Co.

Governor . . . Bulletin 1047 describes the SLDG governor designed especially for steam-driven reciprocating pumps or for pumps driven by steam turbines.

204E Blaw-Knox

Gyrol Fluid Drive . . . answers virtually every power-transmission need involving adjustable-speed drive. Complete details on type VS, Class 2 & other types is offered.

78 *Amer. Standard, Amer. Blower Div.

Lubrication System . . . An exclusive feature of these motors is Lubriflush. Old grease is completely flushed out as new grease is forced in. Full information in bulletin.

41 *U. S. Electrical Motors Inc.

* From advertisement, this issue

New Improved JERGUSON Gage Illuminator

gives up to
3 times the
illumination

Low cost explosion-proof
lighting of entire gage
glass with no glare or
blind spots

New Features:

Simplified Relamping . . .
loosen one thumb screw
to lift out cover and
glass housing in one
piece.

New Safety Chain pre-
vents accidental drop-
ping.

Now both UL and CSA
Approved.



Easily mounted on back
of Transparent Gage.

The New Jerguson EPL-56 Illuminator gives three times the illumination (and 3 times the bulb life) . . . a bright, evenly diffused light over the entire length of gage glass, thus enabling you to see the liquid level clearly and easily under all conditions. Relamping is simplified: one turn of the thumb screw and you lift out cover and glass housing in one piece.

Jerguson Illuminators incorporate the principle of solid wedge lighting. Illumination from a single bulb is reflected from the angular surface of the plastic wedge and is evenly diffused through the transparent gage glass.

Jerguson Illuminators are UL approved and are built in accordance with their Standard for Electric Lighting Fixtures for use in hazardous locations for Class I, Group D Services. They are made in a variety of sizes.

Write for Data Unit on Process Gage
Illuminators.

(See Both 631—Power Show)

JERGUSON

Gages and Valves for the
Observation of Liquids and Levels

JERGUSON GAGE & VALVE COMPANY
100 Adams Street, Burlington, Mass.

Offices in Major Cities

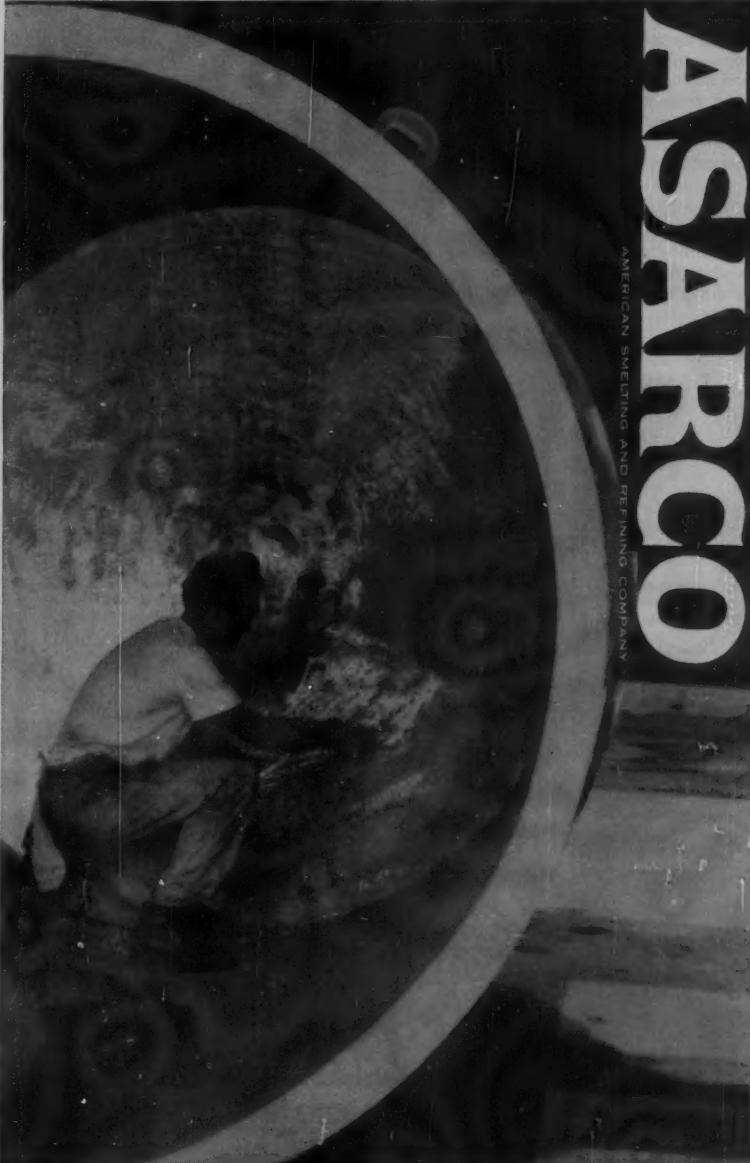
Jerguson Tress Gage & Valve Co., Ltd., London, Eng.
Pétrole Service, Paris, France

Federated Lead Fights Corrosion! Federated lead is one of the most efficient and economical protection materials against many acids. Lead is self-healing. Scratch it and a protective coating re-forms immediately. Lead is easy to work and moderately priced. Federated produces chemical lead in sheets to your requirements. Pipe, bends, traps and standard fittings available from stock. Special forms fabricated to order. Call the Federated Sales Office near you. Or write for Bulletin No. 162, the Lead Handbook for the Chemical Process Industries. Federated Metals Division, 120 Broadway, New York 5. In Canada: Federated Metals Canada, Ltd., Toronto and Montreal.

FEDERATED METALS DIVISION OF

ASARCO

AMERICAN SMELTING AND REFINING COMPANY



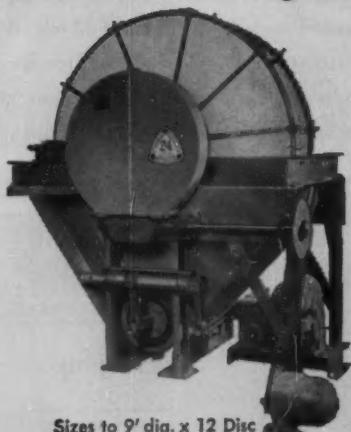
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Exclusive diaphragm-activated agitating mechanism supplies proper pulp agitation. No packing glands, no submerged bearings, no possible contamination from grease or dilution from sealing water. Gives higher filter capacity, lower moisture content and more uniform, dryer filter cake—plus trouble-free, dependable operation.

DENVER Disc Filters without agitator mechanism, DENVERP. Packaged Filter Units and complete dewatering equipment also available. Laboratory Filtering Test Service at no charge.



Sizes to 9' dia. x 12 Disc
Write for Bulletin No. F9-B5

DENVER Equipment for the Chemical Process Industries



DENVER Adjustable Stroke Diaphragm Pumps
1" to 10" Simplex and Duplex, Capacity to 1000 g.p.m.



DENVER Spiral Rake Thickeners
Sizes to 150' diameter
Write for Bulletin No. T5-B5



DENVER Drum Filters
Sizes to 6' dia. x 8' long.
Write for Bulletin No. FG-B1



DENVER Dryers
Sizes to 8' x 60' and larger
Write for Bulletin No. D4-B4



DENVER Steel Head Mills
Sizes to 10' dia. x 20' long
Write for Bulletin No. B2-B20



DENVER Automatic Samplers
8" to 120" Cutter Travel
Write for Bulletin No. S1-B4

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thermometer test wells
thermocouple wells

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Every well is carefully made to assure a plus service. Selected bar stock is machined to within accurate limits. Bore concentricity is held within 5% of wall thickness, depending on well length. They are tested to withstand pressures up to 3000 psi., depending on the wall thickness. Exterior surface has a mirror-like finish for minimum resistance to flow in lines.

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Give SERV-RITE a trial on your next drilled well requirements. There is none better.

Write for Bulletin No. 2000
for specifications, size, and ordering information on SERV-RITE drilled wells.

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LITERATURE . . .

Microwave Oscillator.....A new tool for applications in microwave spectroscopy aids detection of free radicals atomic analysis and measurement of dipole moments.
207A Laboratory For Electronics

Motors.....New illustrated booklet gives design & special features of chemical, explosion proof & totally enclosed fan cooled motors. All 3 available in frame sizes 56 thru 680.
207B *Marathon Electric Co.

Motors & Generators.....specially built for all atmospheric & hazardous conditions in chemical plants. Bulletin SB-185 gives complete factual information.
34 *Marathon Electric Mfg. Corp.

Motors, Open.....Super-Seal is completely unaffected by moisture, dust, dirt, oil, acids & alkalis. Information available on this & the Silco-Flex.
55 *Allis-Chalmers

Starters, Motor.....eliminates any possibility of heater misalignment. Bulletin SM-275 gives complete story on starters with one-piece thermal overload relays.
101 *Square D Company

Handling & Packaging

Air Hoists.....This fire-safe air hoist easily handles loaded filter plates. Also, provide easily controlled speed for a swift, steady lift. Bul. 80.
201 *Gardner-Denver Co.

Blending Scale.....A blending scale for free-running materials automatically receives, weighs and records granular materials of up to $\frac{1}{4}$ in. diameter.
207C Richardson Scale Co.

Conveyor Components.....Recently introduced screw conveyor components reduce power demands and maintenance delays. They include conveyor screws, hangers, etc.
Folder 2489.
12 *Link-Belt Co.

Conveyor Elevators.....Brochure shows sanitary construction features including cantilever design. Also illustrates buckets, pulleys. Dimensions and capacities.
207D Bucket Elevator Co.

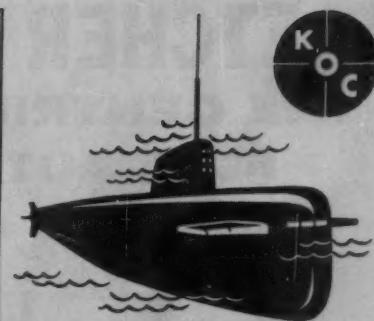
Conveyors, High Temperature.....feature heavy conveying troughs, replaceable trough sections & heat protected drive. Full information is available.
103 Carrier Conveyor Corp.

Containers, Chemical.....Stainless steel acid containers that build a safe, compact stack. Low tare weight reduces transportation costs. Hackney Drum & Barrel Catalog offered.
13 *Pressed Steel Tank Co.

Elevator, Vertical Screw.....The Rotor-Lift elevates & conveys bulk chemicals. Handles capacities up to 6,000 cu. ft. per hr. Engineering catalog is available.
R218 *Southwestern Supply & Machine

Loading Arm, Barge.....saves on line handling injuries, dock clutter, lengthy hookup time, hose bursts & replacement costs. Illustrated literature available.
111 *Chiksan Co.

* From advertisement, this issue



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During her history-making voyage under the Polar icecap, the Nautilus, like all other submarines in the atomic fleet, carried two periscopes designed and manufactured by Kollmorgen. The high degree of optical and mechanical skill required to produce these periscopes can be drawn on to solve your remote viewing and inspection problems. For literature, write Department 140

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LITERATURE . . .

Portable Bag Closer Requires no installation, supports or plant space. Handles textile & paper bags. Complete Catalog File of bag-closing equipment offered.

208A *Dave Fischbein Co.*

Tanks in vertical & horizontal styles for a wide range of applications. Bul. 574 contains 12-pages of specifications plus facts about weather-proof tanks.

188 **The Day Co.*

Heating & Cooling

Boilers available in 19 sizes, 130 models, 15 to 600 hp . . . steam or hot water, gas, oil, or combination oil/gas fired. Facts on the self-contained boiler offered.

170 **Cleaver-Brooks Co.*

Generators, Steam features controlled circulation & balanced feed, a principle of using a continuous single pass tube. Produces steam in 3 minutes, from a cold start.

184 **Clayton Mfg. Co.*

Heat Exchanger Paracoll self-cleaning eliminates need to stop processing for cleaning purposes. Gives process plants increased and better heat transfer. Bul. 1000.

R229 **Davis Engineering Corp.*

Heat Exchangers The Cross-Bore is immune to thermal shock, accommodates working pressures to 200 psi at temp. to 340 F., & available in 14 standard capacities. Bulletin.

172 **Falls Industries Inc.*

Heat Exchanger Heat is removed from your process at the rate of input, giving precisely the temperature you require & assuring quality of product. Bul. 132.

TL185 **Niagara Blower Co.*

Packaged Firing Units Capacities of standard units range from 200 to 830 boiler horsepower. Details, specifications, illustrations & dimensions in Bul. 28.

R219 **National Airoil Burner Co.*

Preheater For details on air pre-heaters and information on potential fuel economy, a factual article is available. Slagging is reduced & cuts boiler downtime.

37 **The Air Preheater Corp.*

Vaporizers both packaged & field erected, can be outfitted for heating with oil, gas, waste heat or special fuel in outdoor & indoor installations. Bul. "DV".

212 **Union Iron Works*

Instruments & Controls

Chromatograph, Gas Instrument for monitoring multiple components in a complex process stream. Detailed instrument specifications in data file P-1-14.

61 **Beckman Instruments, Inc.*

Computers, Electronic LGP-30 is easy to operate, plugs into any regular wall outlet and is completely mobile. Detailed information & specifications offered.

94 **Royal McBee Corp.*

* From advertisement, this issue

PUMPS

of NICKEL, MONEL
or CHROME-NICKEL
ALLOYS but only for the
WETTED END
write TABER



Because at Taber, your PUMP NEEDS will receive the personal attention of highly specialized pump engineers .. your objectives are most likely to be realized. Many of the oldest, largest and most respected producers in the chemical industry have and are using both Taber service and pumps.

NOTE, the vertical design pump permits locating stuffing box above and out of liquid level .. nothing to leak. Horizontal Pumps, write for Bulletin C-355. Vertical, Bulletin V-837.

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LITERATURE . . .

Computer, Liquid Horizontal tank content indicator is offered. It insures accurate inventories & helps you plan more efficient & economical storage.
105 *Modern Welding Co.

Controls Self-powered automatic temperature regulators have special advantages such as no compressed air or electrical wiring required. A 10-page bulletin gives details.
42B *Saro Company, Inc.

Controls, Liquid Meters & accessories offer complete systems for every type of liquid control. Complete information illustrating the types of systems is offered.
71 Bowser, Inc.

Controller Pyr-O-Volt is an accurate instrument for reliable stepless control of saturable reactors, r.f. generators and other power amplifiers. Details available.
16-17 Minneapolis-Honeywell

Gages available in a variety of materials & special designs, to meet all practical requirements for measuring & observing liquids. Complete line in Catalog 36.
190 Penberthy Mfg. Co.

Gage Illuminator The new EPL-56 model gives 3 times the illumination & 3 times the bulb life. Data Unit on process gage illuminators is offered.
L205 *Jerguson Gage & Valve Co.

Instruments Pneumatic, electronic, miniature telemeters & recording gauges... all in a planned line. Technical data is offered on the miniature instruments.
10-11 *Bristol Company

Instruments, Control Choose from four controller types ... that include magnetic modulation. Get the facts on their proved performance & installation.
180 Barber-Colman Co.

Meters, Liquid Designs to measure most anything that flows... including all stainless steel meters for corrosive liquids. Full details on meters & accessories.
87 Rockwell Mfg. Co.

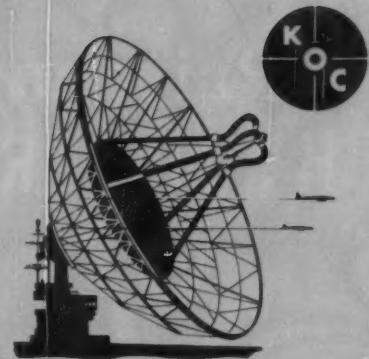
Meter Tubes New 20-page catalog details features and specifications of flow-measurement meter tubes. Also specifications on manufacturer's orifice flange.
209A Daniel Orifice Fitting

Miniature Instruments Publication 1275 describe the specifications for the manufacturer's line of plastic-door miniature recorders and controllers.
209B Fischer & Porter

Recorder Transcope plug-in provides a complete cascade system. Gives continuous 30 day record. The unique set point transmitter allows continuous control.
30-31 *Taylor Instrument Co.

Thermometers Bimetal thermometers feature a dampening bearing above the bimetal element that makes them extra resistant to shock & vibration.
92a Rochester Mfg. Co.

Timing Systems Brochure depicts manufacturer's products, facilities and staff capabilities. Products for observing and recording reactions and events accurately.
209C Edgerton, Gereshausen, Grier



fire control

Where hit or miss means life or death, Kollmorgen fire control devices put the projectile on target and keep it there. Combining optical, mechanical and electronic skills, these devices demonstrate the type of highly precise instrumentation work Kollmorgen is prepared to do for you. For literature on fire control write to Department 140

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author

TALITARIAN. — *n.* One who *talitari-ism* (tāl-thōr'ē-tār'ē-izm) from, authority; entitled to or *thoritari* fire teachings. 2. *Ha-
peremphory*. — *au-thor'i-ta-tiv* *au-thor'i-ta-ty* (ō-thōr'ē-tē-tē), *n.*; *p-
auctoritas*, *l.* Legal or high

Chemical Engineering

HAS MORE ENGINEERS *hand*; — *pledged to*, in support of opinion

ON ITS *only*; witness. *b* A pre-

PUBLISHING STAFF *hand*; or its author. *d* Just

THAN ALL OTHER *like*. — *Syn.*

CHEMICAL PROCESS *•* *industries* (ō-thōr'ēs), *v.t.* *1* *commission*; as, *autho-*

TECHNICAL PUBLICATIONS *act*.

PUT TOGETHER *und for*. — *au-thor-i-ized* (ō-thōr'ē-izd), *adj.* *2* *au-thor-i-ty*. *b* *Sanctioned* or *ap-*

Chemical Engineering

ABC McGraw-Hill Building, **ABP**
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Published every other Monday for
Chemical Engineers in all functions

* From advertisement, this issue

Pritchard HYDRYERS

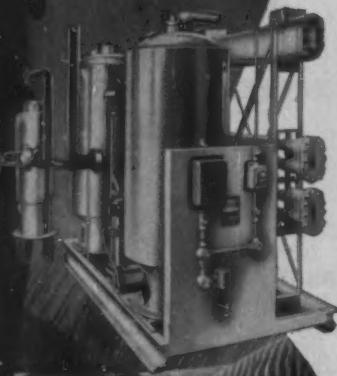
*do the work
of field-built
gas dryers
at a fraction
of the cost*

Why pay a premium for a field-built air and gas dryer when the factory-built Pritchard Hydryer does the same job for less? Factory fabrication, moreover, means greater quality control, convenient ordering, faster delivery.

Pritchard Hydryers are ideal for drying synthesis gas, instrument air and many other compressed gases.

They reduce dew points to -40°F . or lower, preventing corrosion, icing, line losses and flow stoppages. They have been successfully used by E. I. duPont, Dow, Liquid Carbonic, Monsanto, and many other leading companies in the chemical industry.

If you would like full details on the functions and exclusive features of Pritchard Hydryers, mail the coupon for your copy of the interesting bulletin illustrated below.



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Please send Hydryer Bulletin 16.0.061

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Firm _____

Address _____

City _____ Zone _____ State _____



LITERATURE . . .

Pipe, Fittings, Valves

Bellows, Stainless Steel for toughest airborne applications. In single or multiple ply, in a wide range of sizes & shapes, including braid covered types. Bul. TC-1400.
187 *Robertshaw-Fulton Controls.

Compensators high - pressure, heavy-duty expansion compensators cost much less per inch of stroke than any other method of absorbing pipe. Design & cost data offered.
182 *Flexonics Corp.

Fittings The low carbon C-1025 steel insures optimum weldability & strength. Information about 1025 steel & your commercial forging requirements is offered.
214 *H. K. Porter Co., Inc.

Fittings Usco Weld features fast, easy assembly, automatic alignment of pipe & fittings & strong joint interference. Details available on Usco Weld & plastic pipe & fittings.
163 *U. S. Rubber

Fittings, Welding any type of special fittings made from plate to the most rigid specification. Closer tolerances & quality control. Bul. 5801 for details.
89 *Midwest Piping Co.

Joints, Expansion circular or toroidal expansion joint provides lower operating stress & is suitable for use at high temperature. Data is available.
37 *Zallea Brothers

Nozzles Lightweight, precision built steel spray nozzles feed just the right amount of fuel into combustion chamber. Complete information is available.
196 *Spray Engineering Co.

Packings Teflon packings last longer under corrosive conditions. Ideal for sealing pump & other rotating shafts against acid, caustics, aromatics, etc. Bul. CP552.
1215 *Chemical & Power Products, Inc.

Packings Lattice-Braid Teflon packings provide tight seal up to 100 psi pressure. Folder AD-131 gives details on 2000 different styles of packings, gaskets & seals.
14-15 *The Garlock Packing Co.

Pipe Flexipipe connectors come in convenient sizes & are sold by leading distributors. Detailed information on service application & samples are available.
159 *The American Brass Co.

Pipe Bulletin TS-1A gives complete details on fluoroflex-T pipe. It resists corrosion, and can handle hydrofluoric acid with complete safety & no maintenance problems.
107 *Resistoflex Corp.

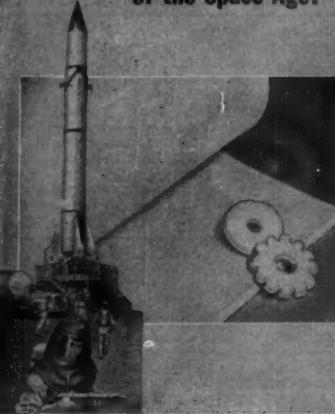
Pipe, Polyvinyl for a variety of uses in the chemical industry. Resistant to many chemicals, including acids, alkalies, salt solutions & alcohol. Bul. 24.
112 *U. S. Steel, National Tube Div.

Pipe, Saran-lined fittings, valves and pumps are available for systems operating from vacuum to 300 psi. & from well below zero of 200°F . Complete details on request.
95 *Dow Chemical Co.

* From advertisement, this issue

SYNTHETIC-FIBER FEUTRON FELTS

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1. Du Pont polyester fiber trademark.
2. Du Pont acrylic fiber trademark.
3. Carbide & Carbon Chemicals Co. acrylic fiber trademark.
4. Allis-Chalmers Corp. triacetate fiber trademark.
5. Chemstrand Corp. acrylic fiber trademark.

LITERATURE . . .

Tees lined with pure, white Teflon, $\frac{1}{8}$ " thick. Lining has no welds. Solve corrosion & contamination problems. Details outlined in Bulletin K-57-A.
28 *John L. Dore Co.

Tubing send for a copy of the new Trent 48-page tubing handbook. Gives details on applications, special features and uniformity of this tubing.
80 *Trent Tube Co.

Tubing, Stainless Complete data on the many analyses of welded stainless tubing & pipe is outlined in Bulletin T. D. 120. Features corrosion control.
104 *Carpenter Steel Company

Tubing, Polyethylene Special types of cabled instrument tubing to meet specific needs. Bulletin 458-H.
BL213

*Crescent Insulated Wire & Cable Co.

Unions, Tri-Lug Model 603A offers strength, interchangeability & corrosion-resistance. Complete information and prices on these unions is available.
125 *Rockwood Sprinkler Co.

Valves Alloy construction gives ease of operation & low maintenance. Folder, "Valves & Fittings in the Pulp & Paper Industry" gives details on the complete line.
114 *Cooper Alloy Corp.

Valves Cupola back pressure valve is also adapted to air lines in industrial plants where weight is a factor. Installation, sizes etc. in detail... see Bulletin 10000.
211A Norwalk Valve Company

Valves Nine new flanged and forged steel Gate, Globe & Check valves are available. Literature on sizes, pressures and types of the complete line is offered.
128 *Henry Vogt Machine Co.

Valves, Control Super 70 diaphragm valves are available in either clamp ring, float ring, sealed bonnet or flanged-gasketed body closures. Information offered.
79 *Black, Sivals & Bryson, Inc.

Valves, Diaphragm Horizontal & vertical types provide positive check against reverse flow of gas or air. Complete data contained in Bulletin 2000.
211B Norwalk Valve Co.

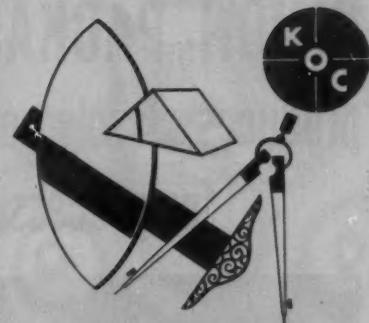
Valves, Drain cannot clog up. Designed so that in the closed position the piston or ram extends up into the tank. In open position, full flow assured. Catalog.
R183 *Strahman Valves, Inc.

Valves & Fittings, PVC are designed to regulate the flow of alkalies, acids, & similar corrosive fluids. Booklet describes mechanical & thermal properties, sizes, etc.
169 *Walworth

Valves, Gate Exceptional performance, longer valve life, less maintenance and easier operation. Get all the details on types & sizes in catalog 57.
194 *Darling Valve & Mfg. Co.

Valves, Needle for finer regulation of water, oil or gas. Offers a maximum working pressure of 10,000 PSI. New catalog gives complete details.
TL213 *Marsh Instruments Co.

* From advertisement, this issue



from ideas to instruments

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Men on the Move

Now available
in a new edition...
with new figures.

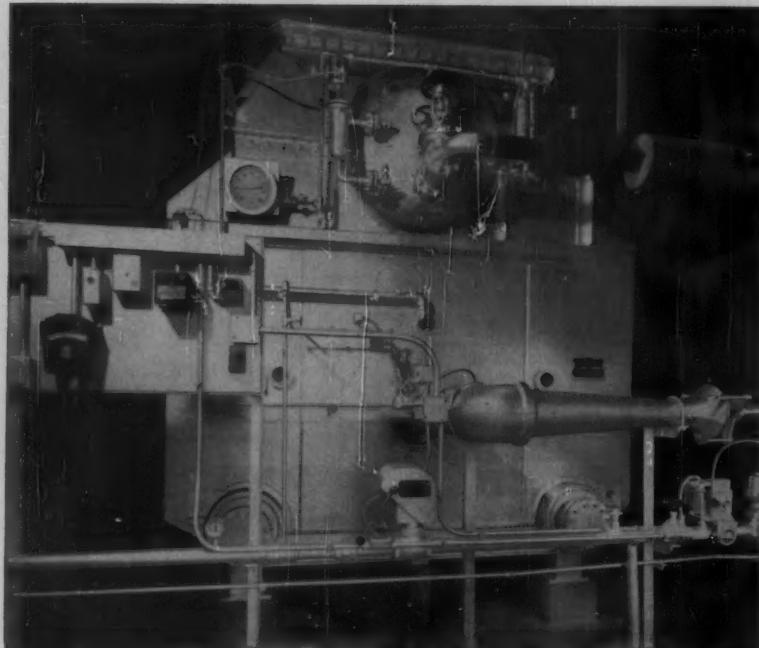
This popular booklet points up the important sales problem of personnel turnover in industry. Out of every 1,000 key men (over a 12-month period) 343 new faces appear . . . 65 change titles . . . 157 shift . . . and 435 stay put. These figures are based on average mailing address changes on a list of over a million paid subscribers to McGraw-Hill magazines.

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UNION PACKAGED VAPORIZER

produces closely controlled temperatures for processing Wesson Oil



Delivering accurately controlled vapor temperatures at low pressures, Union Type MH Vaporizers play an important role in the food and chemical processing industries. The unit shown is used in deodorizing vegetable fats and oils at the South Texas Cotton Oil Co., a subsidiary of Wesson Oil & Snowdrift Co., Inc. Shipped as a package completely shop-assembled, piped and wired with controls mounted, it produces 4 million BTU/hr. at 600°F and 31 psig, and has a rated capacity of 4½ million BTU/hr.

"Very satisfactory" operation is reported by this Wesson Oil subsidiary. Similar MH results have been achieved by numerous other companies in the process industry. Dependable, efficient performance and sensitive temperature control at all times are assured by the

compact, divided tube bank design, straight-through gas flow, and maximum heating surface per BTU.

Both packaged and field erected Union Vaporizers can be outfitted for heating with oil, gas, waste heat or special fuel in outdoor and indoor installations. Union also produces a complete line of Process Heating Equipment for use with Dowtherm "A" and "E", Para-Cymene, Anisole, Aroclor #1248 and Heat Transfer Oil, either convection or forced circulation.

COMPLETE DETAILS

are covered in
Union Bulletin
"DV". Write
for your copy.



UNION

IRON WORKS

Erie, Pennsylvania

LITERATURE . . .

Valves, Safety Relief features the Eductor Tube which efficiently removes pressure from the closed bonnet. Complete details contained in Catalog 1900.
96 *Manning, Maxwell & Moore, Inc.

Valves, Stainless Steel designed for viscous liquids & other fluids difficult to move at room temperature. Other designs for specific applications.
117 *Alloy Steel Products Co.

Process Equipment

Agitators, Portable Nettco drip-proof construction prevents oil-in-mix contamination. Available in high speed & medium speed, 1/6 to ½ HP. Bul. 581.

228 *New England Tank & Tower Co.

Blenders Rotary blenders start 4-way blending while charging, continue it during discharge, thus producing highly intimate, even blends of dry & semi-dry materials.

1218 *Sturtevant Mill Co.

Catalytic Purifier is combined with an automatically operated drying unit to provide oxygen-free hydrogen that is ideally pure & dry. Descriptive literature offered.

99 *Engelhard Industries, Inc.

Centrifugal The Tornado is fully automatic, gives you 24-hr. production. Also available in manual & semi-automatic models. Detailed information offered.

208 *The New Fletcher Works, Inc.

Centrifugals Catalog CE-58 gives complete information on size, type and capacities of "Ter Meer" centrifugals. Designs for every process in the chemical industry.

115 *Baker Perkins, Inc.

Centrifugals Reineveld automatic centrifuges used for dewatering & washing of crystalline solids & for separation & clarification of fine amorphous slurries. Bul. 356.

TL195 *Heyl & Patterson, Inc.

Centrifugal Process for continuous acidulation process for tall oil production. Detailed information on this process is available, plus ways of producing quality product.

6-7 *The De Laval Separator Co.

Conveyor Dryer offers increased drying capacity per square foot of surface, easier apron cleaning, & improved uniformity of dried product. Literature available.

124 *National Drying Mach. Co.

Cooling Towers If water conservation is in your development plans, you will find it profitable to investigate Marlite Bulletin M-58. Installation is Fungus-Proof.

97 *The Marley Company

Crystallizers assure you operating advantages that include: lower centrifuging costs, less processing, dust elimination, minimum caking etc.

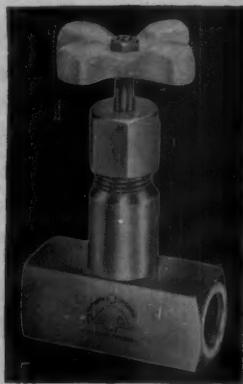
Bul. CE-57.

39 *Struthers Wells Corp.

Dryer, Air remove unwanted moisture from compressed air. End freezups, corrosion & clogging due to water in the air lines. Complete information in Bul. 223B.

91 *Pittsburgh Lectrodryer Div.

* From advertisement, this issue

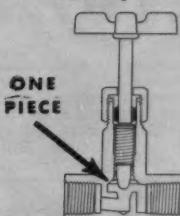


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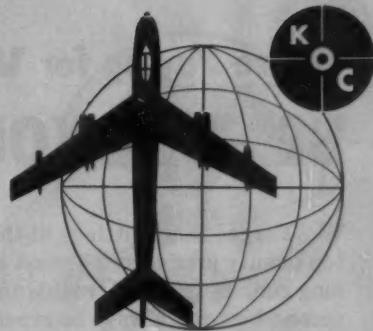
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BULLETIN

TALITARIAN. — *n.* One who **tar'ti-an-ism** (*tär-thör'ē-tär'ē-tän*) **au-thor'i-ta'tive** (*tō-thör'ē-tä-tī-tiv*) from, authority; entitled to ob*th*eritative teachings. 2. *n.* **peremptory**. — *au-thor'i-ta'tiv* (*tō-thör'ē-tī-tiv*), *n.*; *v.* *au-thor'itatis* 1. *legal or righ* **Chemical Engineering** (*khem'ikl īng'ē-nērē*) *son*, *in* *particular field*; *as*, *the* *first* *in* **HAS MORE ENGINEERS** (*hāz mōr īng'ē-nērēz*) *hand*; *—* *used* *to*, *in* *support* *of* *opini* **ON ITS** (*ōn īts*) *on*; *witness*. *3. A* *pre* **PUBLISHING STAFF** (*pūb'lishing* *stāf*) *part* *of* *an* *influence* *of* *than* *all* *other* (*thān* *āl* *ōthrē*) *like*. — *syn*. **CHEMICAL PROCESS INDUSTRIES** (*khem'ikl prōsēs* *indūstēz*), *v. t.* 1. *to* *commission*; *as* *autho* **TECHNICAL PUBLICATIONS** (*tek'nikal* *pübl'kāshən*) *recognition*; *as*, *customs* **PUT TOGETHER** (*püt tō'gē-thər*) *and* *for*. — *au'th* *uthor-ized* (*ō'þor'īzēd*), *adj.* *2. Sanctioned* *or* *appro*

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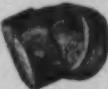
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171 *General Amer. Trans. Corp.

Dryers Hydryers are ideal for drying synthesis gas, instrument air & many other compressed gases. Illustrated bulletin details the functions & exclusive features.
210 *J. F. Pritchard & Co.

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181 *F. J. Stokes Corp.

Dust Collection Systems Booklet, "The Collection & Recovery of Industrial Dusts," gives information on Cyclone, "SF" Electric Precipitator & Precipitator-Cyclone.
216 *Buell Engineering Co.

Dust Collectors Miniature cyclone tubes, cast of white iron, provide ultra-hard, cling-free, self-cleaning surface for maximum material recovery. Bul. D-584.
TL183 *Dustex Corp.

Dust Controls An efficient dust collecting system, scientifically planned, designed & constructed. Cloth filters bag collectors offer maximum efficiency. Bul. 922.
85 *Pangborn Corp.

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186 *Elliott Company

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BL183 *Prater Pulverizer Co.

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93 *American Machine & Metals.

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1 *Commercial Filters Corp.

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214A Komline-Sanderson Engr. Corp.

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226 *Brown Company

Filter, Gas removes all fine dust & scale from gas. Composed of removable filter material in tricurled hair or spun glass wool. Bulletin 9200 for details.
214B *Norwalk Valve Co.

* From advertisement, this issue

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Filters, Water . . . Where high quality process water is needed, diatomite filters provide an effluent second only to distilled water. Bul. 651 & Bul. 900 give details.

178 *R. P. Adams Co., Inc.

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215A Graver Water Conditioning

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116 *Nordberg Mfg. Co.

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202a *Eastern Industries, Inc.

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232 *Mixing Equipment Co.

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126 *National Engineering Co.

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175 *Philadelphia Gear Corp.

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81 *Read Standard

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168 International Engineering, Inc.

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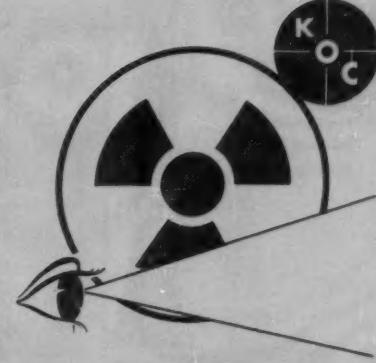
4 *Bird Machine Co.

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177 *The J. H. Day Co.

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215C Hendrick Mfg. Co.



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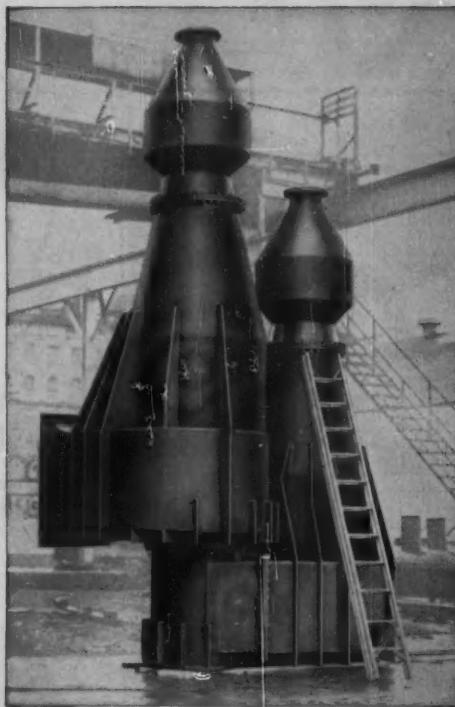


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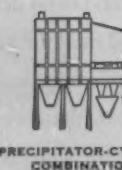


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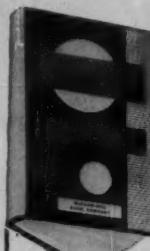
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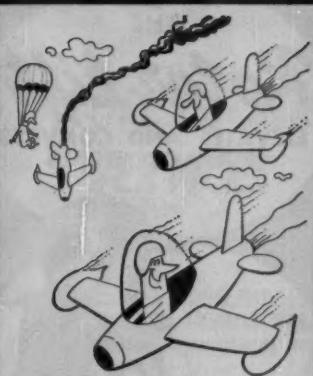
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Compressors . . . Electric-Driven, Steam-Driven, Gas-Engine compressors and Centrifugal compressors are available. Form 3132A gives information on process compressors. 49 *Ingersoll-Rand

Compressors, Rotary . . . There are twelve sizes of two-stage Ro-Flo compressors to choose from. For complete information see bulletins 16B8244 and 16B8126 119 *Allis-Chalmers

Compressor, Rotary . . . New illustrated bulletin ACO 100.1 gives typical performance data on the axial-flow unit that combines advantages of reciprocating & centrifugal models. 231 Fairbanks-Morse & Co.

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Pumps, Process . . . The complete range offers all types of chemical process pumps, in all sizes & frames. Bul. EM-79 on "Mechanical Consideration in Pump Design" is offered. 90 *Food Mach. & Chem. Corp.

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Wearing Rings . . . eliminate pump jamming and prolong high efficiency. Give constant pump service. Complete details are available on request. 53 *Allis-Chalmers

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Blends while discharging; No segregation or flotation

Sturtevant Rotary Blenders start 4-way blending while charging, continue it during discharge, thus producing highly intimate, even blends of dry and semi-dry materials — within 3 to 5 minutes of start of charging.

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Scoops cascade material as drum rotates. Movement forces material from both ends to middle. Thus blending is 4-way right from start of charging.

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LITERATURE . . .

Services, Processes, Misc.

Bench-Scale Equipment a complete integrated line of professionally designed equipment for pressures up to 5000 p.s.i. Detailed information in Bulletin 658. 179 *Autoclave Engineers, Inc.

Construction Surveys, Reports, Appraisals, Process Engineering & Design, Procurement of Equipment & Materials for process industries. 83 *Stone & Webster Engineering Corp.

Cooling System The Uniltron Semi-Conductor Rectifier can be built in any desired d-c voltage & current rating. Complete information offered on request. 108 *I-T-E Circuit Breaker Co.

Disinfectants Manufactured products for promotion of health & sanitation. Research with insecticides, soap, etc. Literature available with complete information. 218A West Disinfecting Co.

Dynel Fabric Chemically resistant industrial clothing virtually unaffected by acids & alkalies. Booklet gives effects of reagents on dynel fabric after tests. 167 *Union Carbide Chemicals Co.

Fire Protection Systems new 44-page manual gives you a comprehensive picture of advanced methods for Special Hazard fire protection, with applications & charts. 36 *Grinnell Co.

Industrial Apparel resists punishing acids & chemicals. Complete facts about acid & caustic resistant apparel contained in catalog which is offered. 166 *Worklon, Inc.

LPG Installations 8 p. bulletin No. 66 illustrates and describes the design features of liquefied petroleum gas plants. Covers product properties and uses. 218B W. C. Holmes & Co. Ltd.

Metallurgy, Chloride 36 p. brochure, "Chloride Metallurgy", describes physical and chemical properties, uses, reactions of aluminum chloride, and antimony trichloride. 218C Stauffer Chemical Co.

Optical Systems Technical skill & complete facilities for highly precise work in optics, mechanics & electronics. Literature offered gives complete information. R211 *Kollmorgen Optical Corp.

Pulp Chlorination 9 p. bulletin No. P-1006, "Introduction of Chlorine Gas to Pulp Chlorinating Towers," includes equipment sketches and flow diagrams. 218D Pennsalt Chemicals Corp.

Structures Engineers, fabricators & erection specialist, for the challenge of things to come in the atomic age . . . structures to silhouette major reactor projects. 73 *Chicago Bridge & Iron Co.

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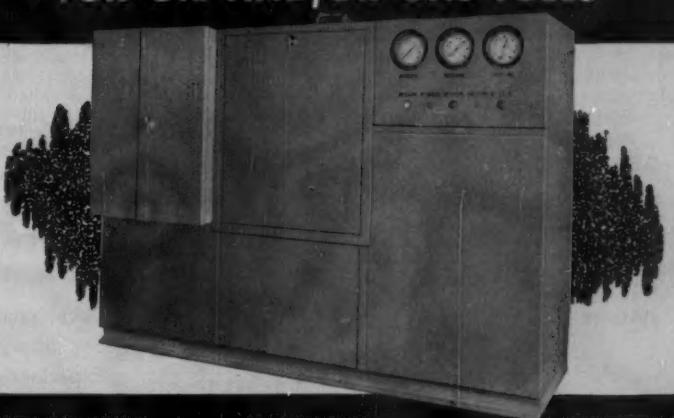
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3—American 42" x 120" Double Drum Dryers, 10 HP motors.
3—Bird 40" suspended Centrifugals, 347 S.S. perforated basket.
2—Bullovak, 250 & 20 sq. ft., 304 S.S. forced circulation Evaporators.
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1—Niagara 36 H-110 horizontal 304 S.S. Filter, 110 sq. ft.
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1—Baker Perkins #15 VUHM, 100 gal. jacketed Mixer, 100 HP motor.
1—Baker Perkins #15 JNM, 100 gal. jacketed Mixer, sigma blades.
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October 20 Issue

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316 S.S.

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8"x8" Precoat rubber covered Rotary Vacuum; 1—Oliver 3"x4" lead
Rotary Vacuum; 4—Sperry 36" rubber covered Plate & Frame, 30
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ROTARY DRYERS: 1—Traylor 5"x50"; 1—5"x24"; 1—4"x25"; 1—4"x20";
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agitated; 1—10"x8"; 2—9"x9"; 1—9"x10" agitated; 1—8"x40" Scrubber
Tank; 1—8"x24" Scrubber Tank; 1—8"x8" agitated; 1—6"x8" agitated;
2—5"x6" agitated; 1—4"x6" agitated.

LEAD LINED TANKS: 1—15"x20"; 1—15"x12"; 2—12"x14" agitated;
1—12"x12"; 2—10"x8"; 1—8"x12"; 1—8"x10" agitated; 2—8"x7" agitated.

STEEL TANKS: 1—12"x15"; 1—10"x12" agitated; 2—10"x10"; 1—8"x30"
pressure; 4—8"x30"; 1—8"x14"; 6—8"x10" agitated; 1—8"x8"; 1—8"x6"
agitated; 1—5"x12".

COMPRESSORS: 1—Worthington 1000 cfm, 30 psi; 1—Sullivan 1000
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cfm, 180 psi.

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Elevators 65 to 125 ft. high; Redler Conveyors 5" and 10"; Screw
Conveyors 6" and 9"; 150—LaBur, Durco, Worthite, Duriron and Stainless
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Tel. CYpress 2-5703

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Two complete briquetting plants

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- 4—Ruggles-Coles Class #XA-18 double shell indirect-direct heat rotary dryers, 104" x 70" x 5" welded steel outer shell.
- 4—Komrek-Greaves briquetting presses, 75 HP, 25 tons per hour.
- 4—Komrek-Greaves vertical Fluxers (paddle mixers), triple shaft, 150 HP.
- 4—K-G Horiz. Fluxers 41" dia., 50 HP.
- 4—K-G Pug Mills, 30" dia. x 14' 4" long.
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- 4—Vulcan type 316 SS bubble cap column, 3' dia x 18' with 11 trays
- 1—Foster Wheeler Dowtherm vaporizer, 6,000,000 BTU'S



THE GELB GIRL—OCTOBER 1958

CENTRIFUGES:

- 1—32" suspended type centrifuge with imperforate basket
- 3—Tolhurst center slung centrifuges, 40" and 48" with rubber covered perforated basket
- 1—Baker Perkins type 316 SS Ter Meer Centrifuge, Model HS-24"
- 1—Sharples #16P pressurite SS super centrifuge

DRYERS:

- 4—Link Belt steel roto louver dryers, Model 207-10, 310-16, 310-20, 604-20
- 1—Buflovak double drum dryer, 42" x 120"
- 1—Stokes Model 59DS steel rotary vacuum dryer, 5' x 30'
- 1—Stokes double drum dryer, 5' x 12'
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- 1—Oliver horizontal filter, 6'6"
- 1—Feinc SS rotary string filter, 3' x 3' (NEW)
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- 1—Lee SS jacketed kettle, 125 gals. 90° W. P.
- 1—Theo. Walters 500 SS jacketed reactor
- 1—Nickel jacketed 1000 gal. kettle
- 1—Patterson steel jacketed 3000 gal. kettle with agitator

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- 3—Robinson type 316 SS sigma type jacketed heavy duty mixers, 300 gal. 60 HP.
- 3—Howes 40 cu. ft. rubber covered ribbon blenders
- 1—Leader SS jacketed 51 cu. ft. ribbon blender

MISCELLANEOUS:

- 2—Heat Transfer Products steel bubble cap column, 36" and 42" with 5 and 10 trays
- 1—Acme steel bubble cap column 42" dia. with 10 trays
- 1—Downington Iron steel bubble cap column, 34" dia. with 14 trays
- 1—Type 316 SS stripping column 8" x 20'
- 7—Patterson Kelley, Carpenter 20 SS heat exchangers, 500 sq. ft. each
- 2—Patterson Kelley, steel heat exchangers, 1000 sq. ft. each
- 2—Badger type 316 SS heat exchangers, 400 and 480 sq. ft.
- 2—Belle & Grossett heat exchangers, steel, 73 sq. ft. each
- 6—Struthers Wells heat exchangers, 885 sq. ft.
- 1—Patterson Kelley steel heat exchanger, 427 sq. ft.
- 50—Steel heat exchangers from 15 sq. ft. to 400 sq. ft.
- 4—Type 317 SS heat exchangers, 892 sq. ft. each 200 PSI
- 30—Struthers Wells SS heat exchangers 650 sq. ft. each
- 1—Struthers Wells type 316 SS heat exchanger, 330 sq. ft.
- 2—Stokes tablet presses, Model T
- 1—Boiling 8" x 16" 3 roll laboratory calender
- 1—Swenson type 316 SS vacuum crystallizer, 3'6" x 12'
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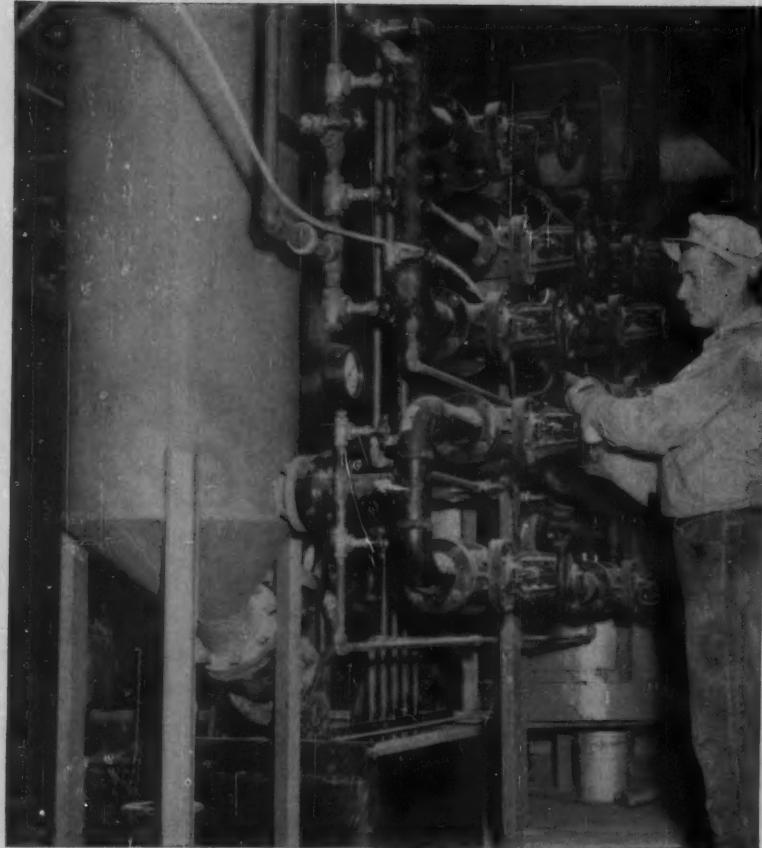
- 1—Badger type 316 SS bubble cap column 36" dia. with 8 trays
- 1—Badger type 316 SS bubble cap column 42" dia. with 11 trays
- 1—Acme type 316 SS jacketed kettle, 2000 gal.
- 1—Pfaudler glass lined jacketed kettle, Series P. 20 gal.

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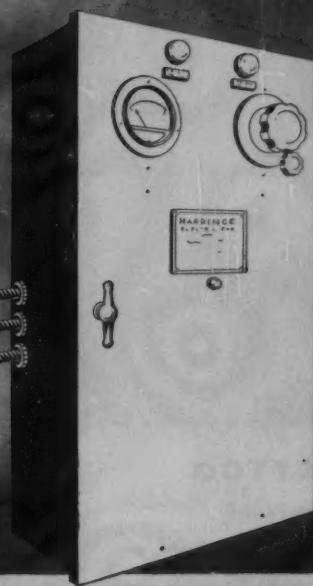
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In a recent survey of Hardinge "Electric Ear" users, many of them reported 10% to 15% increased grinding mill capacity after installing an "Electric Ear." This unit controls the mill feed, based upon grinding sound level, to produce optimum grinding conditions.

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"Approximately 25% gain in capacity."

"Helps prevent plug-ups."

"Maintains uniform mill load. Estimated gain in capacity 10%."

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"Eliminates human element in mill feed level."

"Saving per year—\$10,000.00."

"Principal reason for 'Electric Ear' use is that it aids the operator, and the mill can be operated from a remote panel."

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- Exclusive split coupling permits quick shaft interchange.
- High efficiency drive.

For pilot plant, continuous, or batch process operations, let Nettco specialists engineer the "process-rated" agitator best suited to your needs. Request Bulletin 581. Write **New England Tank & Tower Co.**, 87 Tileston Street, Everett 49, Massachusetts.



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WATER

REMOVE

organic matter
turbidity
color
iron



U. S. AIR FORCE PHOTO

HIGH-FLOW, UP-FLOW CLARIFIER

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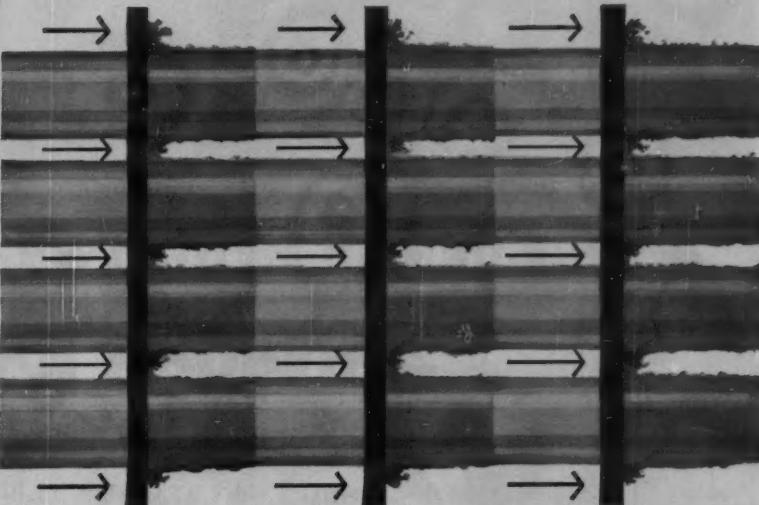
How a Paracoil "clean shave" gives you better heat transfer

Back and forth go the baffles . . . like blades . . . along the tube surfaces . . . shaving away accumulations of fouling materials . . . cleaning the heat exchanger . . . and giving process plants continuous, increased and better heat transfer.

This is the unique and principal feature of the Paracoil Self-Cleaning Heat Exchanger. Engineered with movable baffles, operated manually or by timed and automatic motor drive, stationary tubes are scraped and "shaved" free of fouling materials which are then carried away in the liquid.

The Paracoil Self-Cleaning Heat Exchanger eliminates the need to stop processing for cleaning purposes.

If you have a fouled heat exchanger problem, we may have the answer.



Davis Makes it — Better!

Below: Paracoil Vegetable Oil Chiller for converting a batch process to continuous cycle operation. Constructed of stainless steel and with an automatically timed, self-operating, self cleaning baffle assembly. The unit is presently improving product quality and rate of production in a vegetable oil processing plant.

Write for Bulletin 1000



DAVIS ENGINEERING CORPORATION

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B.F.Goodrich



Photo courtesy Jones & Laughlin Steel Corporation, Pittsburgh, Penna.

Good riddance to bad rubbish —through hose

B.F. Goodrich improvements in rubber brought extra savings

Problem: At this power plant they have to get rid of huge loads of a waste material, called fly ash, every day. It's collected from furnaces, washed, then piped down the side of that building and away to a disposal pit so as not to pollute the air or a near-by river. Fine, except that this mixture of gritty fly ash, corrosive acid water, sharp slivers of metal was eating holes through the metal pipe in only six months. Each pipe replacement cost \$700 plus about 100 hours of workers' time.

What was done: Company engineers,

working with a B.F.Goodrich distributor, decided to replace the pipe with rubber hose specially developed by B.F.Goodrich to handle rough materials. The lining of this hose is made with the toughest, wear-resisting rubber known. The hose is so rugged that it's even used in some places to handle broken glass, chunks of coal, granite chips.

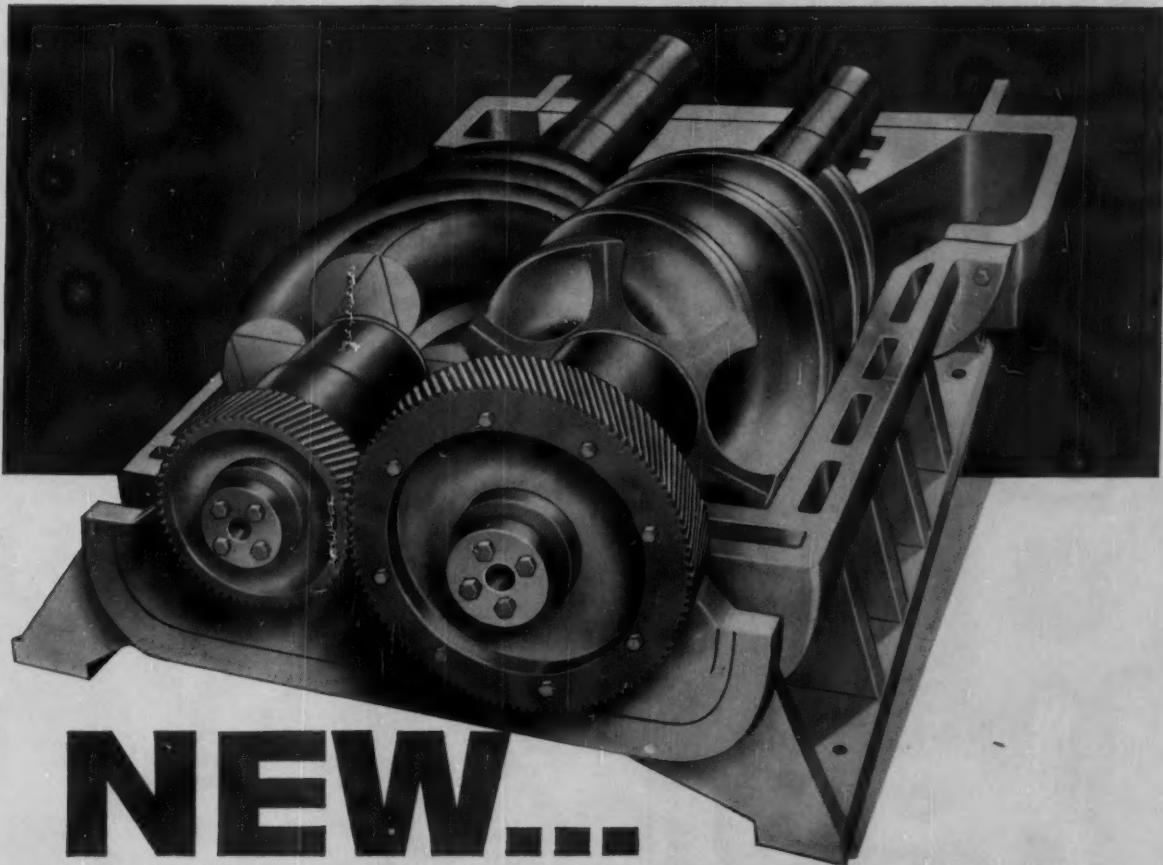
Savings: The B.F.Goodrich hose had been on the job 8 years when the picture was taken. It gulps thousands of gallons of acid water and grit every day,

but shows no sign of wear, looks good for many years more.

By lasting 7½ years longer than pipe, plant engineers figure that the B.F.Goodrich hose has already saved \$6400 in replacement costs and \$4800 worth of maintenance time.

Where to buy: Your B.F.Goodrich distributor has exact specifications for the B.F.Goodrich hose described here. And, as a factory-trained specialist in rubber products, he can answer your questions about *all* the rubber products B.F.Goodrich makes for industry. *B.F.Goodrich Industrial Products Company, Dept. M-451, Akron 18, Ohio.*

B.F.Goodrich *industrial rubber products*



NEW...

Fairbanks-Morse Positive Displacement Axial-Flow Rotary Compressor

Combines the best features of reciprocating and centrifugal compressors

Consider the advantages of the all-new Fairbanks-Morse two-impeller, helical-lobe type, axial-flow rotary compressor:

- 1 Delivers oil-free air or gas with low ratios of unit weight and space to capacity.
- 2 Exhibits high efficiencies and positive-displacement stability of flow at varying compression ratios and speeds.

Result: Ideal performance from a relatively small compressor that is mechanically simple, flexible in application, adaptable to any power source; a compressor that provides stable performance, smooth operation, and variable-capacity control.

This all-new F-M Compressor is available in 5 standard case and impeller sizes, single-stage and multi-stage units—for pressure, vacuum or booster service. Capacities range from 800 to 13,000 cfm.—also higher or lower if desired, on custom-designed basis. Contact your Fairbanks-Morse branch for further information, or write directly to Fairbanks, Morse & Co., 600 So. Michigan Ave., Chicago 5, Illinois.



Ask for new illustrated bulletin ACO 100.1 giving typical performance characteristics and other important data.



FAIRBANKS-MORSE
a name worth remembering when you want the **BEST**

Will you reap the long-term payoff of good mixer shaft sealing?

If you want to minimize your mechanical fluid mixing costs, take a hard look at *mixer shaft sealing*.

This is the area where profits can leak away unnoticed. The right shaft seal makes all the difference between an efficient mixing operation and a ruinously expensive one.

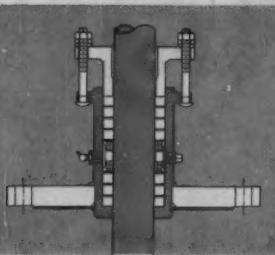
When you're aiming for low-cost shaft sealing, *don't be fooled* by low first cost. Instead, look for solid long-range savings you can make in terms of *smooth opera-*

tion, rapid maintenance, minimum downtime.

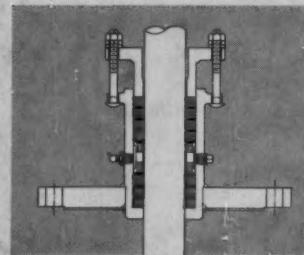
Here are some mechanical reasons why you get these savings with **LIGHTNIN Mixers**. Every one of the features illustrated below is a **LIGHTNIN "first."** Many are yours only with **LIGHTNIN**s. And only **LIGHTNINs** give you *all* of them!

For lowest-cost fluid mixing, see your **LIGHTNIN Mixer** representative soon. Look him up in *Chemical Engineering Catalog*. Or write us direct.

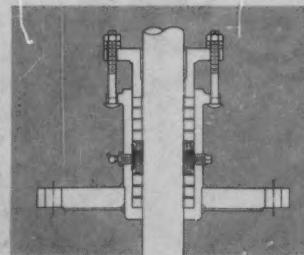
How you cut mixing cost with the *Lightnin* stuffing box



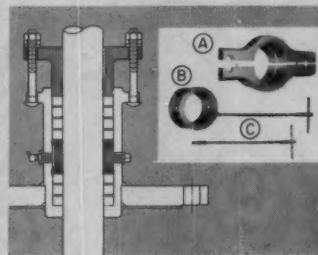
1. SAVE COST of a special-alloy mounting flange with all-welded **LIGHTNIN** construction. Forged steel flange is faced with correct alloy for your process conditions. Hub is solid alloy. Alloy parts are shown in color.



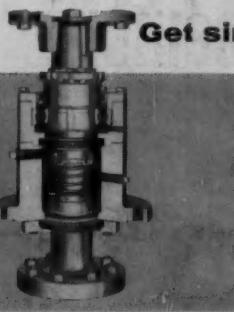
2. GET SUPERIOR SEALING with 7 rings of large-cross-section packing. Separators facilitate packing removal, distribute force uniformly. Gland bolts, threaded part way, prevent overtightening.



3. GET BETTER LUBRICATION without repacking. Lantern ring evenly distributes lubricant; permits continuous lubrication under pressure; extends time between repackings. Relief plug prevents overlubrication.



4. REPACK FASTER with exclusive split packing gland (A) that comes right off the shaft to allow maximum work space. Lantern ring (B) lifts out quickly by means of pullers (C), standard accessories.



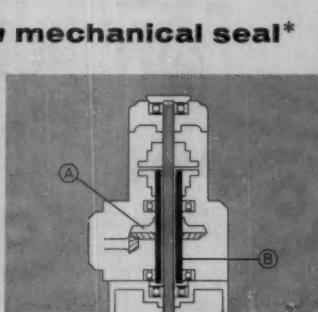
1. ELIMINATE REPACKING and adjustment with this cartridge-type **LIGHTNIN** rotary mechanical seal assembly, optional on all **LIGHTNIN** Mixers. It's saving many users thousands of maintenance dollars a year.



2. GET WIDEST CHOICE of seal designs and materials to meet your conditions: stainless steels, Stellite, Hastelloy alloys, bronze, ceramic, Teflon, etc. Handle pressures to 2500 psig and all temperature ranges.



3. REPLACE SEAL ASSEMBLY quickly, if ever necessary—without dismantling mixer or removing it from tank, and without skilled manpower. Seal cartridge unbolts, comes out as a unit; replacement bolts in.



4. RETAIN GEAR ALIGNMENT when changing seal. Mixer gears (A) are isolated from shaft by hollow drive quill† (B) —cannot get out of line when seal is removed. Shaft realignment is automatic on reassembly.

†patented

WHAT MIXING OPERATIONS are important to you? You'll find a wealth of information on fluid mixing in these helpful bulletins describing **LIGHTNIN** Mixers:

- Top or bottom entering; turbine, paddle, and propeller types: 1 to 500 HP (B-102)
- Side entering: 1 to 25 HP (B-104)
- Top entering; propeller types: 1/4 to 3 HP (B-103)
- Laboratory and small-batch production types (B-112)
- Portable: 1/4 to 3 HP (B-106)
- Condensed catalog showing all types (B-109)
- Quick-change rotary mechanical seals for pressure and vacuum mixing (B-111)
- Confidential data sheet for figuring your mixer requirements (B-107)

Check, clip and mail with your name, title, company address to:

MIXING EQUIPMENT Co., Inc., 128-K Mt. Read Blvd., Rochester 3, N.Y.

In Canada: **Greay Mixing Equipment, Ltd.**, 100 Miranda Ave., Toronto 19, Ont.

Lightnin
Mixers

MIXCO fluid mixing specialists

*patent pending